

AD-A102 979

OGDEN AIR LOGISTICS CENTER HILL AFB UT PROPELLANT AN-ETC F/6 21/9.2
PROPELLANT SURVEILLANCE REPORT ANB-3066 PROPELLANT. (U)

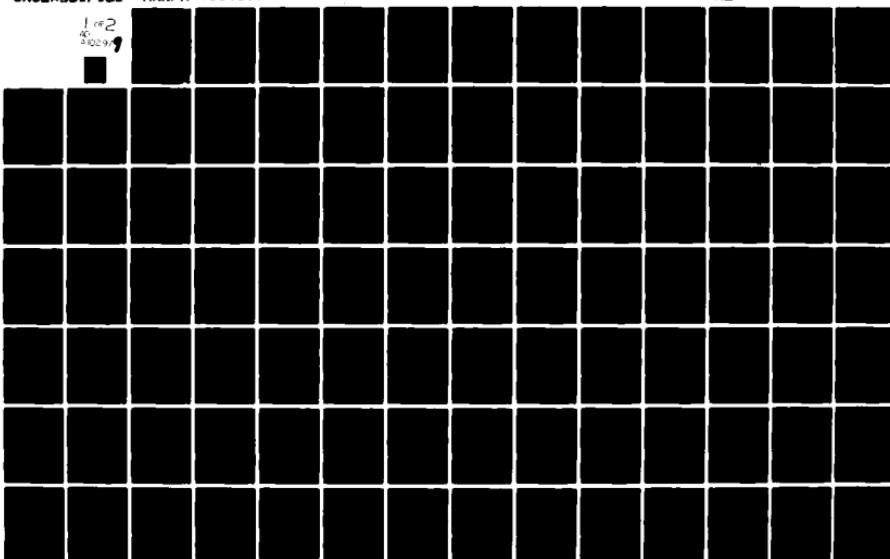
DEC 80 E M DALABA

UNCLASSIFIED

MAKPH-850(80)

NL

1 of 2
40
30299



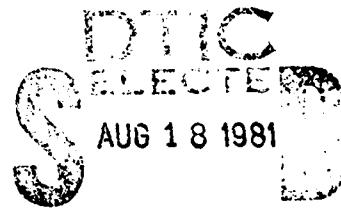
ADA102979

HEADQUARTERS
OGDEN AIR LOGISTICS CENTER
UNITED STATES AIR FORCE
HILL AIR FORCE BASE, UTAH 84056

PROPELLANT
SURVEILLANCE REPORT
ANB-3066 PROPELLANT

PROPELLANT LABORATORY SECTION

MAKPH REPORT NR 450(80)



A

DECEMBER 1980

APPROVED FOR PUBLIC RELEASE, DISTRIBUTION UNLIMITED

DTIG FILE COPY

MAKPH REPORT NR 450(80)
MMWRM PROJECT M14058C

PROPELLANT SURVEILLANCE REPORT
ANB-3066 PROPELLANT

Author

Elizabeth M. Dalaba

ELIZABETH M. DALABA, CHEMIST
Component & Combustion Test Unit

Engineering & Statistical Review By

Glenn S. Porter
GLENN S. PORTER, Project Engineer
Engineering & Reliability Branch

Dan L. Petersen
DAN L. PETERSEN, Mathematician
Data Analysis Unit

Recommended Approval By

Leonidas A. Brown
LEONIDAS A. BROWN, Chief
Component & Combustion Test Unit

Ronald F. Larsen
RONALD F. LARSEN, Chief
Physical & Mechanical Test Unit

Approved By

Anthony J. Inverso
ANTHONY J. INVERSO, Chief
Propellant Analysis Laboratory

December 1980

Directorate of Maintenance
Ogden Air Logistics Center
United States Air Force
Hill Air Force Base, Utah 84056

ABSTRACT

This report contains test results from LGM-30 F and G, Stage II and Stage III propellant. Data are shown in linear regression plots.

The differences between polymers used in the propellant are shown in the composite plots for very low rate tensile, high rate tensile and stress relaxation data and are most evident in gradient stress relaxation modulus.

Case liner bonds continue to show significant degradation although the rate of change has slowed.

Accession For	
NTIS	GP&I
F77C TAB	<input checked="" type="checkbox"/>
Unannounced	<input type="checkbox"/>
Classification	
Distribution/	
Availability Codes	
Avail and/or	
Direct	Special
A	

TABLE OF CONTENTS

<u>Section</u>		<u>Page</u>
	Abstract	ii
	List of Tables	iv
	List of Figures	v
	List of References	ix
	Glossary of Terms and Abbreviations	xi
I	Introduction	1-1
II	Test Program	2-1
III	Statistical Summary	3-1
IV	Very Low Rate Tensile	4-1
V	High Rate Tensile	5-1
VI	Stress Relaxation and Strain Dilatation	6-1
VII	Thermal Coefficient of Linear Expansion	7-1
VIII	Case Liner Bonds	8-1
IX	Tear Energy	9-1
	Distribution List	10-1
	DD 1473	10-2

LIST OF TABLES

<u>Table</u>		<u>Page</u>
1-1	Failure Criteria	1-2
2-1	Comparison of Standard Deviation	2-3
	Analysis of Covariance Comparison of Regressions	
3-1	Very Low Rate Tensile	3-3
3-2	High Rate Triaxial Tensile	3-4
3-3	High Rate Hydrostatic Tensile	3-5
3-4	Stress Relaxation Modulus	3-6
3-5	TCLE	3-7
3-6	Strain Dilatation	3-8
4-1	Very Low Rate Tensile, Significance of Regressions	4-2
5-1	High Rate Triaxial Tensile, Significance of Regression Slopes	5-2
5-2	High Rate Dogbones, Significance of Regressions	5-2
6-1	Stress Relaxation, Significance of Regressions	6-3
6-2	Strain Dilatation, Significance of Regressions	6-3
7-1	TCLE, Significance of Regression Slopes	7-3
8-1	Summary of Regression Analyses, Stress vs Time-to-Failure	8-4
9-1	Tear Energy, Significance of Regression Slopes	9-2

LIST OF FIGURES

<u>Figure Nr</u>		<u>Page</u>
Data Plots, Very Low Rate Tensile		
4-1	ANA 'G' Maximum Stress, Unlined Cartons	4-3
4-2	ANA 'G' Strain at Rupture, Unlined Cartons	4-4
4-3	ANA 'G' Modulus, Unlined Cartons	4-5
4-4	ANB 'G' Maximum Stress, Unlined Cartons	4-6
4-5	ANB 'G' Strain at Rupture, Unlined Cartons	4-7
4-6	ANB 'G' Modulus, Unlined Cartons	4-8
4-7	ANB 'G' Maximum Stress, Lined Cartons	4-9
4-8	ANB 'G' Strain at Rupture, Lined Cartons	4-10
4-9	ANB 'G' Modulus, Lined Cartons	4-11
4-10	ANT 'P' Maximum Stress, Unlined Cartons	4-12
4-11	ANT 'P' Strain at Rupture, Unlined Cartons	4-13
4-12	ANT 'P' Modulus, Unlined Cartons	4-14
4-13	ANA & ANB 'G' Maximum Stress, Unlined Cartons	4-15
4-14	ANA & ANB 'G' Strain at Rupture, Unlined Cartons	4-16
4-15	ANA & ANB 'G' Modulus, Unlined Cartons	4-17
4-16	ANB 'G' & 'P' Maximum Stress, Unlined Cartons	4-18
4-17	ANB 'G' & 'P' Strain at Rupture, Unlined Cartons	4-19
4-18	ANB 'G' & 'P' Modulus, Unlined Cartons	4-20
4-19	ANB 'G' & 'P' Maximum Stress, Lined Cartons	4-21
4-20	ANB 'G' & 'P' Strain at Rupture, Lined Cartons	4-22
4-21	ANB 'G' & 'P' Modulus, Lined Cartons	4-23
4-22	ANT & ANB 'P' Maximum Stress, Lined Cartons	4-24
4-23	ANT & ANB 'P' Strain at Rupture, Lined Cartons	4-25
4-24	ANT & ANB 'P' Modulus, Lined Cartons	4-26

LIST OF FIGURES (cont)

<u>Figure Nr</u>		<u>Page</u>
Data Plots, High Rate Triaxial Tensile		
5-1	ANB 'G' Maximum Stress, Lined Cartons	5-3
5-2	ANB 'G' Strain at Rupture, Lined Cartons	5-4
5-3	ANB 'G' Modulus, Lined Cartons	5-5
5-4	ANT 'P' Maximum Stress, Lined Cartons	5-6
5-5	ANT 'P' Strain at Rupture, Lined Cartons	5-7
5-6	ANT 'P' Modulus, Lined Cartons	5-8
5-7	ANB 'G' & 'P' Maximum Stress, Unlined Cartons	5-9
5-8	ANB 'G' & 'P' Strain at Rupture, Unlined Cartons	5-10
5-9	ANB 'G' & 'P' Modulus, Unlined Cartons	5-11
5-10	ANT 'P' & ANB 'P' Maximum Stress, Lined Cartons	5-12
5-11	ANT 'P' & ANB 'P' Strain at Rupture, Lined Cartons	5-13
5-12	ANT 'P' & ANB 'P' Modulus, Lined Cartons	5-14
Data Plots, High Rate Hydrostatic Tensile, 600 psi		
5-13	ANB 'G' Maximum Stress, Unlined Cartons	5-15
5-14	ANB 'G' Strain at Rupture, Unlined Cartons	5-16
5-15	ANB 'G' Modulus, Unlined Cartons	5-17
5-16	ANB 'P' Maximum Stress, Unlined Cartons	5-18
5-17	ANB 'P' Strain at Rupture, Unlined Cartons	5-19
5-18	ANB 'P' Modulus, Unlined Cartons	5-20
5-19	ANT 'P' Maximum Stress Lined Cartons	5-21
5-20	ANT 'P' Strain at Rupture, Lined Cartons	5-22
5-21	ANT 'P' Modulus, Lined Cartons	5-23
Data Plots, Stress Relaxation Modulus (Polymer)		
6-1	ANB 'G' Unlined Cartons, 10 sec, 1% Strain	6-4
6-2	ANB 'G' Unlined Cartons, 1000 sec, 1% Strain	6-5

LIST OF FIGURES (cont)

<u>Figure Nr</u>		<u>Page</u>
6-3	ANB 'G' Unlined Cartons, 10 sec 3% Strain	6-6
6-4	ANB 'G' Unlined Cartons, 1000 sec, 3% Strain	6-7
6-5	ANB 'P' Unlined Cartons, 10 sec, 1% Strain	6-8
6-6	ANB 'P' Unlined Cartons, 1000 sec, 1% Strain	6-9
6-7	ANB 'P' Unlined Cartons, 10 sec, 3% Strain	6-10
6-8	ANB 'P' Unlined Cartons, 1000 sec, 3% Strain	6-11
6-9	ANB 'P' Lined Cartons, 10 sec, 3% Strain	6-12
6-10	ANB 'P' Lined Cartons, 1000 sec, 3% Strain	6-13
6-11	ANT 'P' Unlined Cartons, 10 sec, 3% Strain	6-14
6-12	ANT 'P' Unlined Cartons, 1000 sec, 3% Strain	6-15
6-13	ANT 'P' Lined Cartons, 10 sec, 1% Strain	6-16
6-14	ANT 'P' Lined Cartons, 1000 sec, 1% Strain	6-17
6-15	ANT 'P' Lined Cartons, 10 sec, 3% Strain	6-18
6-16	ANT 'P', Lined Cartons, 1000 sec, 3% Strain	6-19
6-17	ANA & ANB 'G' Unlined Cartons, 10 sec, 1% Strain	6-20
6-18	ANA & ANB 'G' Unlined Cartons, 1000 sec, 1% Strain	6-21
6-19	ANT & ANB 'P' Unlined Cartons, 10 sec, 1% Strain	6-22
6-20	ANT & ANB 'P' Unlined Cartons, 1000 sec, 1% Strain	6-23
6-21	ANT & ANB 'P' Lined Cartons, 10 sec, 1% Strain	6-24
6-22	ANT & ANB 'P' Lined Cartons, 1000 sec, 1% Strain	6-25
6-23	ANB & ANT Gradient Stress Relaxation Modulus, 6 sec	6-26
6-24	ANB & ANT Gradient Stress Relaxation Modulus, 60 sec	6-27
Data Plots, Thermal Coefficient of Linear Expansion (TCLE)		
7-1	ANB 'G' Glass Point, Unlined Cartons	7-3
7-2	ANB 'G' TCLE Below Tg (glass Point)	7-4

LIST OF FIGURES (cont)

<u>Figure Nr</u>		<u>Page</u>
7-3	ANB 'G' TCLE Above Tg, Unlined Cartons	7-5
7-4	ANB 'P' Glass Point, Unlined Cartons	7-6
7-5	ANB 'P' TCLE Below Tg, Unlined Cartons	7-7
7-6	ANB 'P' TCLE Above Tg, Unlined Cartons	7-8
7-7	ANT 'P' Glass Point, Unlined Cartons	7-9
7-8	ANT 'P' TCLE Below Tg, Unlined Cartons	7-10
7-9	ANT 'P' TCLE Above Tg, Unlined Cartons	7-11
7-10	ANT 'P' Glass Point, Lined Cartons	7-12
7-11	ANT 'P' TCLE Below Tg, Lined Cartons	7-13
7-12	ANT 'P' TCLE Above Tg, Lined Cartons	7-14

REFERENCES

<u>Report Nr</u>	<u>Title</u>	<u>Date</u>
MAGCP 75 (67)	Zero Time Test Results LGM-30 Second Stage Wing VI Propellant	13 Jan 67
MAGCP 111 (67)	ATP Test Results LGM-30 Stage II Propellant Wing VI, Phase I	1 Dec 67
MAGCP 142 (68)	ATP Test Results LGM-30, Stage II Propellant, Wing VI, Phase I Series II	Nov 68
MAGCP 188 (70)	ATP Test Results LGM-30, Stage II Propellant, Wing VI, Phase I Series II	Jul 70
MAGCP 212 (71)	Propellant Surveillance Report LGM-30 Stage II (Wing 6 ANB-3066)	Jun 71
MAGCP 240 (72)	Propellant Surveillance Report LGM-30F Stage II ANB-3066	May 72
MAGCP 256 (72)	Propellant Surveillance Report Minuteman III, Stage III	Oct 72
MANCP 331 (75)	Propellant Surveillance Report Minuteman III, Stage III	Oct 75
Aerojet 0162-AS-6-1A	Ten Year Aging Program for Wing VI Minuteman Second Stage Motors and Components	Sep 67
Aerojet 0162-06-SAAS-7		Oct 71
0162-06-SAAS-8		Apr 71
0162-06-SAAS-9	Ten Year Aging and Storage Program Wing VI Minuteman Second Stage	Oct 71
0162-06-SAAS-10	Motors and Components Program Progress	Apr 72
0162-06-SAAS-11		Oct 72
0162-06-SAAS-12		Apr 73
0162-06-SAAS-13		Oct 74
0162-06-SAAS-14		Jul 75
0162-06-SAAS-15		Dec 75
0162-06-SAAS-16		Jul 76
0162-06-SAAS-17		Mar 77

REFERENCES (cont)

<u>Report Nr</u>	<u>Title</u>	<u>Date</u>
Aerojet 0162-06-AS-F Appendix E	Final Report, Wing VI Minuteman Second Stage Motor Propellant Aging	Jan 74
MVS-1	Manufacturing Variables, Study of The Minuteman Stage II Motor	11 Jun 76
0162-06-SAAS-18	Ten Year Aging and Storage Program Wing VI Minuteman Second Stage	18 Aug 77
0162-06-SAAS-19	Motors and Components Program Progress	19 Feb 78
0162-06-SAAS-20		20 May 78

GLOSSARY OF ABBREVIATIONS AND TERMS

Aging Trend	A change in properties of performance resulting from aging of material or component
ANA	Aerojet Propellant, Stage III (ANB 3066 Formulation)
ANT	Thiokol Propellant, Stage III (ANB 3066 Formulation)
ANB	Aerojet Propellant, Stage II (ANB 3066 Formulation)
ASPC	Aerojet Strategic Propulsion Co.
CSA	Cross Sectional Area
DB	Dogbone
Degradation	Gradual deterioration of properties or performance
E	Modulus (psi), defined as the slope of the line drawn tangent to the initial linear portion of the curve
EB	End Bonded
EGL	Effective Gage Length
e _m	Strain at Maximum Stress (in/in)
e _r	Strain at Rupture (in/in)
"F" ratio	The ratio of the variance accounted for by the regression function to the random unexplained variance. The regression function having the most significant "F" ratio is used for plotting data. The ratio is also used in detecting significant changes in random variation between succeeding time points.
JANNAF	Joint Army, Navy, NASA, Air Force Committee
MAKPH	Propellant Laboratory at OOALC
OOALC	Ogden Air Logistics Center
Post Curing	Period up to 12 - 16 months after manufacture

GLOSSARY OF ABBREVIATIONS AND TERMS (CONT.)

Regression	The general form of the regression equation is $Y = a + bx$
Regression Line	Line representing mean test values with respect to time
s_b	Standard error of estimate of the regression coefficient
s_e or $s_{Y.X}$	Standard deviation of the data about the regression line
s_m	Maximum Stress (psi)
s_r	Stress at Rupture (psi)
Standard Deviation (s_y)	Square root of variance
Strain Rate	Crosshead speed divided by the EGL
Thiokol	Thiokol/Wasatch Division
"t" Test	A statistical test used to detect significant differences between a measured parameter and an expected value of the parameter (determines if regression slope differs from zero at the 95% confidence level)
Variance	The sum of squares of deviations of the test results from the mean of the series after division by one less than the total number of test results
3 Sigma Band	The area between the upper and lower 3 sigma limit. It can be expected that 99.73% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed.
90-90 Band	It can be stated with 90% confidence that 90% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed.

SECTION I
INTRODUCTION

A. PURPOSE:

The purpose of testing ANB-3066 propellant, used in Minuteman II Stage II and Minuteman III Stage II and Stage III, is to monitor and evaluate aging effects on this propellant which will contribute to the operational motor serviceability prediction. Testing was performed according to General Test Directive GTD-2C, Amendment 1, and MMWRBM Project M14058C.

B. BACKGROUND:

Service life testing of ANB-3066 carton propellant from Aerojet production began at Ogden ALC in 1966. When production for Minuteman III Stage III was transferred to Thiokol, the propellant samples from both Aerojet and Thiokol were tested. As lined cartons were produced, these were tested adding propellant liner bond specimens to the program. This report contains data from all these sources for propellant aged 13 to 162 months.

Although many of the parameters tested indicate significant aging trends, only case liner/insulation bond strengths appear to be approaching the alert limit. Significance tables for aging trend lines are given in the respective sections of the report.

Statistical techniques used are described in Section III.

Low rate uniaxial tensile tests and hardness are routine tests for all propellant. The next report will include these data. Poisson's ratio and cohesive tear energy tests have been applied to only a portion of the cartons. Regressions are shown only when all parameters of a test are significant.

SECTION II

TEST PROGRAM

Cartons representing raw material combinations were subjected to a random selection process designed to test all material lots within a two year-four test periods interval. When propellant cartons have been aged one year, they are added to the test program. Latest acquisition of Stage II was manufactured Dec 17, 1978, and Stage III manufactured April 4, 1977.

Propellant cartons are identified by source of manufacture. Stage II and III propellant manufactured by Aerojet Strategic Propulsion Company is identified as ANB and ANA respectively. Thiokol Company Stage III propellant is identified as ANT. All regressions use this nomenclature as well as additional information as to the type of carton, lined or unlined. Symbols are used on multiple regressions to separate types. There were two suppliers for polymers for Stage II propellant, "G" polymer manufactured by General Tire and Rubber and "P" polymer for Phillips. In this report the two polymer types have been treated statistically.

Lined and unlined cartons of ANB and ANT have been combined in regression analysis for comparison purposes and cover the time span from 13 through 162 mo.

The physical-mechanical tests which relate directly to stress analysis are limited. Very low rate tensile test data is related to storage conditions, and high rate rails tested under pressure relate to ignition. Stress relaxation modulus also relates to storage conditions. The thermal coefficient of linear expansion reflects some of the thermal stress to which the motor is exposed.

Low rate uniaxial tensile tests and hardness are routine tests for all propellant. These data were subjected to statistical analyses in the last report. Poisson's ratio and cohesive tear energy tests have been applied to only a portion of the cartons. Data from these tests has been analyzed for this report.

TABLE 2-1

Comparison of Standard Deviation

System	Very Low Rate Tensile			High Rate Tensile			Stress Relaxation			
	S _m	er	E	S _m	er	E	10 sec	1000 sec	10 sec	1000 sec
ANA G Unlined	6.16	.0172	70.48	32.19	.0235	834.15				
ANB G Unlined	7.82	.0193	96.00	36.56	.0300	1304.66	174.54	110.21	160.56	85.84
ANB G Lined	6.93	.0187	83.05	28.42	.0219	687.09	91.97	52.06	87.52	52.74
ANB P Unlined	8.56	.0320	134.51	40.37	.0306	1298.00	253.56	147.03	227.47	130.72
ANB P Lined	7.24	.0187	83.20	36.67	.0267	675.97	109.31	67.58	113.81	67.18
ANT P Unlined	8.79	.0210	99.88	33.08	.0285	805.10	142.69	102.38	169.01	100.09
ANT P Lined	8.14	.0172	73.53	33.28	.0223	698.38	122.16	76.49	118.38	68.04
ANA & ANG G Unlined	7.57	.0190	91.71	36.17	.0304	1239.89	174.43	110.17		
ANB G & P Unlined	8.28	.0262	116.85	43.31	.0317	1320.32	240.19	140.06		
ANB G & P Lined	7.14	.0189	83.79	34.55	.0254	677.16	104.70	61.86		
ANB & ANT P Unlined	9.00	.0301	127.57	37.65	.0338	1162.80	222.9	129.48		
ANB & ANT P Lined	8.26	.0195	85.08	35.78	.0264	773.75	121.98	76.06		

SECTION III
STATISTICAL SUMMARY

Data analyses of all propellant tested by MAKPH having the ANB 3066 formulation are contained in this report. ANB 3066 propellant is divided into three groups, each group pertaining to a specific rocket motor application. These propellant groups are further classified with regards to the manufacturer of the polymer contained in the propellant. The two manufacturers of ANB 3066 polymer are General Tire and Rubber ('G' type) and Phillips ('P' type). The three propellant groups are designated in this report as follows:

<u>Code</u>	<u>Polymer Type</u>	<u>Manufacturer and System Application</u>
ANA	G	Aerojet: MINUTEMAN III, Stage III
ANB	G and P	Aerojet: MINUTEMAN II, Stage II
ANT	P	Thiokol: MINUTEMAN III, Stage III

Propellant specimens for the ANA group were taken from unlined cartons and contains only "G" type polymer. Specimens for the ANB and ANT groups were taken from unlined cartons and also from cartons having a simulated case liner along one surface of the carton. Propellant from the ANB group contains both "G" and "P" type polymers. ANT propellant contains only "P" type polymer. Each propellant group is further sub-divided into propellant lots.

Test data from each propellant group have previously been analyzed to test for similarities between propellant lots within a given propellant group, as well as polymer type and carton type. The results of these analyses indicated statistically significant differences in the test data which preclude combining

data from different groups, lots, or cartons. These analyses are shown in Tables 3 - 1 through 3 - 6.

The statistical approach used for this report was to characterize the aging trend for each test parameter using linear regression analyses. Regression techniques were used to study a particular test response as a function of propellant age. A simple linear regression model of the form, $Y = a + b(X)$, was used by assigning propellant age to the variable X in the model.

Separate regression analyses were performed for each propellant group and sub group; i.e., for a specific carton type within a given polymer and propellant group. Regression plots have been included where the slope of the regression line is significantly different from a line of zero slope for all parameters. Tables providing a summary of the significance or non-significance of the regression analysis for each test parameter are included in an appropriate section of this report for each test conducted. Table 2-1 provides a summary standard deviations for the three tests of greatest importance.

Several regression analyses were performed on combined data for various carton types and propellant groups. Carton types and propellant groups are differentiated on the plots for these analyses by using different plotting symbols. Regression plots of these combined or "composite" data are included in this report solely for comparison with corresponding plots from the last test period.

TABLE 3-1
ANALYSIS OF COVARIANCE COMPARISON OF REGRESSIONS
VERY LOW RATE TENSILE (0.0002 in/min)

	<u>Sm</u>	<u>Er</u>	<u>E</u>
ANA-ANB (G-Polymer, Unlined)			
Residual Variance	S	S	S
Slope	NS	NS	NS
Elevation	S	S	NS
Lined-Unlined (ANB P-Polymer)			
Residual Variance	S	S	S
Slope	S	S	S
Elevation	S	NS	S
Lined-Unlined (ANT P-Polymer)			
Residual Variance	NS	S	S
Slope	S	S	NS
Elevation	S	S	S
G-P Polymer (ANB Lined)			
Residual Variance	NS	NS	NS
Slope	NS	NS	NS
Elevation	NS	S	NS
G-P Polymer (ANB Unlined)			
Residual Variance	S	S	S
Slope	NS	NS	NS
Elevation	S	NS	S
ANA-ANB-ANT - Lined-Unlined - G-P			
Chi-square Variance	S	S	S
Slope	S	S	S
Elevation	S	S	S

NOTE: Sm = Maximum Stress (psi)
 Er = Strain at Rupture (in/in)
 E = Modulus (psi)

See pages x and xi for additional information on terms and abbreviations.

TABLE 3-2

ANALYSIS OF COVARIANCE COMPARISON OF REGRESSIONS

HIGH RATE TRIAXIAL TENSILE (1750 in/min, 600 psi)

	<u>Sm</u>	<u>Er</u>	<u>E</u>
ANA (G Unlined) - ANT (P Unlined)			
Residual Variance	S	S	S
Slope	S	S	S
Elevation	S	S	S
G-P Polymers (ANB Unlined)			
Residual Variance	S	NS	NS
Slope	NS	S	NS
Elevation	S	S	S
G-P Polymers (ANB Lined)			
Residual Variance	S	S	NS
Slope	NS	S	S
Elevation	NS	NS	NS
Lined - Unlined (ANB P-polymer)			
Residual Variance	NS	NS	S
Slope	NS	NS	S
Elevation	S	S	S
Lined - Unlined (ANT P-polymer)			
Residual Variance	NS	S	S
Slope	NS	S	S
Elevation	S	S	NS
ANA - ANB (G Unlined)			
Residual Variance	NS	S	S
Slope	NS	NS	NS
Elevation	S	S	S

TABLE 3-3
ANALYSIS OF COVARIANCE COMPARISON OF REGRESSIONS
HIGH RATE HYDROSTATIC TENSILE (1750 in/min, 600 psi)

	<u>Sm</u>	<u>Er</u>	<u>E</u>
G - P (ANB Unlined)			
Residual Variance	S	S	S
Slope	NS	S	S
Elevation	S	S	S
G - P (ANB Lined)			
Residual Variance	NS	S*	S
Slope	S	NS	S
Elevation	S	NS	S
Lined-Unlined (ANT P-polymer)			
Residual Variance	NS	S	NS
Slope	NS	NS	NS
Elevation	S	NS	S
ANB(G) - ANB (P) -ANT (P) (Lined)			
Residual Variance	NS	NS	S
Slope	S	NS	S
Elevation	S	NS	S

*Close to being significant

TABLE 3-4
ANALYSIS OF COVARIANCE COMPARISON OF REGRESSION
STRESS RELAXATION MODULUS

	1% Strain		3% Strain	
	10 sec	100 sec	10 sec	100 sec
G - P (ANB Unlined)				
Residual Variance	S	S	S	S
Slope	S	S	S	S
Elevation	S	S	S	S
G - P (ANB Lined)				
Residual Variance	NS	S*	S	S*
Slope	NS	NS	NS	NS
Elevation	S	NS	S	NS
Lined - Unlined (ANT P-polymer)				
Residual Variance	S	S	S	S
Slope	S	S	S	S
Elevation	NS	NS	S	S
Lined - Unlined (ANB P-polymer)				
Residual Variance	S	S	S	S
Slope	NS	NS	NS	NS
Elevation	S	S	S	S
Lined - Unlined (ANB G)				
Residual Variance	S	S	S	S
Slope	NS	NS	NS	S
Elevation	S	S	S	S
ANA - ANB (G Unlined)				
Residual Variance	NS	NS	NS	NS
Slope	NS	NS	S	S
Elevation	NS	S	NS	NS

* Close to being not significant

TABLE 3-5
ANALYSIS OF COVARIANCE COMPARISON OF REGRESSION

	TCLE <u>Glass Point</u>	TCLE Below GP	TCLE Above GP
G - P (ANB Unlined)			
Residual Variance	S	NS	S*
Slope	NS	NS	NS
Elevation	NS	S	NS
G - P (ANB Lined)			
Residual Variance	S	NS	S
Slope	NS	NS	NS
Elevation	S	NS	S
Lined - Unlined (ANT P-polymer)			
Residual Variance	S	S	S
Slope	S	S	NS
Elevation	S	S	NS
Lined - Unlined (ANB P-polymer)			
Residual variance	NS	NS	S
Slope	NS	NS	S
Elevation	S	S	S
Lined - Unlined (ANB G-polymer)			
Residual Variance	S	NS	S
Slope	NS	S	NS
Elevation	S	S	S
ANA - ANB (G - Polymer Unlined)			
Residual Variance	S	S	S
Slope	NS	NS	NS
Elevation	NS	S	S

* Close to being not significant

TABLE 3-6

ANALYSIS OF COVARIANCE COMPARISON OF REGRESSION

STRAIN DILATATION

	Dilatation at Max Strain	Poisson's Ratio
G - P (ANB Unlined)		
Residual Variance	S	S
Slope	NS	NS
Elevation	S	S
G - P (ANB Lined)		
Residual Variance	S	S
Slope	NS	NS
Elevation	NS	NS
Lined - Unlined (ANT P-polymer)		
Residual Variance	S	S
Slope	NS	NS
Elevation	NS	NS
Lined - Unlined (ANB P-polymer)		
Residual Variance	S	S
Slope	S	NS
Elevation	NS	NS
Lined - Unlined (ANB G - Polymer)		
Residual Variance	S	S
Slope	S	NS
Elevation	NS	NS
ANA - ANB (G - Polymer Unlined)		
Residual Variance	NS	NS
Slope	NS	NS
Elevation	S	S

SECTION IV
VERY LOW RATE TENSILE

This test uses a 1/2 inch thick (1.27 cm) JANNAF dogbone. The specimens are tested at a crosshead speed of 2×10^{-4} in/min (8.5×10^{-2} cm/sec) 7°F (25 °C) and ambient RH. Very low rate tensile testing is related to strain capability for storage at 60°F.

Lined cartons show a statistically significant decrease in strain at rupture except for ANB "P". Maximum stress is generally statistically increased (exception ANT "P") modulus is also significantly increased.

Unlined cartons show a statistical increase in strain at rupture, and an increase in maximum stress. In general, modulus shows a significant decrease (ANT "P" being the exception).

Lined cartons show lower standard deviations than unlined cartons.

TABLE 4-1
VERY LOW RATE TENSILE
Significance of Regression Slopes

SYSTEM	Sm	Fig er	Fig E	Fig
ANA G Unlined	Sig inc	4-1	Sig inc	4-2
ANB G Unlined	Sig inc	4-4	Sig inc	4-5
ANB G Lined	Sig inc	4-7	Sig dec	4-8
ANB P Unlined	NS		Sig inc	Sig dec
ANB P Lined	Sig inc		NS	Sig inc
ANT P Unlined	Sig inc	4-10	Sig inc	4-11
ANT P Lined	NS		Sig dec	Sig inc
ANA & ANB G Unlined	Sig inc	4-13	Sig inc	4-14
ANB G & P Unlined	Sig inc	4-16	Sig inc	4-17
ANB G & P Lined	Sig inc	4-19	Sig dec	4-20
ANB & ANT P Unlined	Sig inc		Sig inc	NS
ANB & ANT P Lined	Sig inc	4-22	Sig dec	4-23
				Sig inc 4-24

NS = Not significantly different from zero slope

Sig Inc = Positive slope

Sig Dec = Negative slope

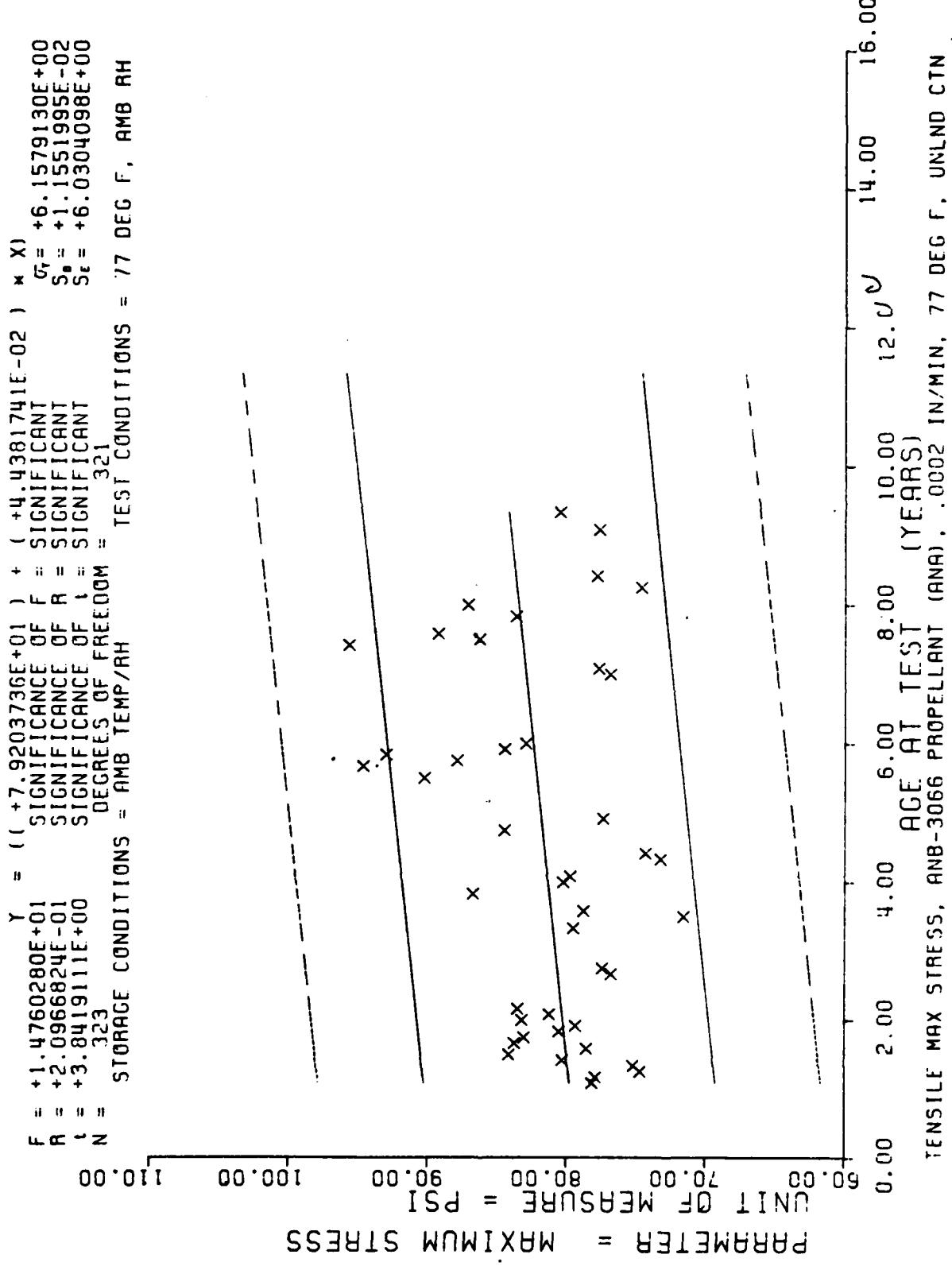


Figure 4-1

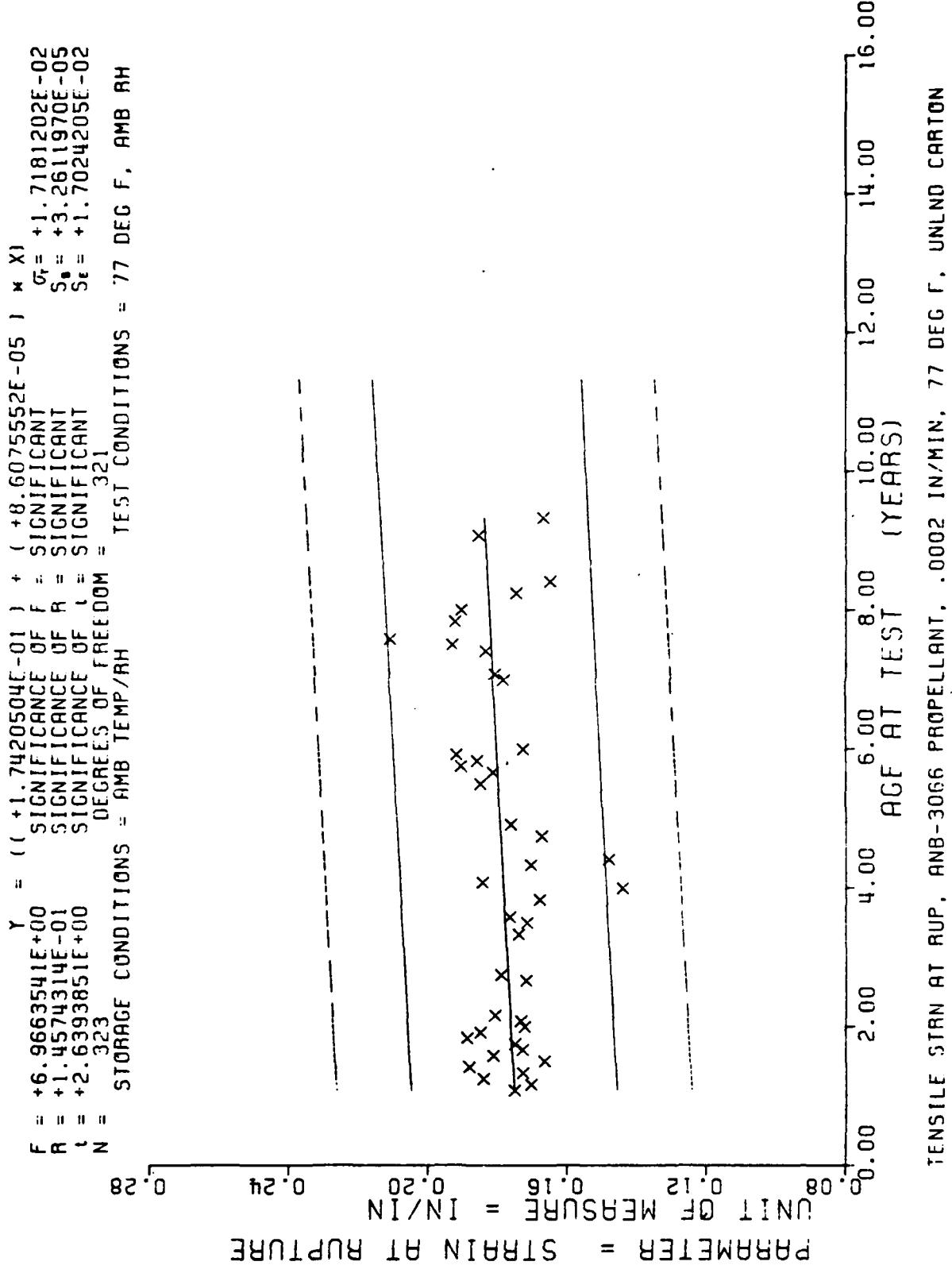
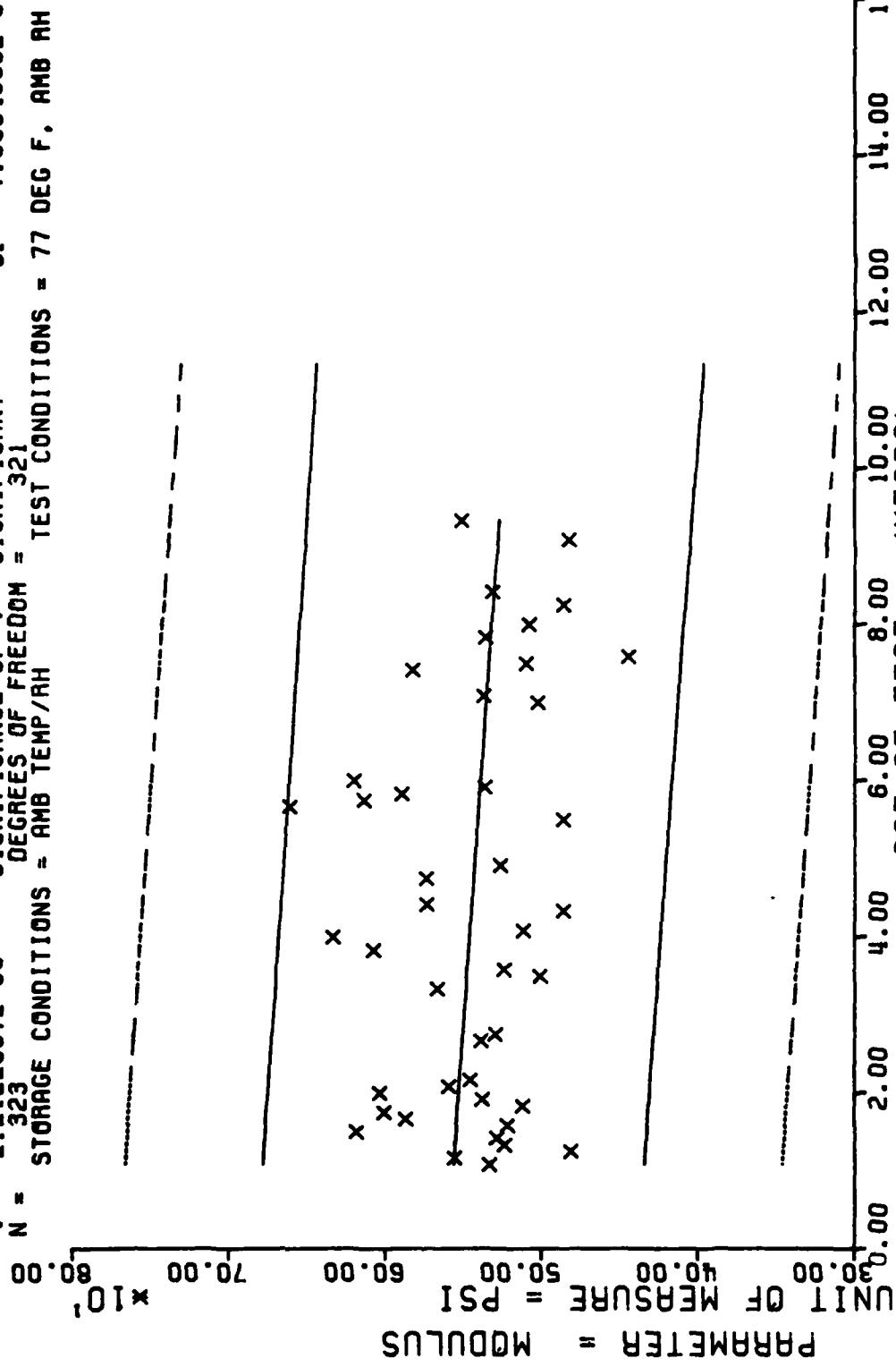


Figure 4-2

$\gamma = ((+5.6015920E+02) + (-2.9687514E-01) \times X)$
 $F = +4.8938585E+00$ SIGNIFICANCE OF $F = \text{NOT SIGNIFICANT}$
 $R = -1.2254274E-01$ SIGNIFICANCE OF $R = \text{SIGNIFICANT}$
 $t^* = +2.2122067E+00$ SIGNIFICANCE OF $t^* = \text{SIGNIFICANT}$
 $N = 323$ DEGREES OF FREEDOM = 321
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F. AMB RH



TENSILE MODULUS, ANB-3066 PROPELLANT (ANA). 0.0002 IN/MIN. 77 DEG F. UNLND CTNS

Figure 4-3

$F = +6.6169156E+00$ $\gamma = ((+7.8012291E+01) + (+1.6423942E-02) \times X)$
 $R = +6.7191999E-02$ SIGNIFICANCE OF F = SIGNIFICANT
 $t = +2.5723366E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 1461$ SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 1459
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F. AMB RH

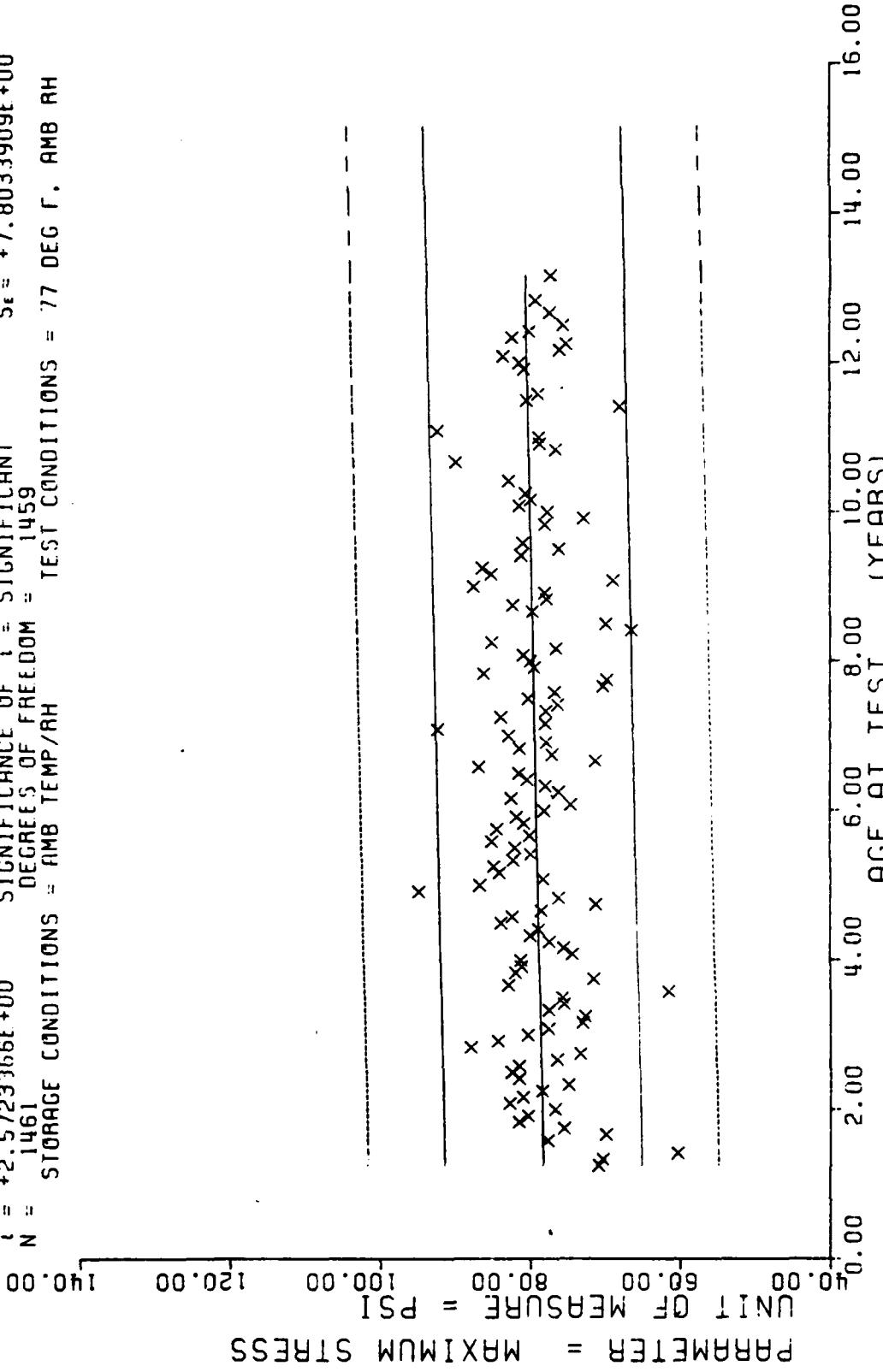


Figure 4-4

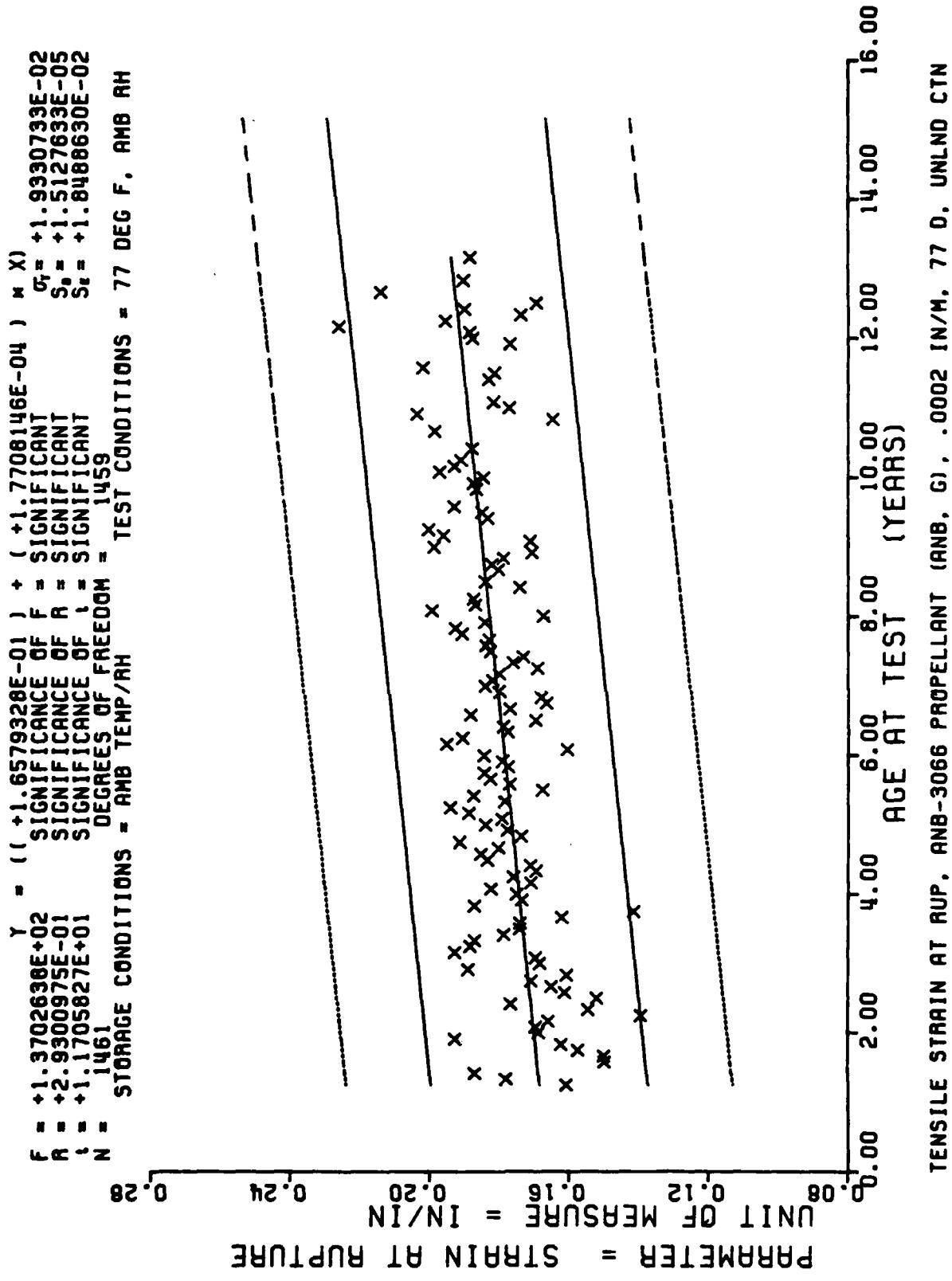


Figure 4-5

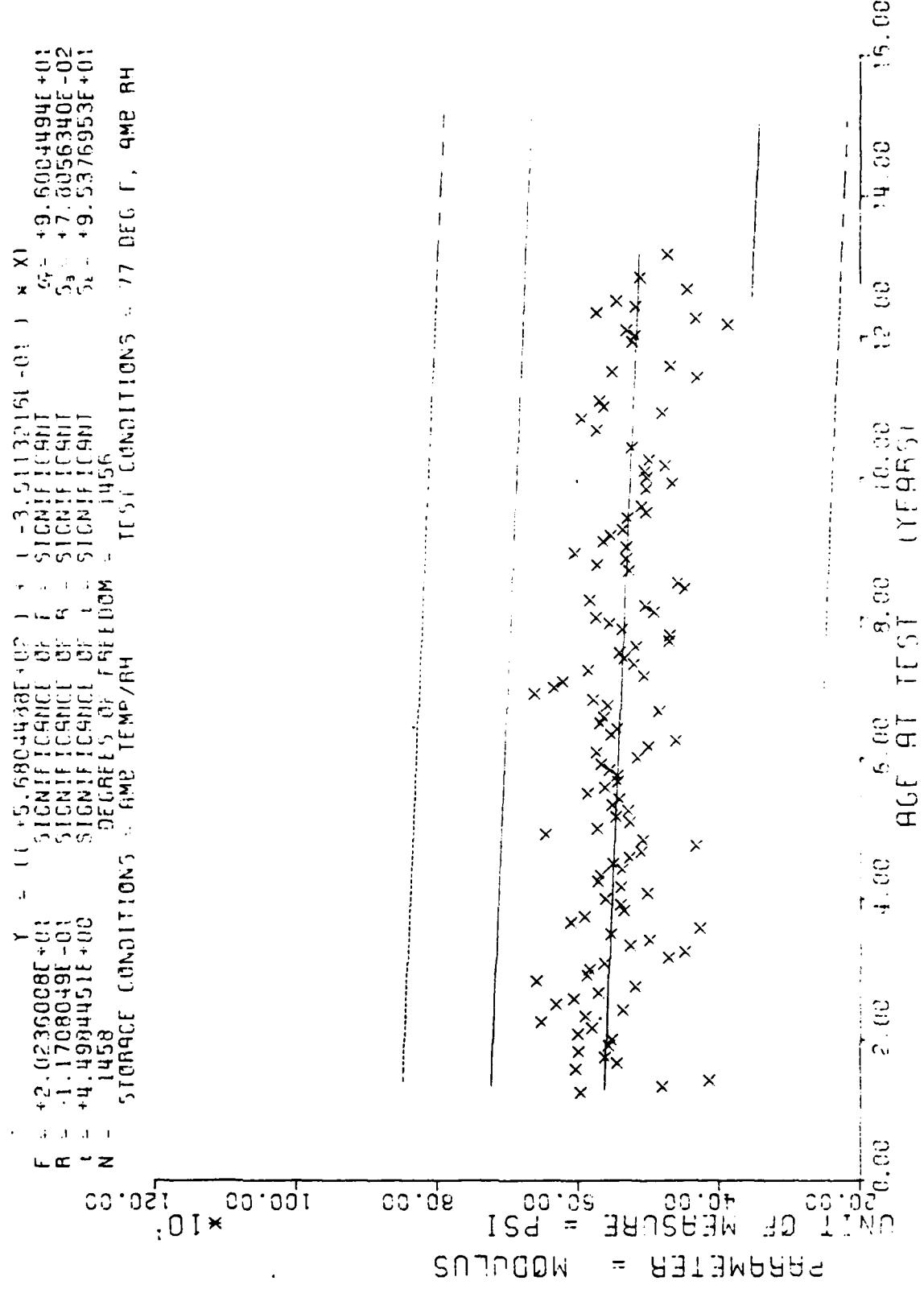


Figure 4-6

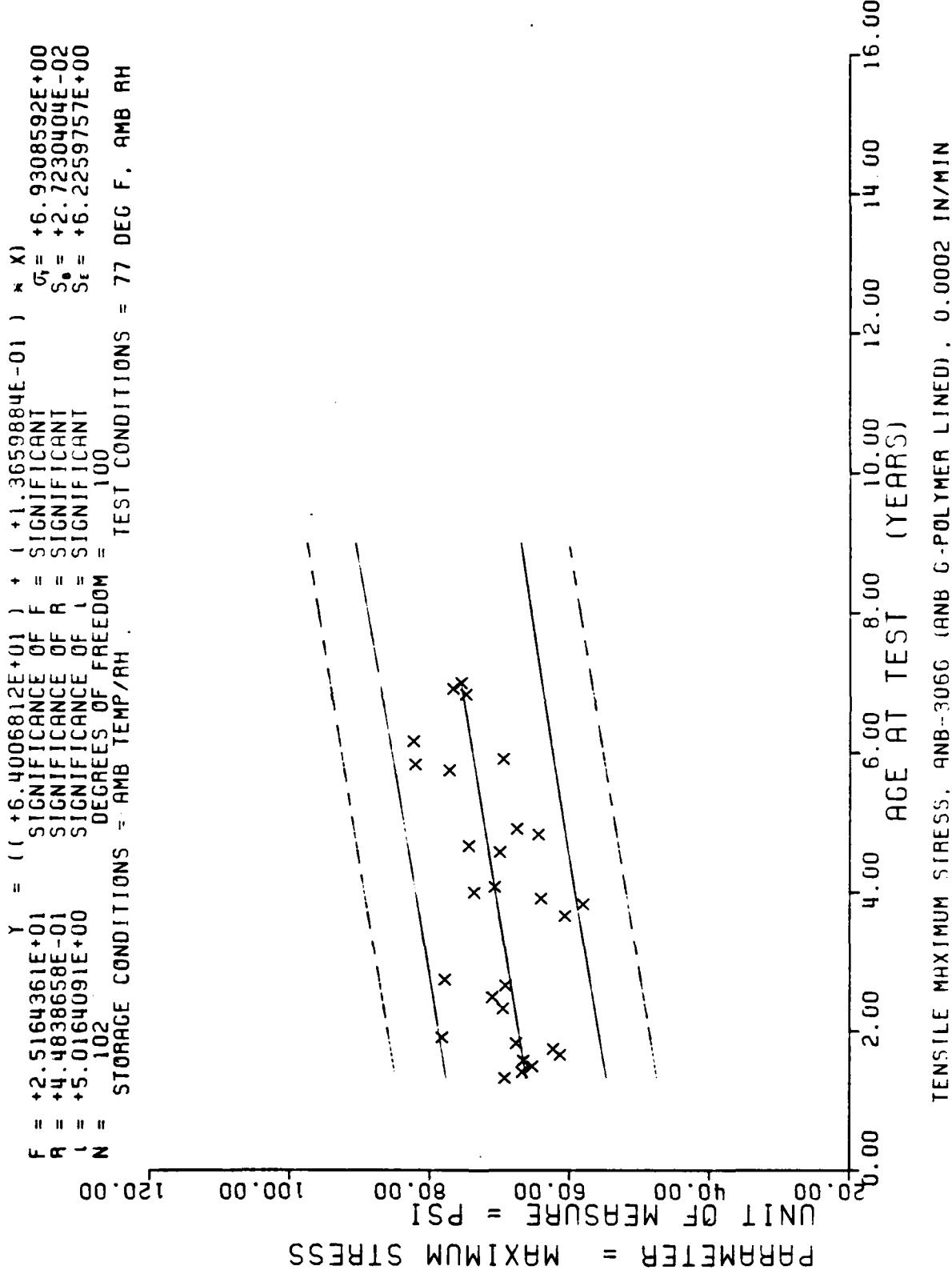


Figure 4-7

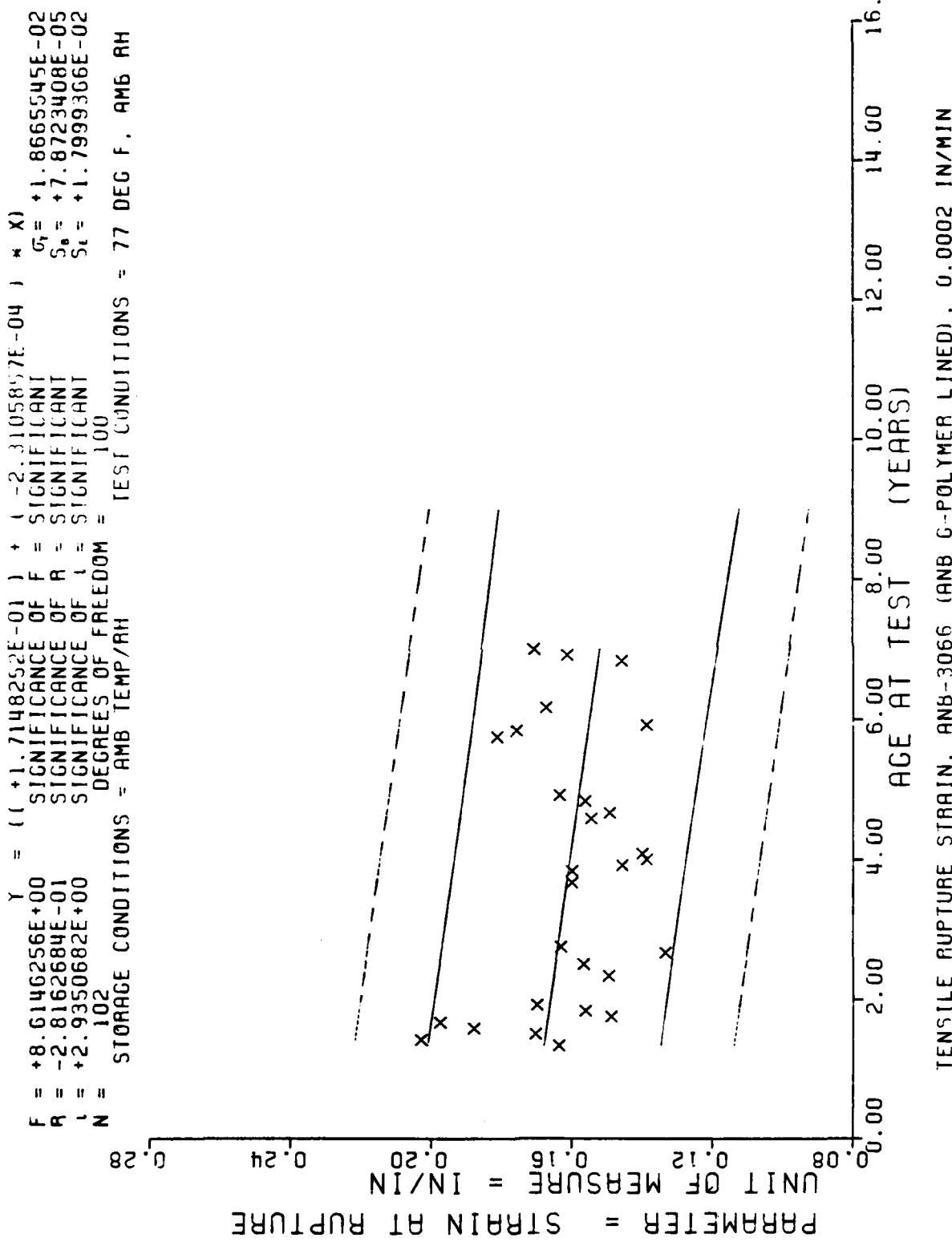


Figure 4-8

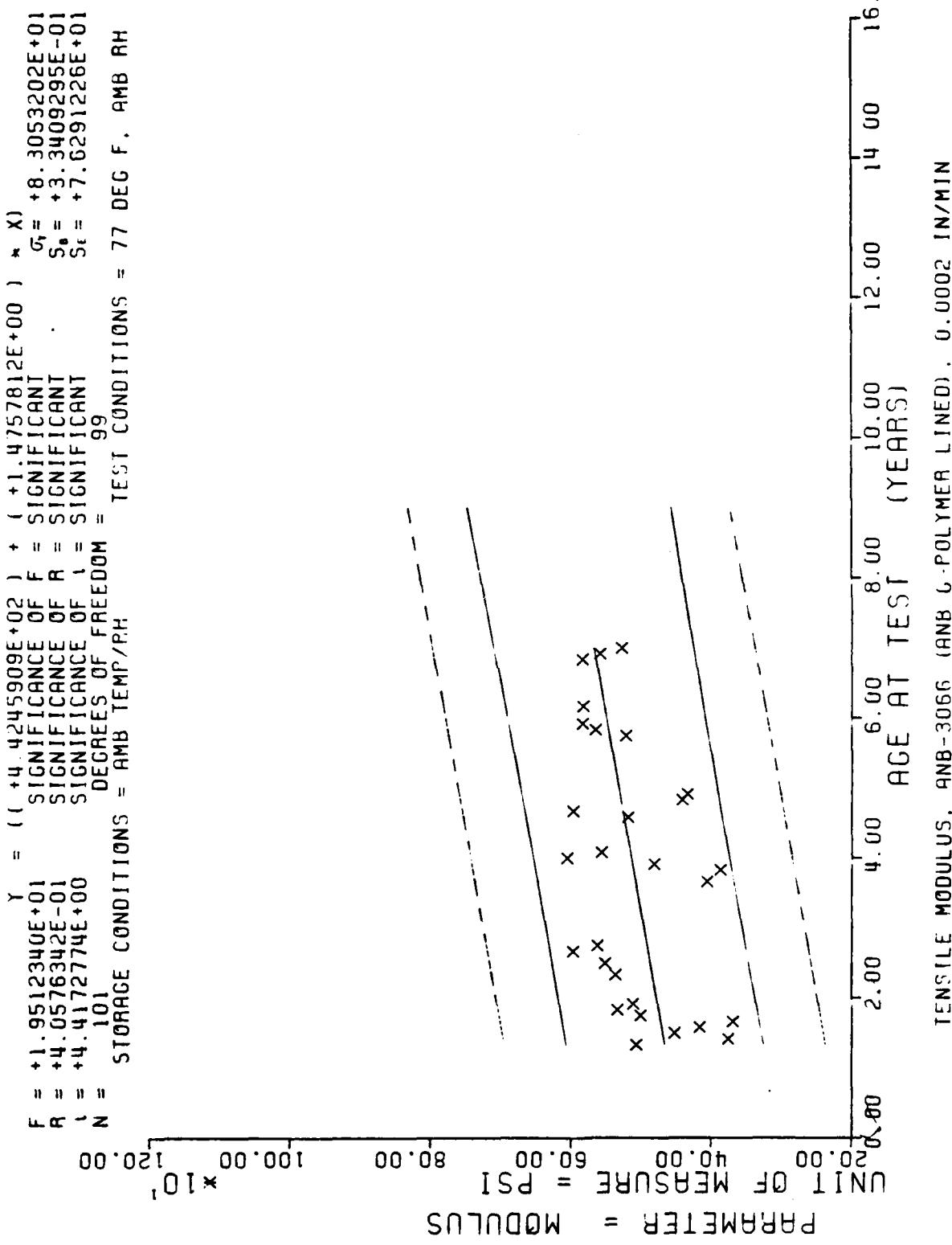


Figure 4-9

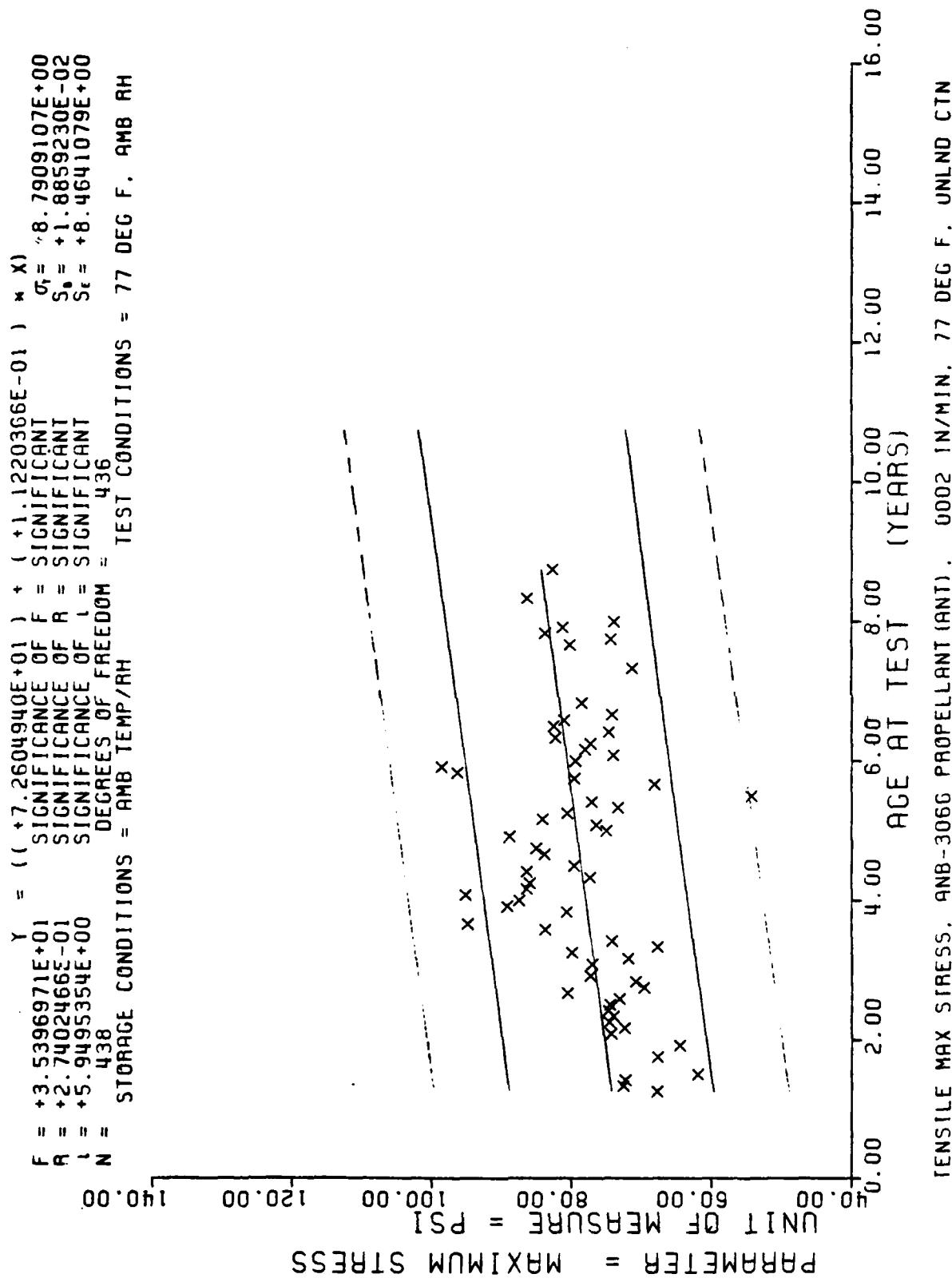


Figure 4-10

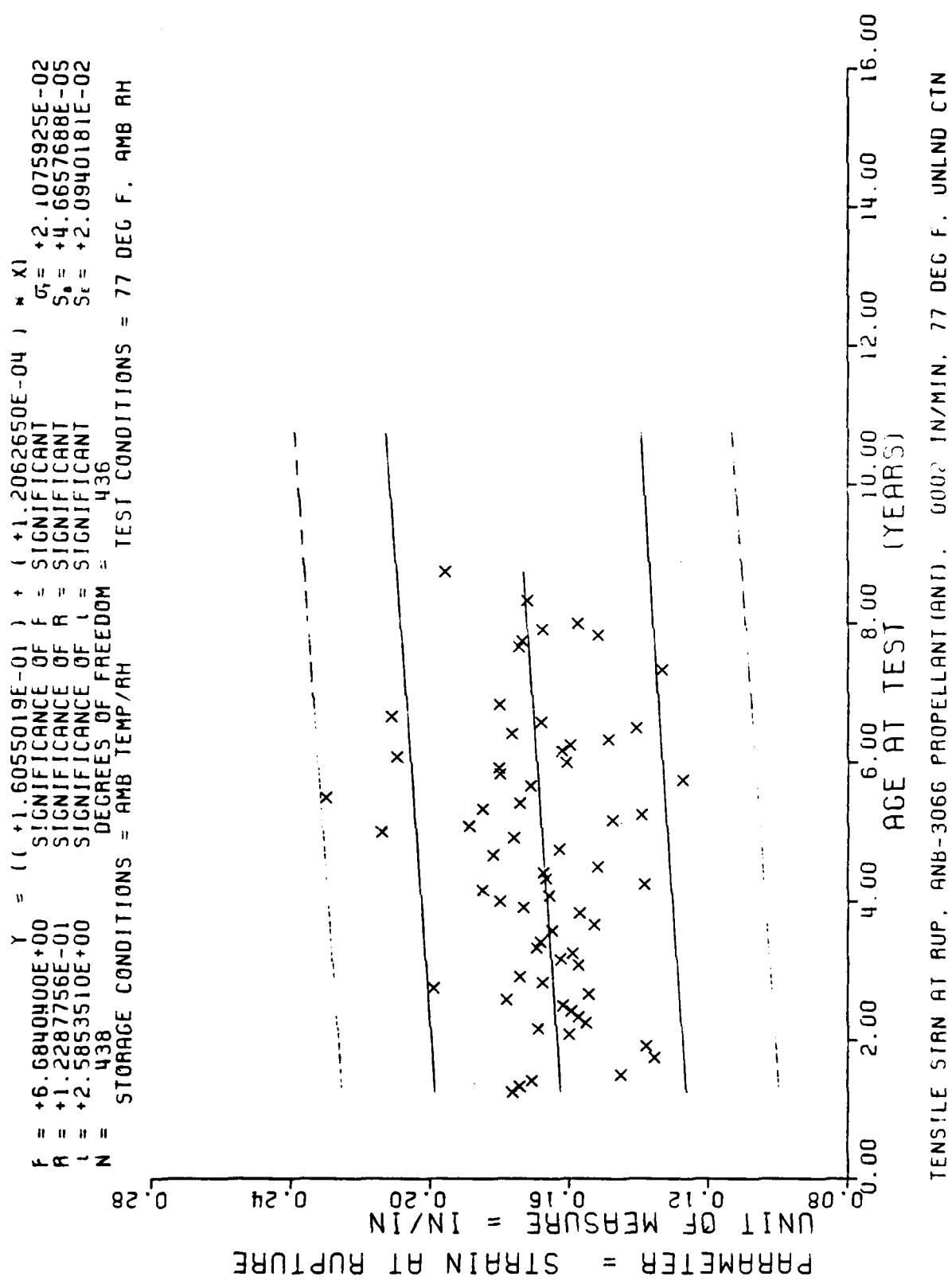


Figure 4-11

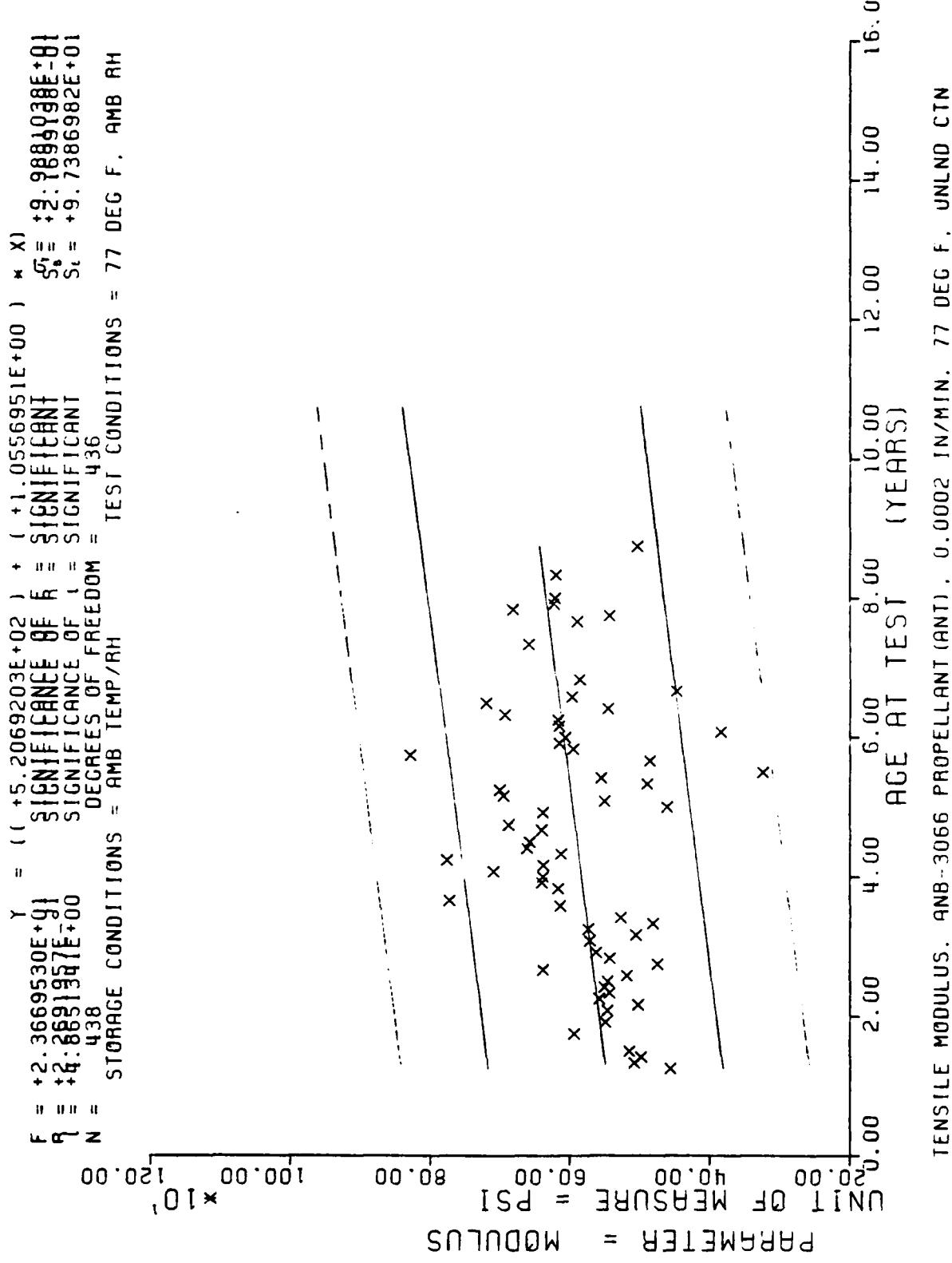


Figure 4-12

$F = +4.4758627E+00$ $\gamma = ((+7.8759763E+01) + (+1.1529107E-02) \times X_1)$
 $R = +4.9914610E-02$ SIGNIFICANCE OF F = SIGNIFICANT
 $L = +2.1156234E+00$ SIGNIFICANCE OF R = NOT SIGNIFICANT
 $N = 1794$ SIGNIFICANCE OF L = NOT SIGNIFICANT
 DEGREES OF FREEDOM = 1792
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = MAXIMUM STRESS
 NIT OF M RSURE = PSI

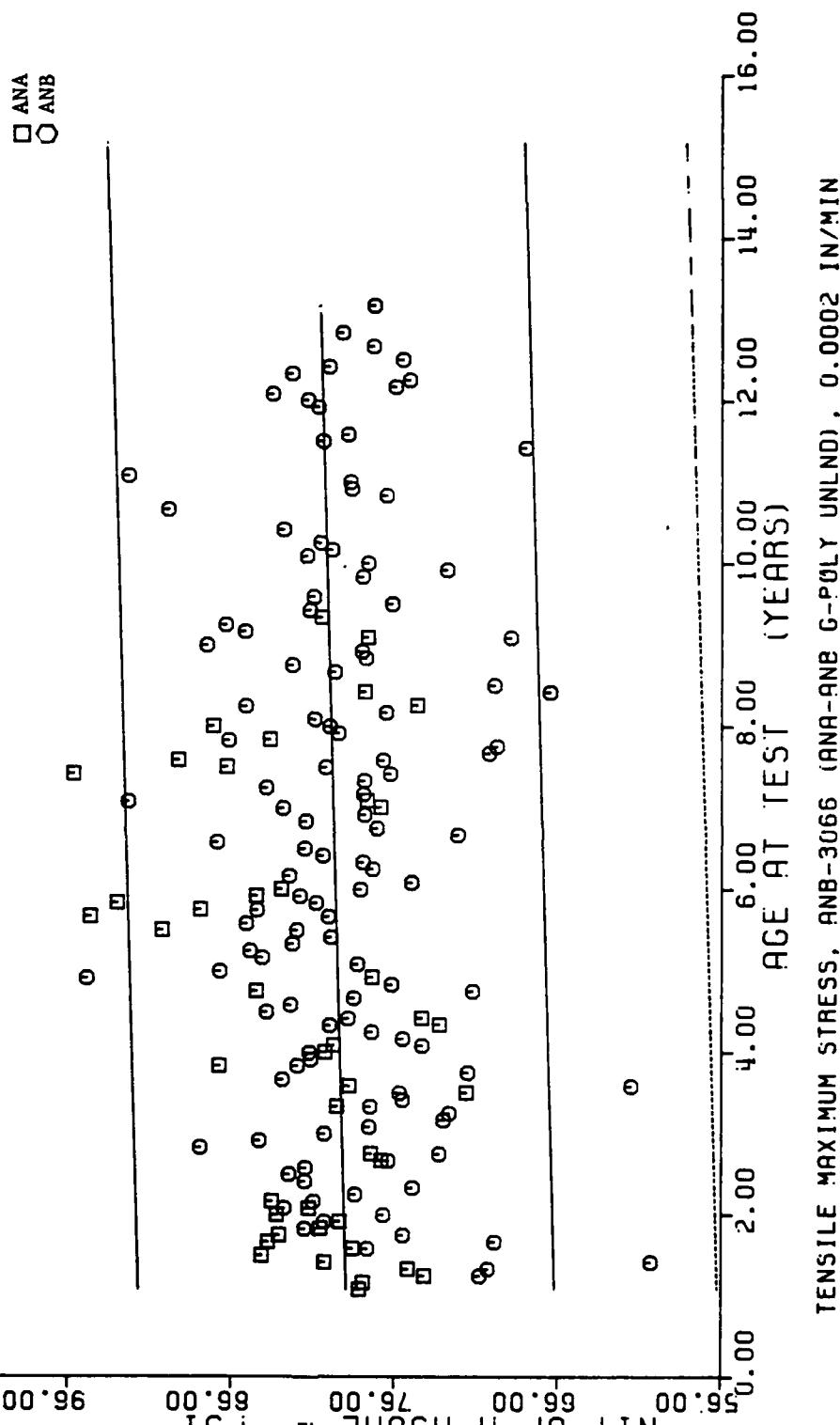


Figure 4-13

$F = +1.2740365E+02$
 $R = +2.5763673E-01$
 $t = +1.128732E+01$
 $N = 1794$
 STORAGE CONDITIONS = 8MB TEMP/RH TEST CONDITIONS = 8MB TEMP/RH
 $F = (+1.682348E-01) * X_1 + (-1.4965913E-04) * X_2$
 $R = SIGNIFICANT$
 $t = SIGNIFICANT$
 $N = SIGNIFICANT$
 $Degrees of Freedom = 1792$
 $G_t = +1.9034925E-02$
 $S_0 = +1.3259046E-05$
 $S_L = +1.8397472E-02$

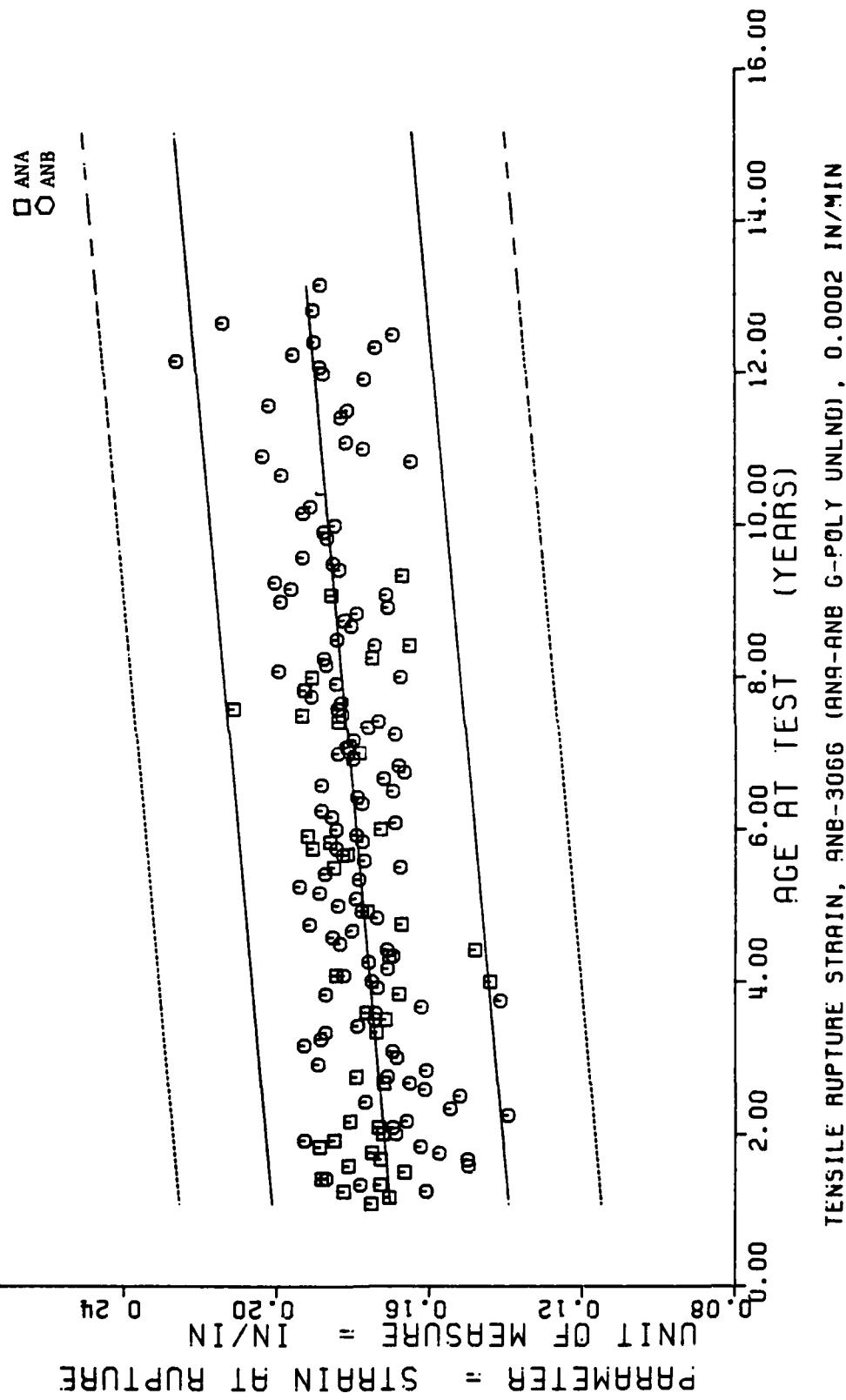


Figure 4-14

$\gamma = ((+5.6617370E+02) + (-3.3364575E-01) * X) + 9.1710133E+01$
 $F = \text{SIGNIFICANCE OF } F = \text{SIGNIFICANT}$
 $R = \text{SIGNIFICANCE OF } R = \text{SIGNIFICANT}$
 $R^2 = \text{SIGNIFICANCE OF } R^2 = \text{SIGNIFICANT}$
 $N = \text{DEGREES OF FREEDOM} = 1789$
 $T = \text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$

ANA
 ANB

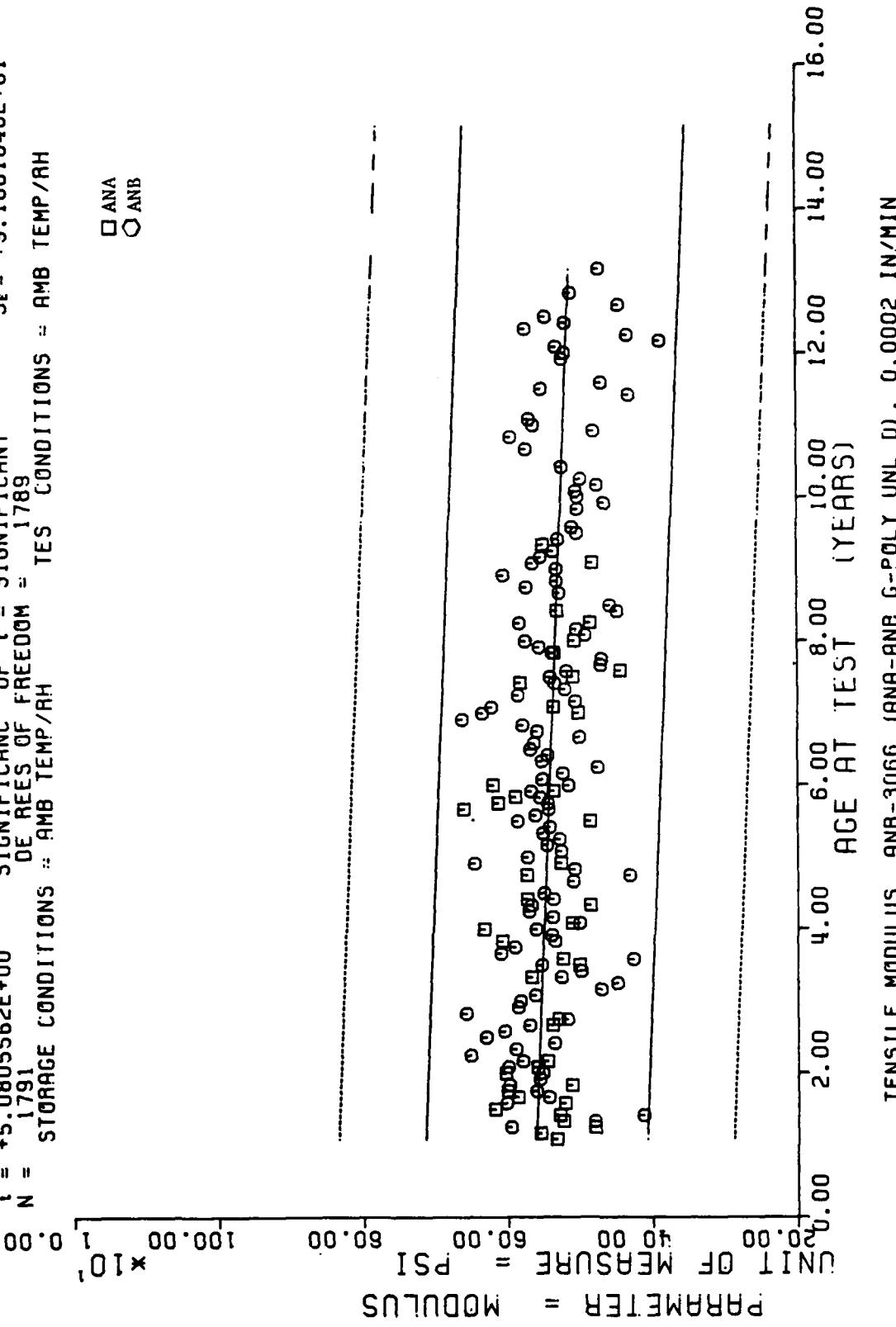


Figure 4-15

$\gamma = ((+7.965352 \times 10^1) + (+1.0922182 \times 10^{-2}) \times X)$
 $F = 5.5715634E+00$ SIGNIFICANCE OF F = SIGNIFICANT
 $F_9 = +4.4428951 -02$ SIGNIFICANCE OF R = SIGNIFICANT
 $F_{17} = +2.3604159E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $N = 2819$ DEGREE OF FREEDOM = 2817
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

Δ ANBG
 X ANBP

UNIT OF MEASURE = PSI
 PARAMETER = MAXIMUM STRESS

4 - 18

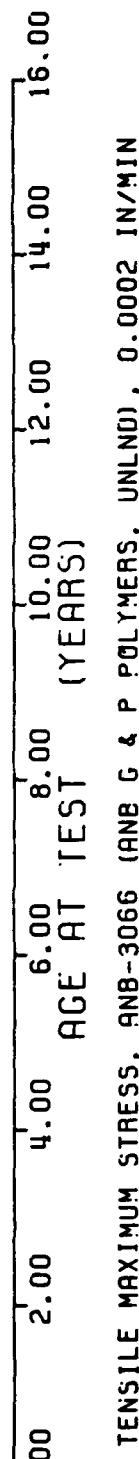


Figure 4-16

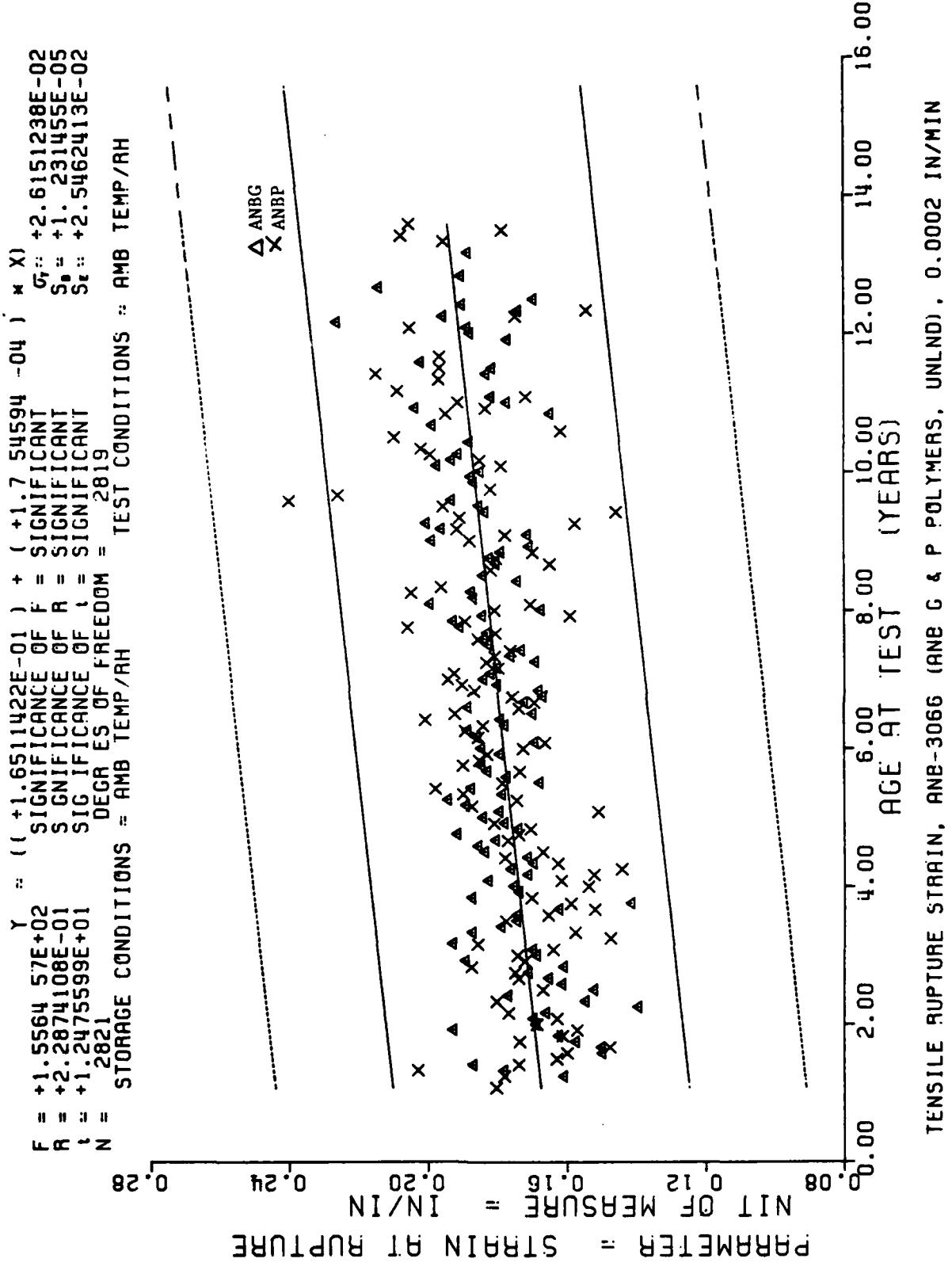
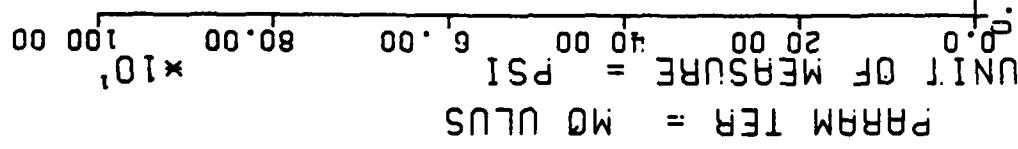


Figure 4-17

$F = +2.3674 \cdot 98E+01$ $Y = ((+5.814 \cdot 159E+02) + (-3.1655885E-01) \times X)$
 $R = -9.132 \cdot 084E-02$ SIGNIFICANCE OF F = SIGNIFICANT
 $I = +4.8656755E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 2817$ SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = 2 15
 STORAGE CONDITIONS = AMB TEMP/RH

TEST CONDITIONS = AMB TEMP/RH

Δ ANBG
 \times ANBP



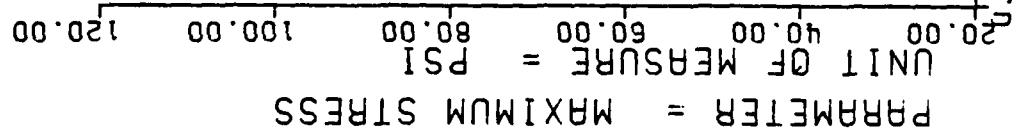
TENSIL MODULUS, ANB-3066 (ANBG & P POLYMERS, UNLND), 0.0002 IN/MIN

Figure 4-18

$F = +7.5799236E+01$ $\gamma = ((+6.3019516E+01) + (+1.5164381E-01) * X)$
 $R = +4.7300006E-01$ SIGNIFICANT OF F = $\sigma_t = +7.1383074E+00$
 $I = +8.7062757E+00$ SIGNIFICANT OF R = $S_o = +1.7417759E-02$
 $N = 265$ SIGNIFICANT OF I = $S_e = +6.3012396E+00$
DEGREES OF FREEDOM = 263 TEST CONDITIONS = AMB TEMP/RH

STORAGE CONDITIONS = AMB TEMP/RH

Δ ANB C
 X ANB P



TENSILE MAXIMUM STRESS, QNB-3066 (ANB C & P POLYMERS LINEU), 0.0002 IN/MIN

Figure 4-19

$F = +1.0468068E+01$ $\gamma = ((+1.7193540E-01) + (-1.6597231E-04) \times X)$
 $R = -1.9565004E-01$ $S_f = \text{SIGNIFICANT}$
 $R = +3.2354393E+00$ $S_o = \text{SIGNIFICANT}$
 $N = 265$ $S_t = \text{SIGNIFICANT}$
 $N = 265$ $\text{DEGREES OF FREEDOM} = 263$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$ $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

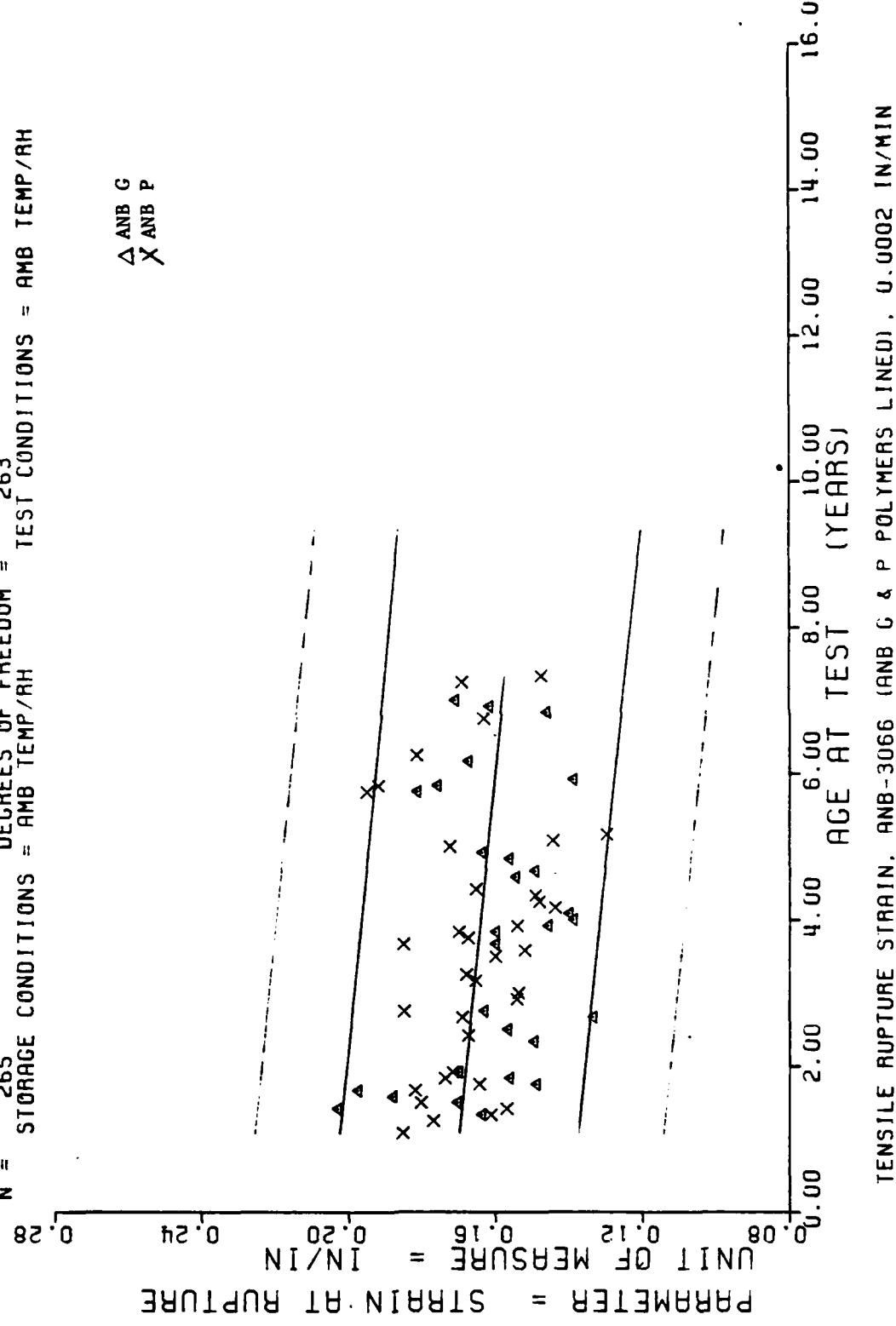


Figure 4-20

$F = +3.5595194E+01$
 $R = +3.4938600E-01$
 $N = +5.9661708E+00$
 $N = 258$
 $F = 11.3931214E+02$
 $R = 1.3056240E+00$
 $N = 1.3788591E+01$
 $S_f = +2.1883785E-01$
 $S_e = +7.8661326E+01$
 $F = \text{SIGNIFICANCE OF F}$
 $R = \text{SIGNIFICANCE OF R}$
 $N = \text{DEGREES OF FREEDOM} = 256$
 $F = \text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

Δ ANB G
 \times ANB P

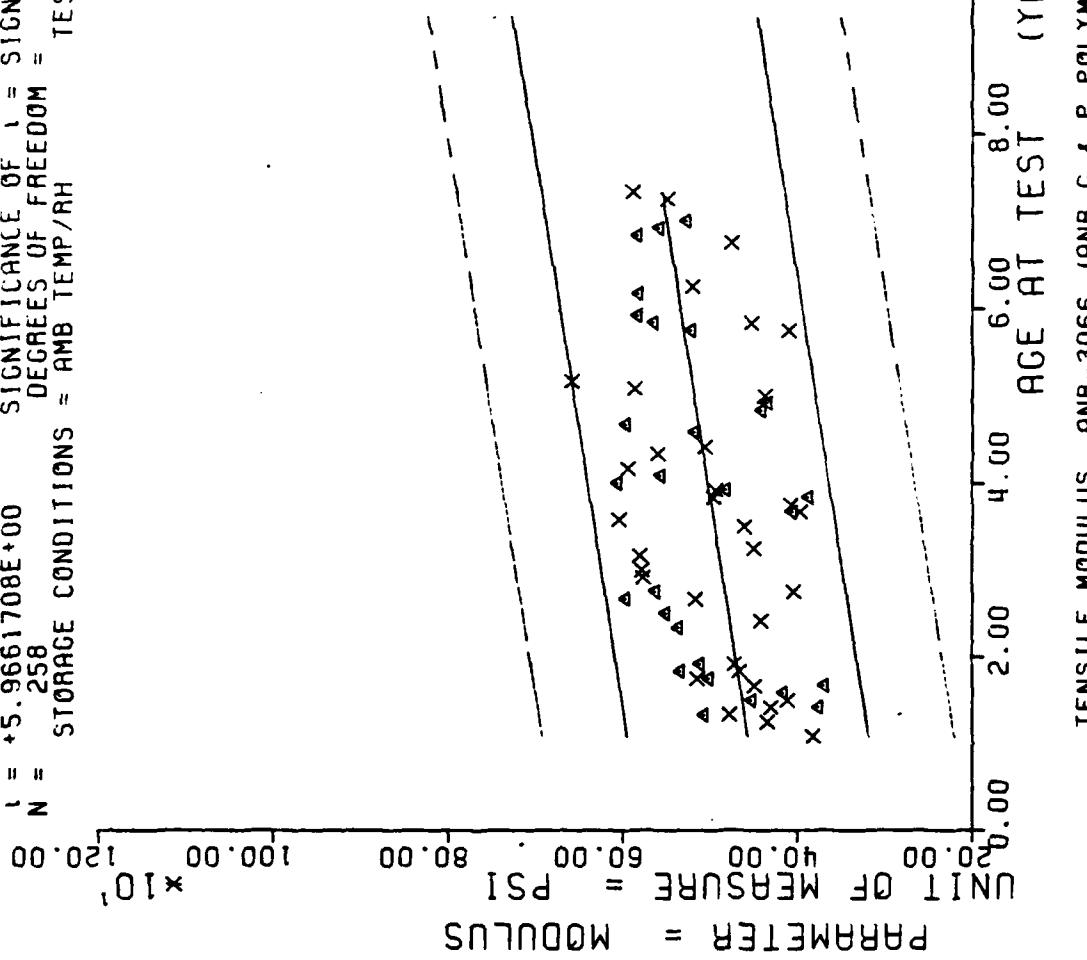


Figure 4-21

$F = +2.2839413E+01$ $\gamma = ((+6.6091970E+01) + (+9078379E-02) * X) * X$
 $R = +2.2582983E-01$ $F = \text{SIGNIFICANT}$
 $L = +4.7790598E+00$ $R = \text{SIGNIFICANT}$
 $N = 427$ $L = \text{SIGNIFICANT}$
 $\text{STORAGE CONDITIONS} = \text{AMBIENT TEMP/RH}$ $\text{DEGREES OF FREEDOM} = 425$
 $\text{TEST CONDITIONS} = \text{AMBIENT TEMP/RH}$

PARAMETER = MAXIMUM STRESS
 UNIT OF MEASURE = PSI
 0.00 2.00 4.00 6.00 8.00 10.00 12.00 14.00 16.00

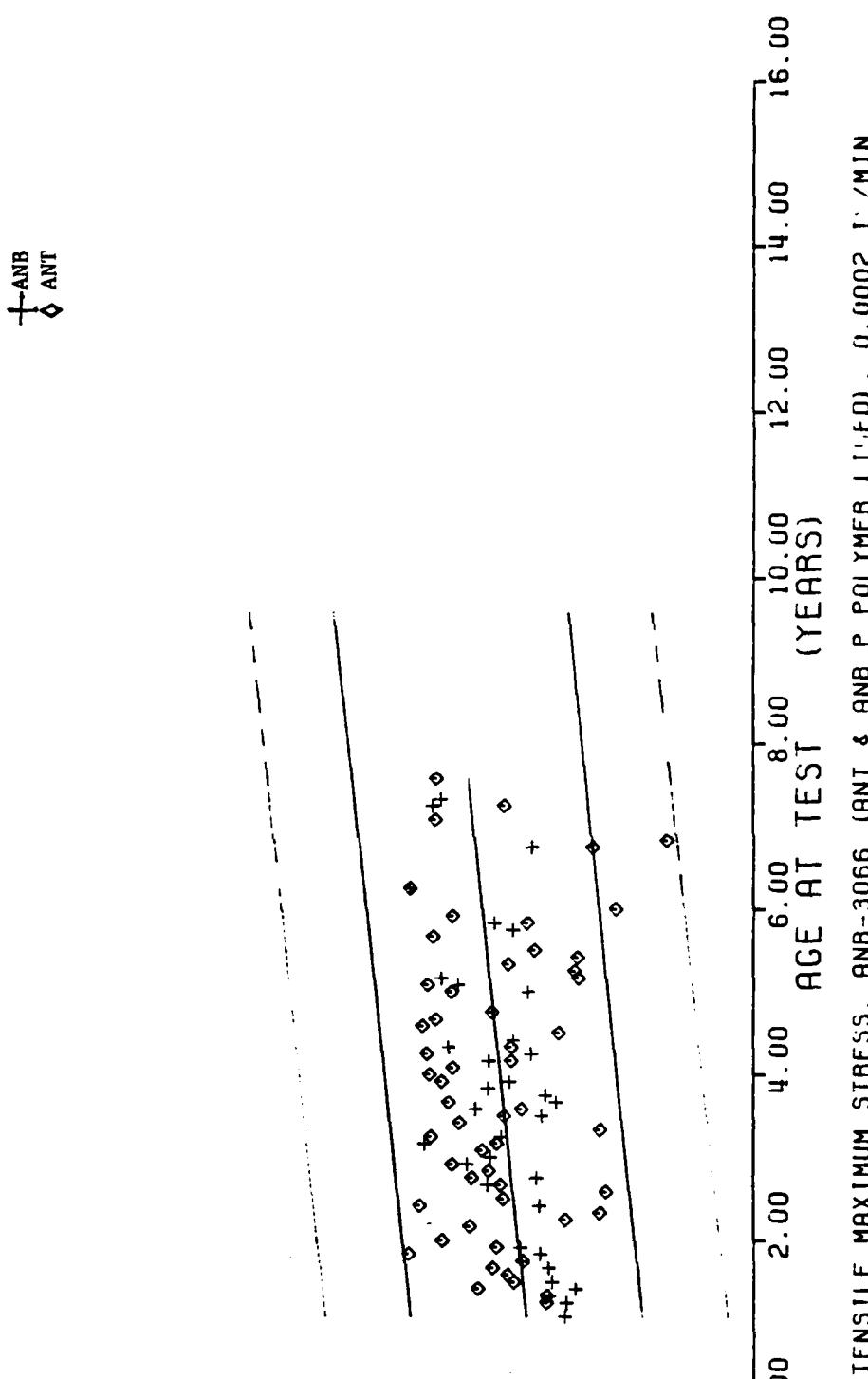


Figure 4-22

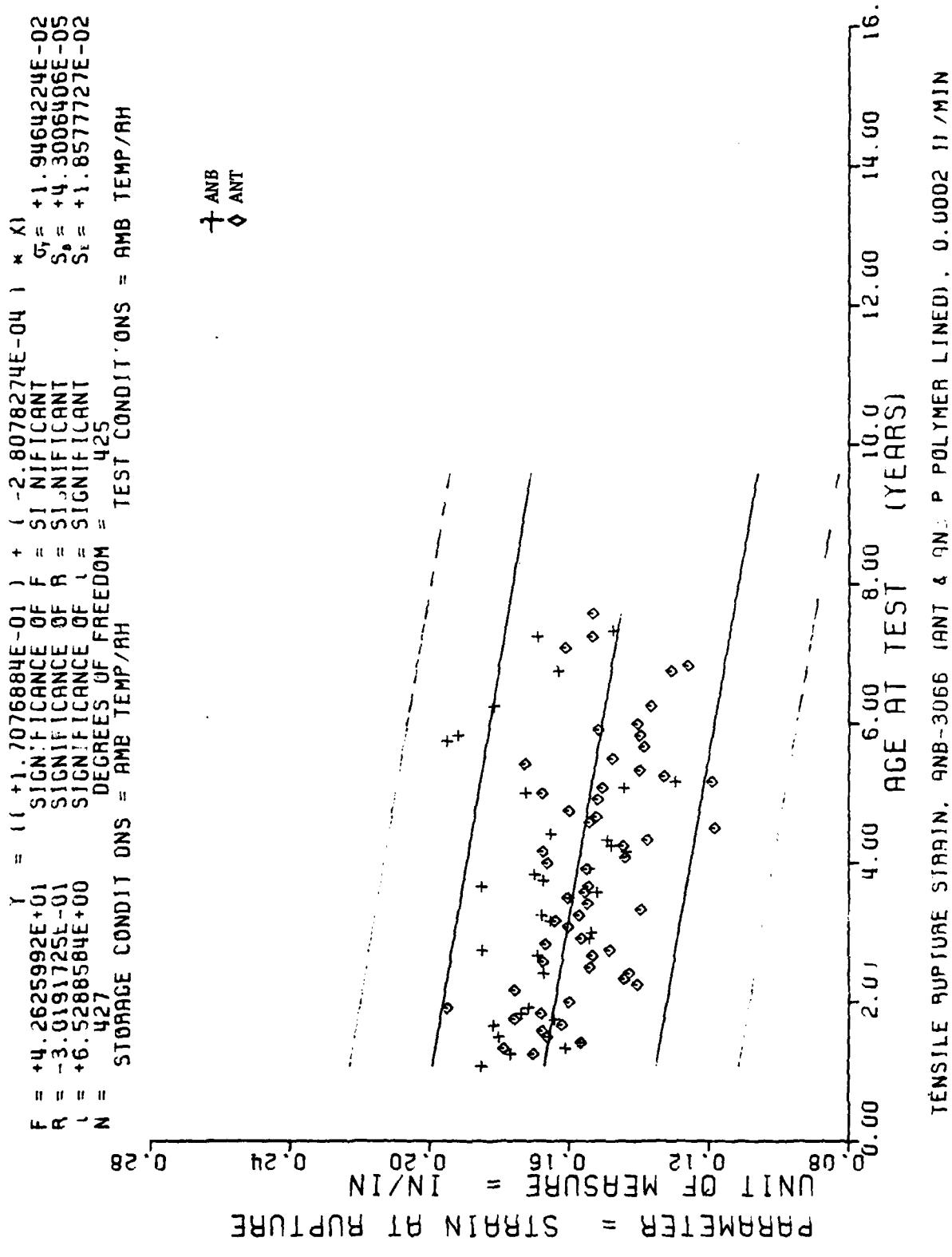


Figure 4-23

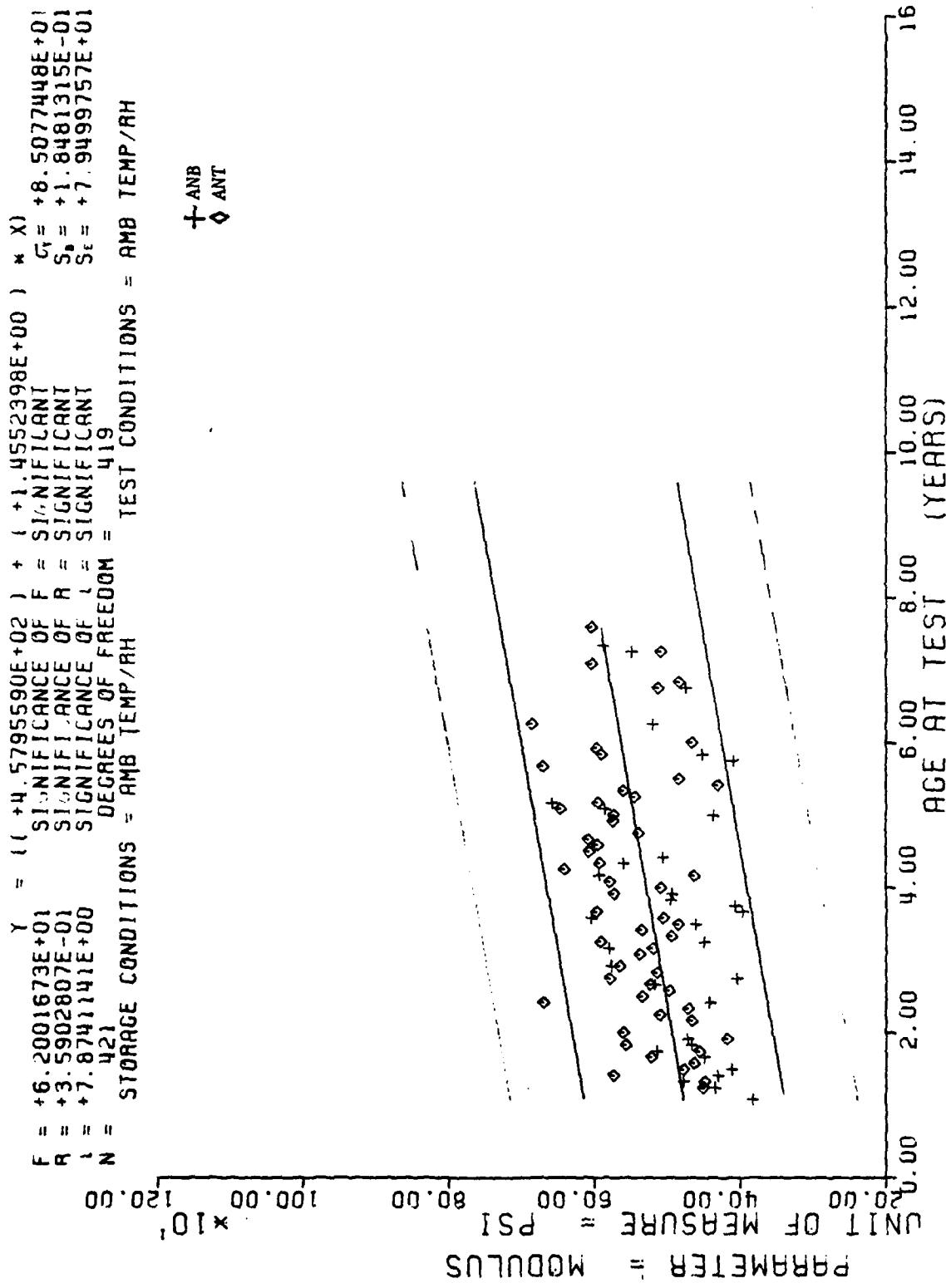


Figure 4-24

SECTION V

HIGH RATE TENSILE

A. HIGH RATE TRIAXIAL:

This test utilizes a specimen 3/4 inch (1.9 cm) GL rail by 5 inches (12.7 cm) long. The specimens are tested on the MTS at a crosshead speed of 1750 in/min (74.08 cm/sec) with 600 psi (42.18 kg/sq cm). Strain rate is 1000 in/in/min. These conditions simulate that of the motor at ignition.

There are fewer significant trends than in the last report. Lined cartons of ANB"G" and ANT"P" propellant show significant trends for all parameters but in opposing directions (Table 5-1).

The most consistent statistical feature of the test is the lower standard deviation of lined cartons compared to unlined cartons (Table 2-1). This characteristic is most noticeable in the standard deviation of modulus which may be less than half that of unlined cartons. Since determination of a consistent modulus has been a problem in high rate testing, the much reduced deviation in lined cartons seems all the more remarkable.

B. HIGH RATE DOGBONES:

This test is performed under the same conditions as the rail specimens. The specimens are shortened dogbones with a nominal gage length of 0.75".

All systems show a significant increase in maximum stress. Modulus shows a significant increase except for ANB"P" lined cartons. Only ANT P and ANB G lined cartons do not show a significant decrease in strain and rupture (Table 5-2).

TABLE 5-1
HIGH RATE TRIAXIAL
Significance Of Regression Slopes

SYSTEM	Sm	Fig	er	Fig	E	Fig
ANA G Unlined	NS		Sig inc		Sig dec	
ANB G Unlined	NS		Sig inc		Sig dec	
ANB G Lined	Sig dec	5-1	Sig inc	5-2	Sig dec	5-3
ANB P Unlined	NS		NS		Sig dec	
ANB P Lined	NS		NS		NS	
ANT P Unlined	Sig inc		NS		NS	
ANT P Lined	Sig inc	5-4	Sig dec	5-5	Sig inc	5-6
ANA & ANB G Unlined	NS		Sig Inc		Sig dec	
ANB G&P Unlined	Sig inc	5-7	Sig inc	5-8	Sig dec	5-9
ANB G&P Lined	NS		NS		NS	
ANT & ANB P Unlined	NS		Sig dec		NS	
ANT & ANB P LINED	Sig inc	5-10	Sig dec	5-11	Sig inc	5-12

TABLE 5-2
HIGH RATE DOGBONES
Significance of Regression Slopes

SYSTEM	sm	Fig	er	Fig	E	Fig
ANA G Unlined no data						
ANB G Unlined	Sig inc	5-13	Sig dec	5-14	Sig inc	5-15
ANB G Lined	Sig inc		NS		Sig inc	
ANB P Unlined	Sig inc	5-6	Sig dec	5-17	Sig inc	5-18
ANB P Lined	Sig inc		Sig dec		NS	
ANT P Unlined	Sig inc		NS		Sig inc	
ANT P Lined	Sig inc	5-19	Sig dec	5-20	Sig inc	5-21

NS = Not significantly different from zero slope
 Sig inc = Positive slope
 Sig dec = Negative slope

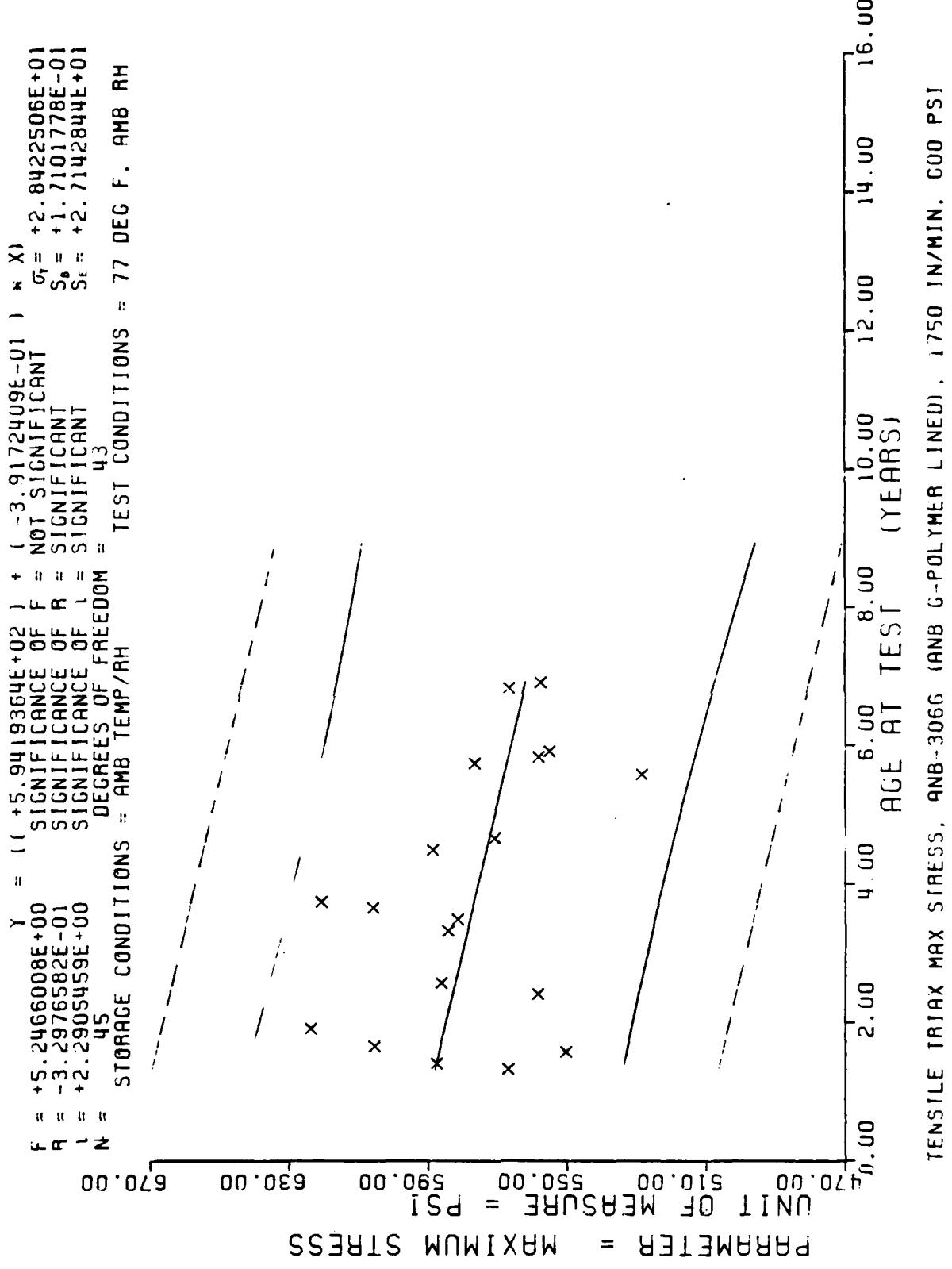


Figure 5-1

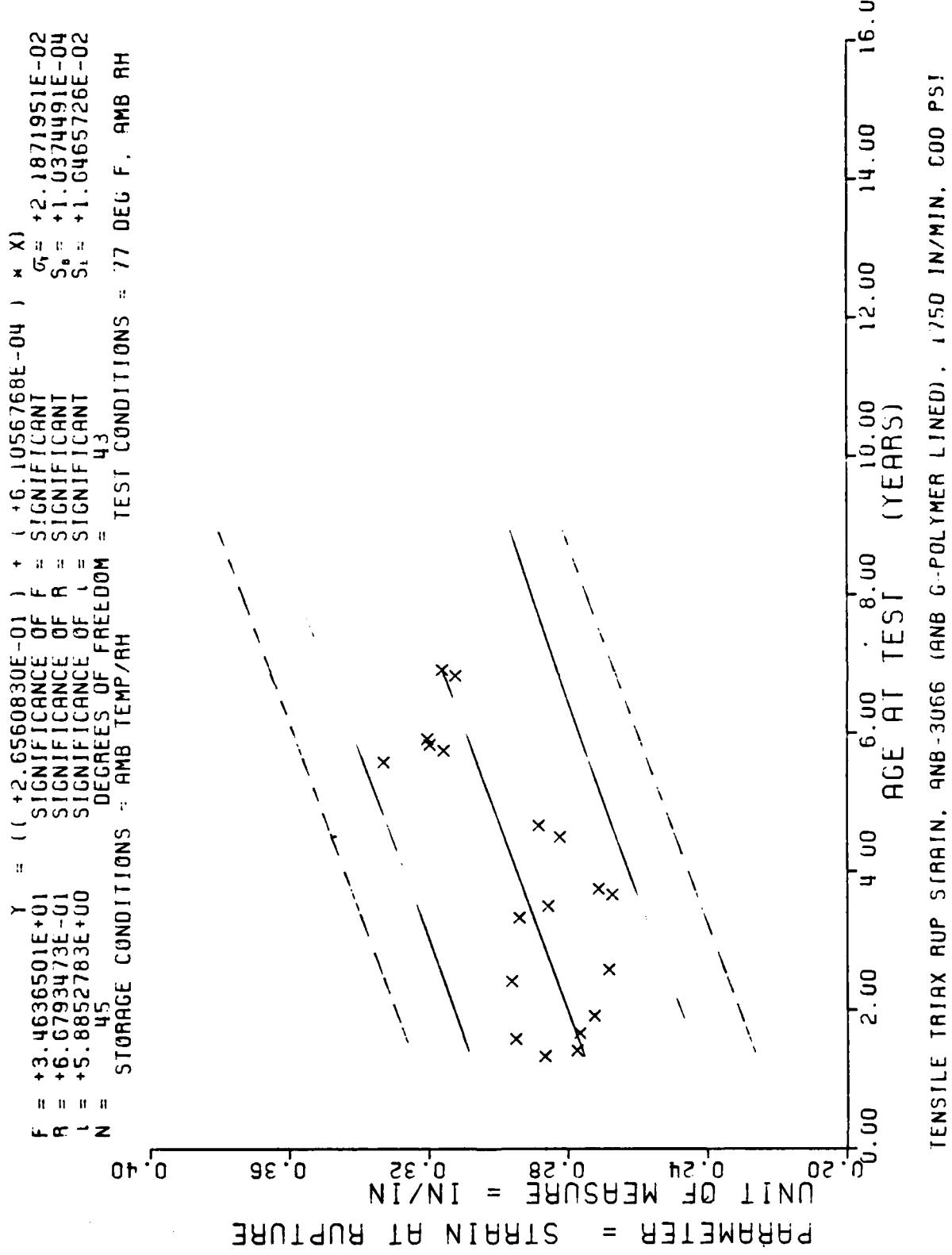


Figure 5-2

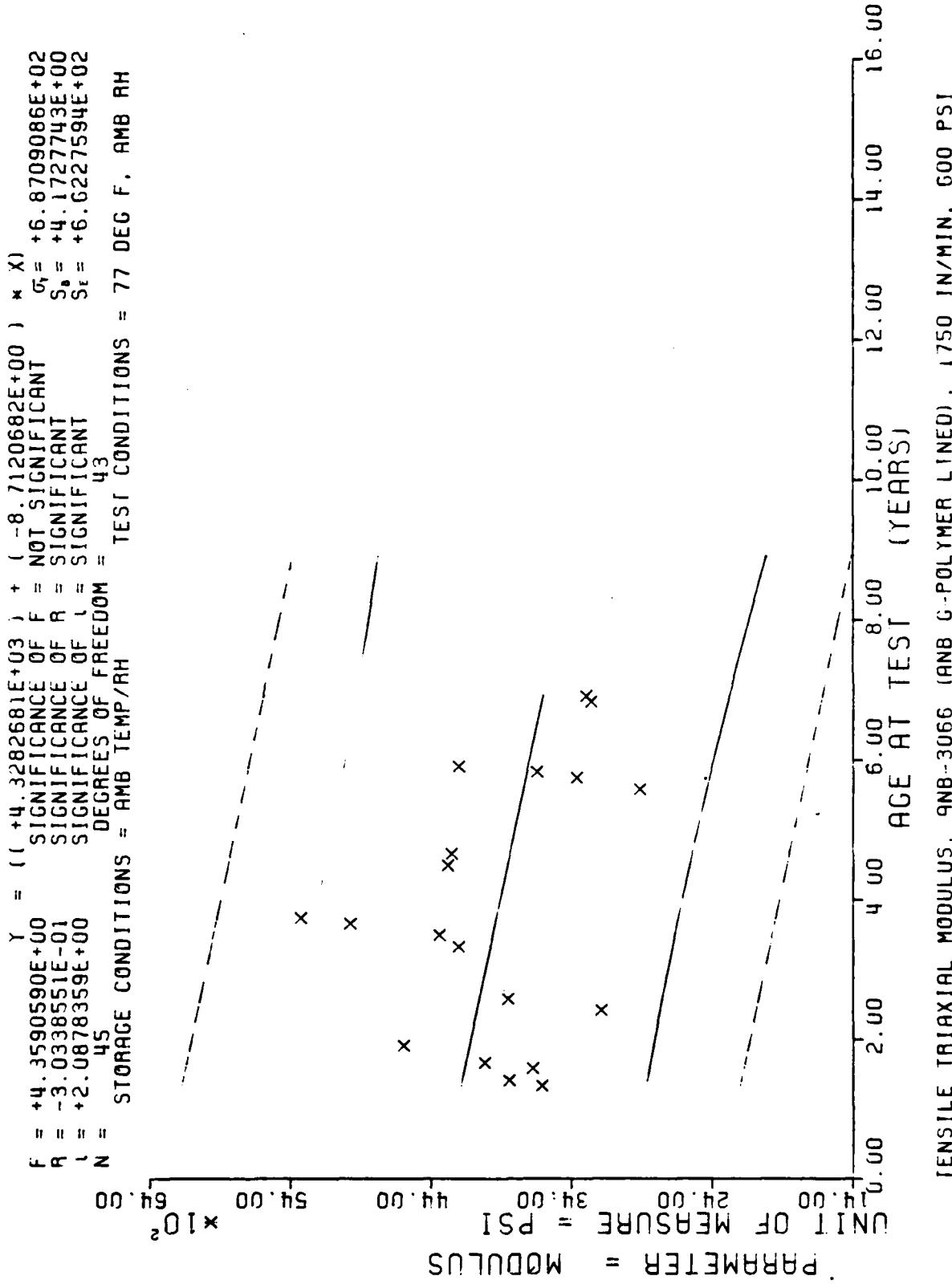


Figure 5-3

F = +2.7188346E+01 Y = ((+5.7184724E+02) + (+6.5205148E-01) * X)
 R₁ = +3.9969295E-01 SIGNIFICANCE OF F = SIGNIFICANT
 R₂ = +5.2142446E+00 SIGNIFICANCE OF R = SIGNIFICANT
 N = 145 DEGREES OF FREEDOM = 143
 TEST CONDITIONS = AMB TEMP/RH STORAG CONDITIONS = AMB TEMP/RH

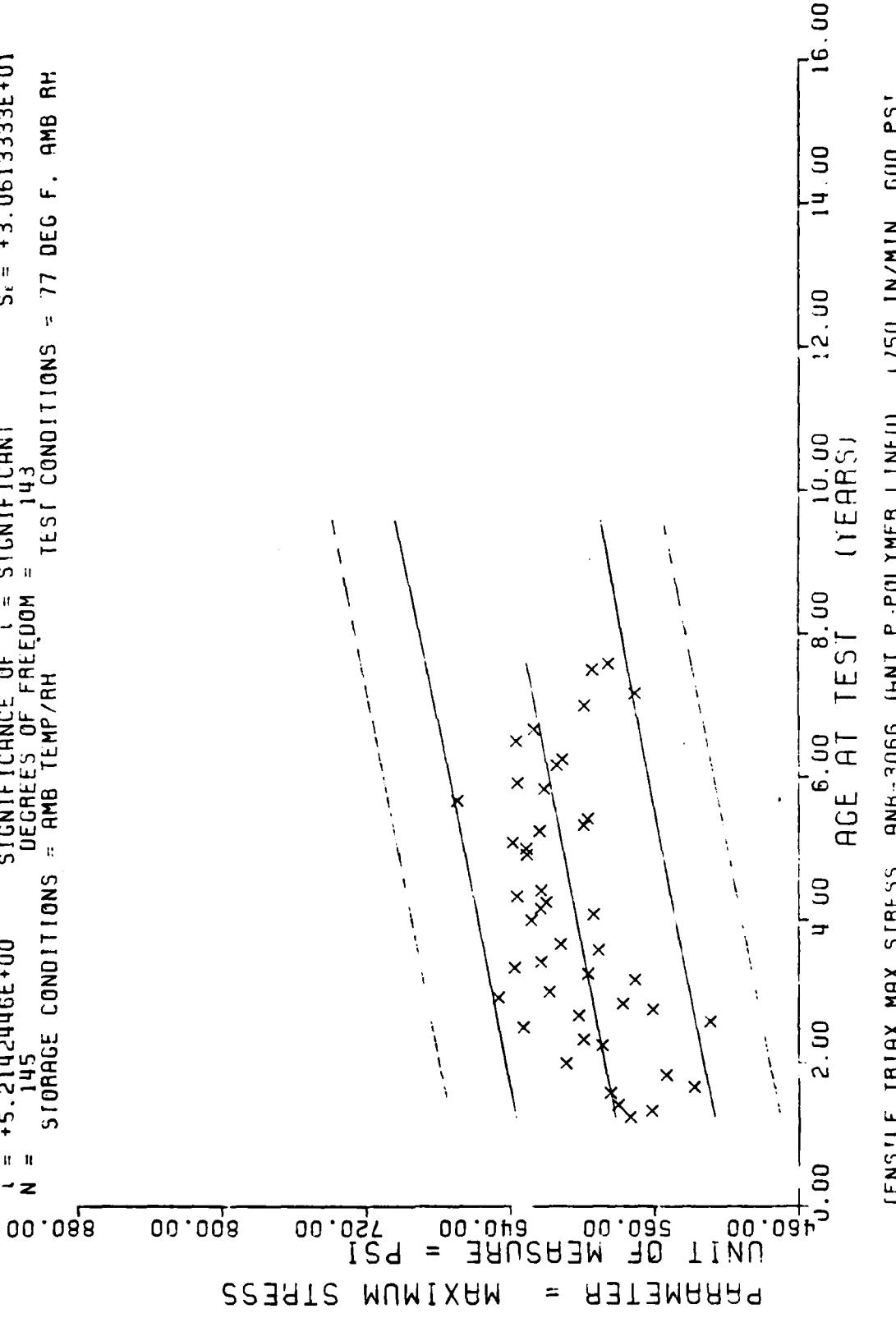


Figure 5-4

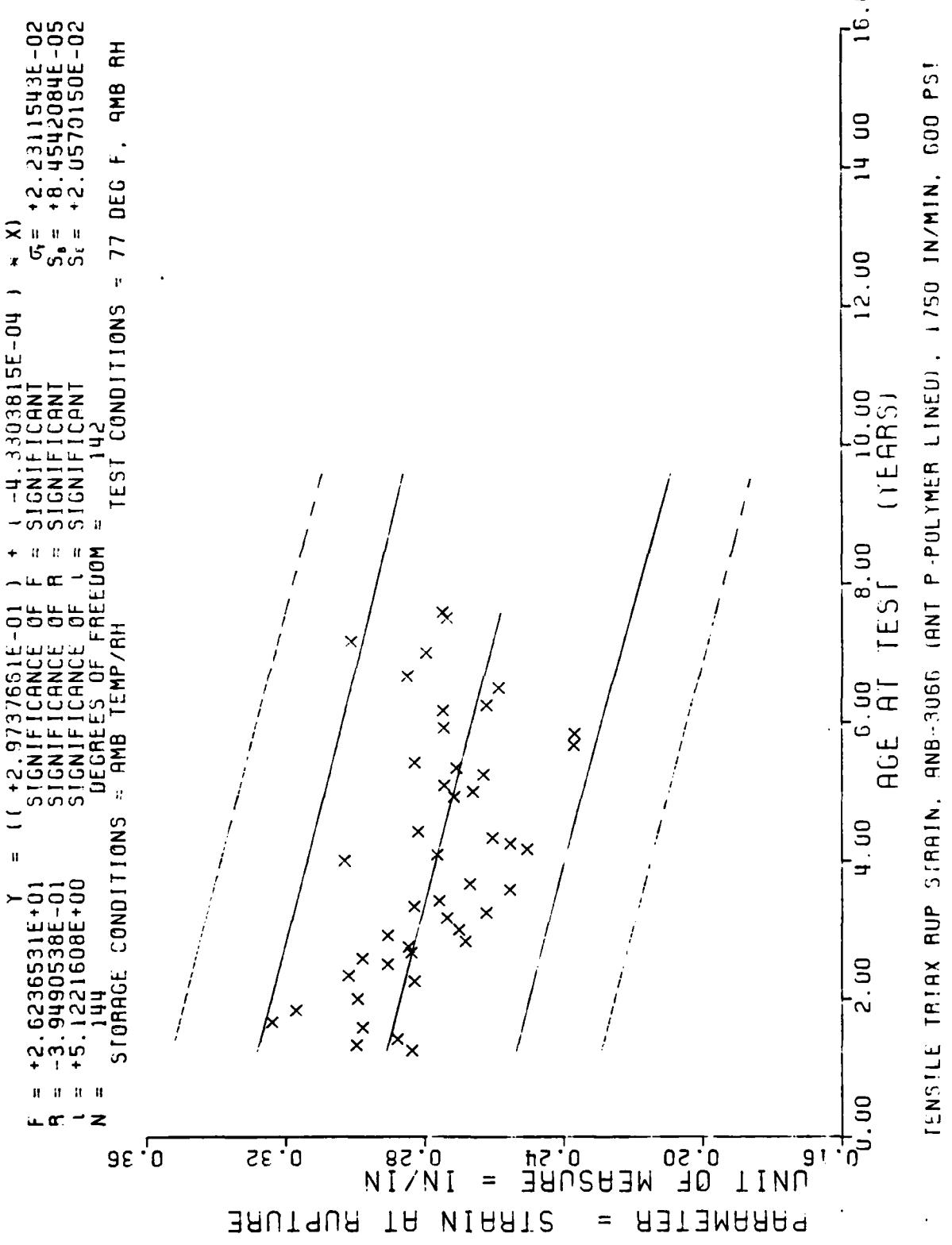


Figure 5-5

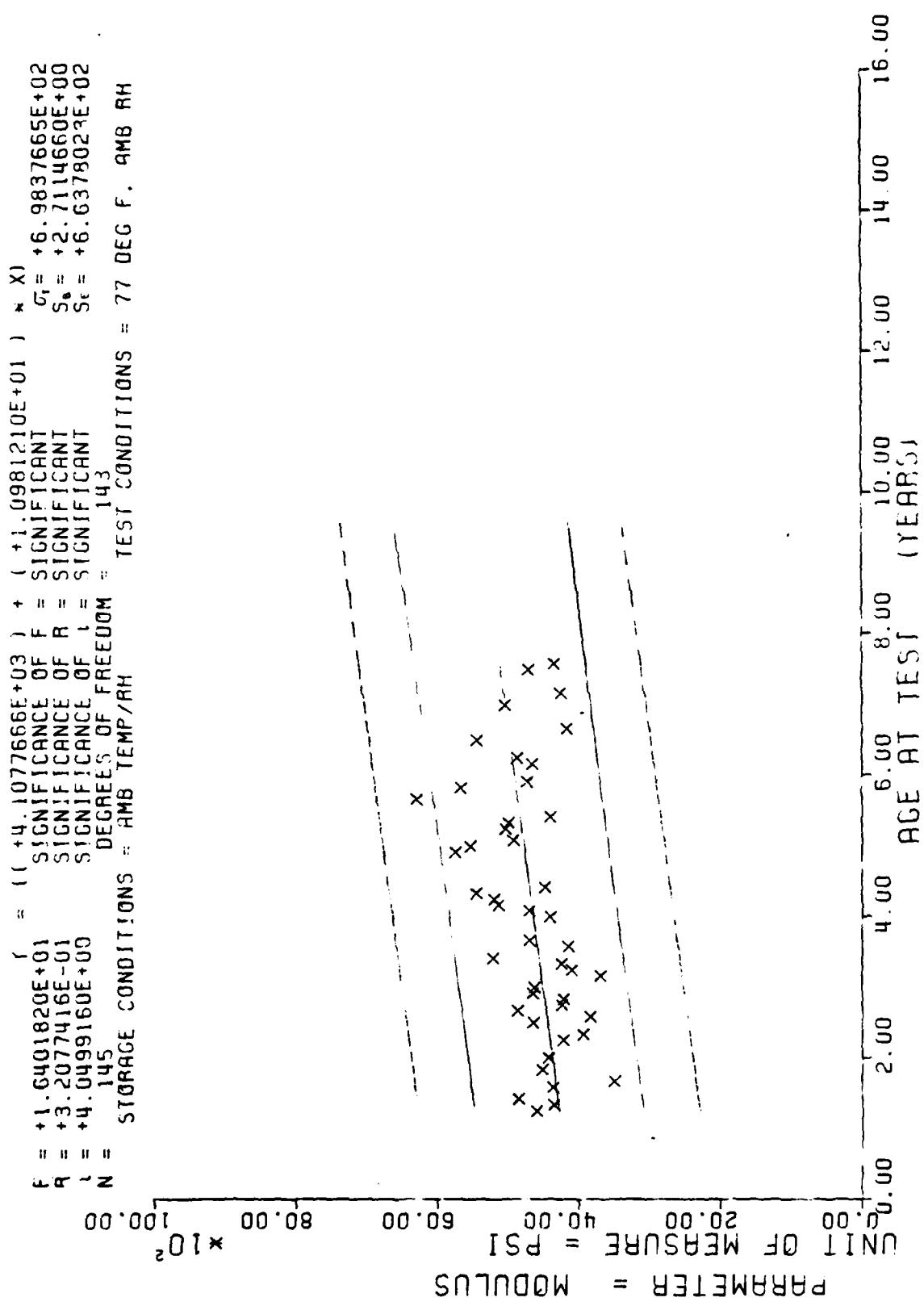


Figure 5-6

$F = +5.5227995E+00$ $\gamma = ((+5.7720833E+02) + (+1.0759085E-01) \times X)$
 $R = +8.7187658E-02$ SIGNIFICANCE OF F = SIGNIFICANT
 $I = +2.3500637E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 723$ SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = TEST CONDITIONS = 721

STORAGE CONDITIONS = AMB TEMP/RH

TEST CONDITIONS =

Δ ANBG
 X ANBP

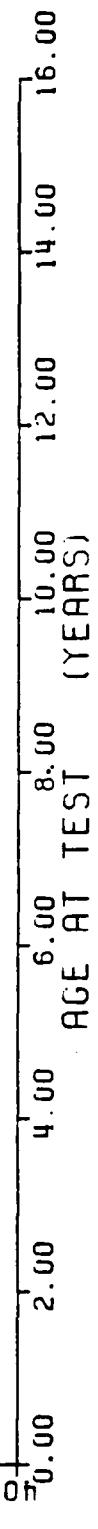
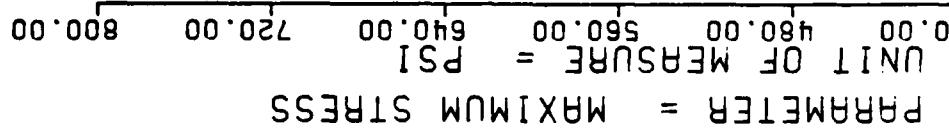


Figure 5-7

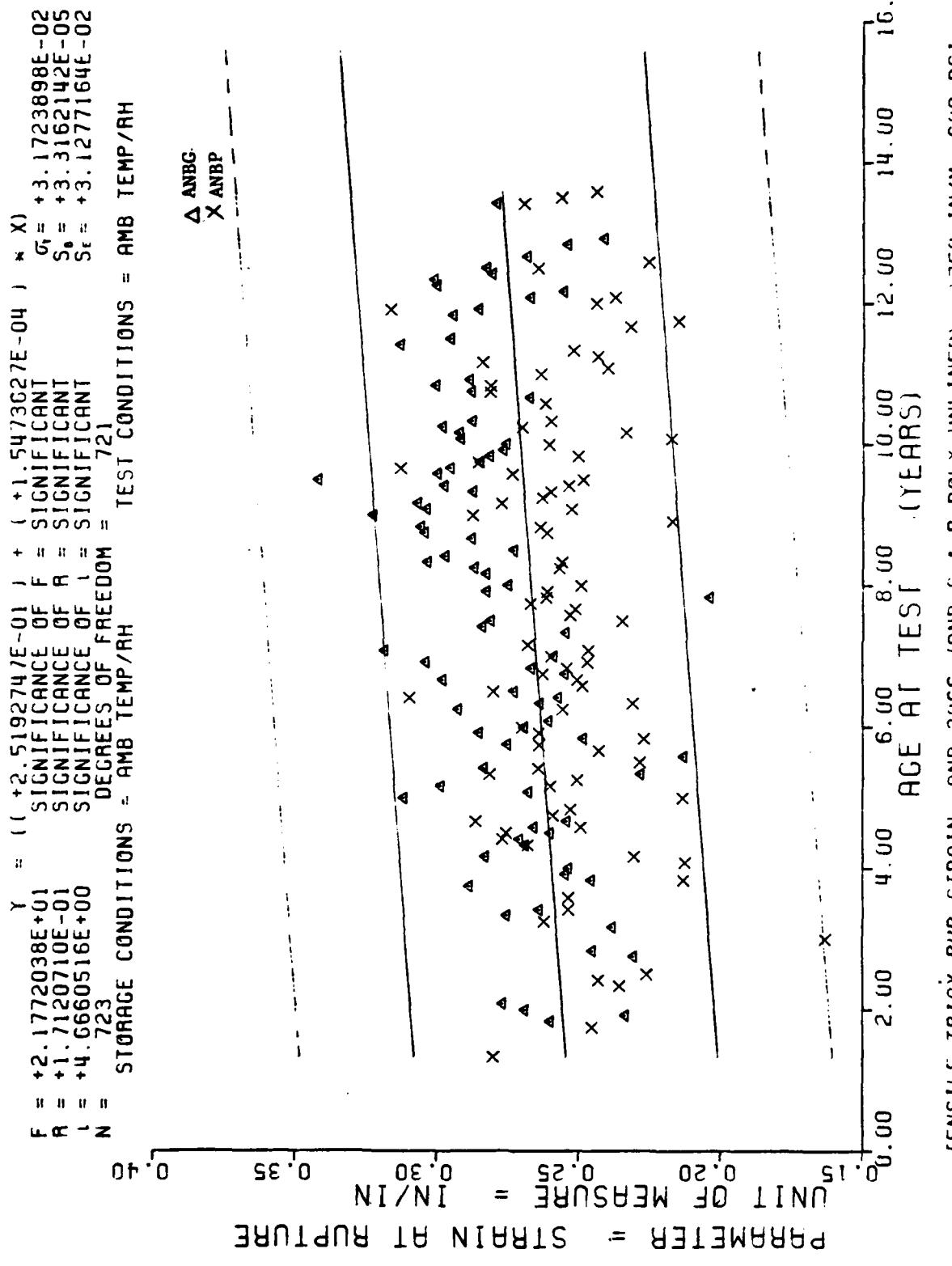


Figure 5-8

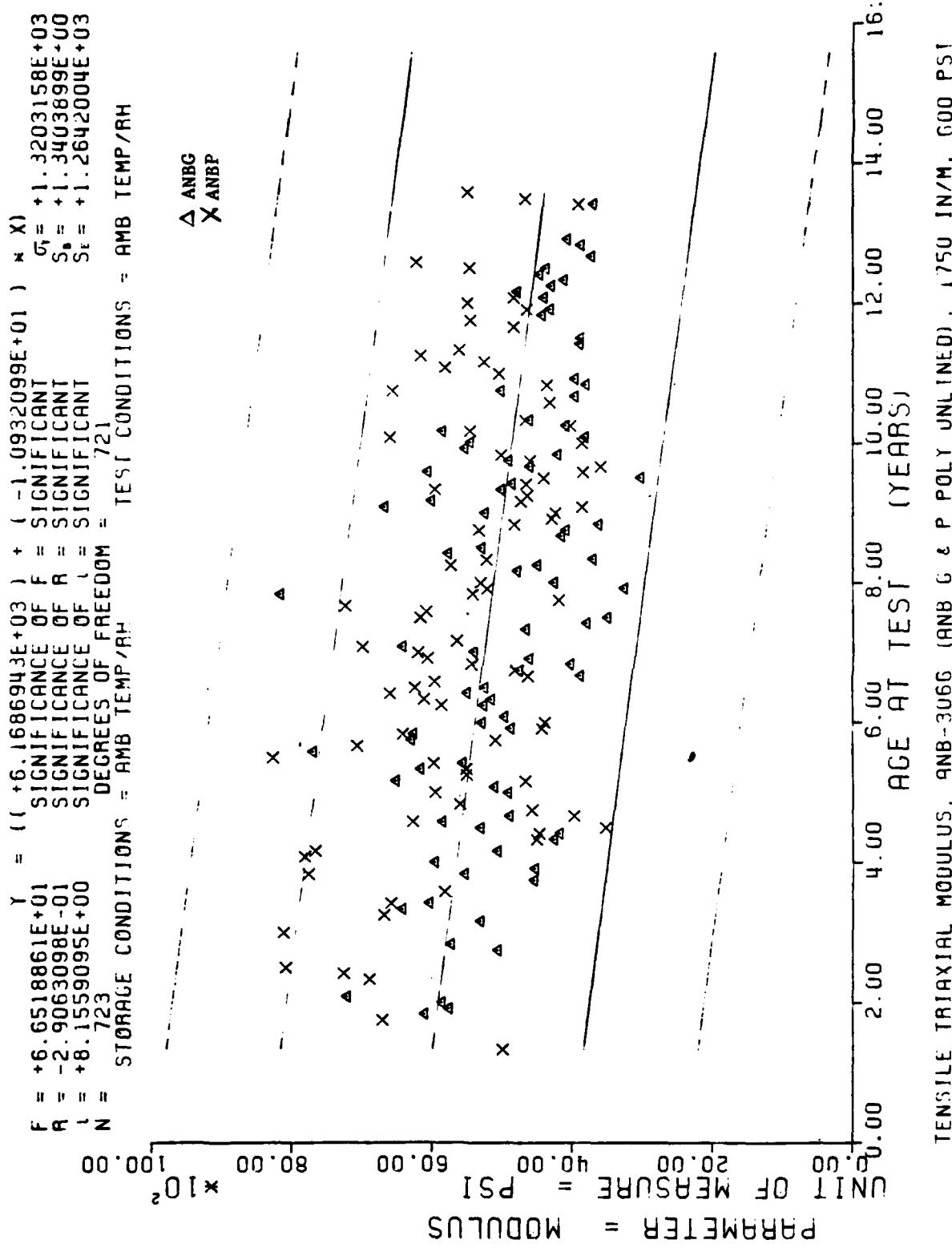


Figure 5-9

$\gamma = ((+5.7345627E+02) + (+4.6798318E-01) \times X)$
 $F = +1.9325899E+01$ SIGNIFICANCE OF $F =$ SIGNIFICANT
 $R = +2.6688503E-01$ SIGNIFICANCE OF $R =$ SIGNIFICANT
 $L = +4.3961231E+00$ SIGNIFICANCE OF $L =$ SIGNIFICANT
 $N = 254$ DEGREES OF FREEDOM = 252
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

+ ANBP
 ♦ ANT P

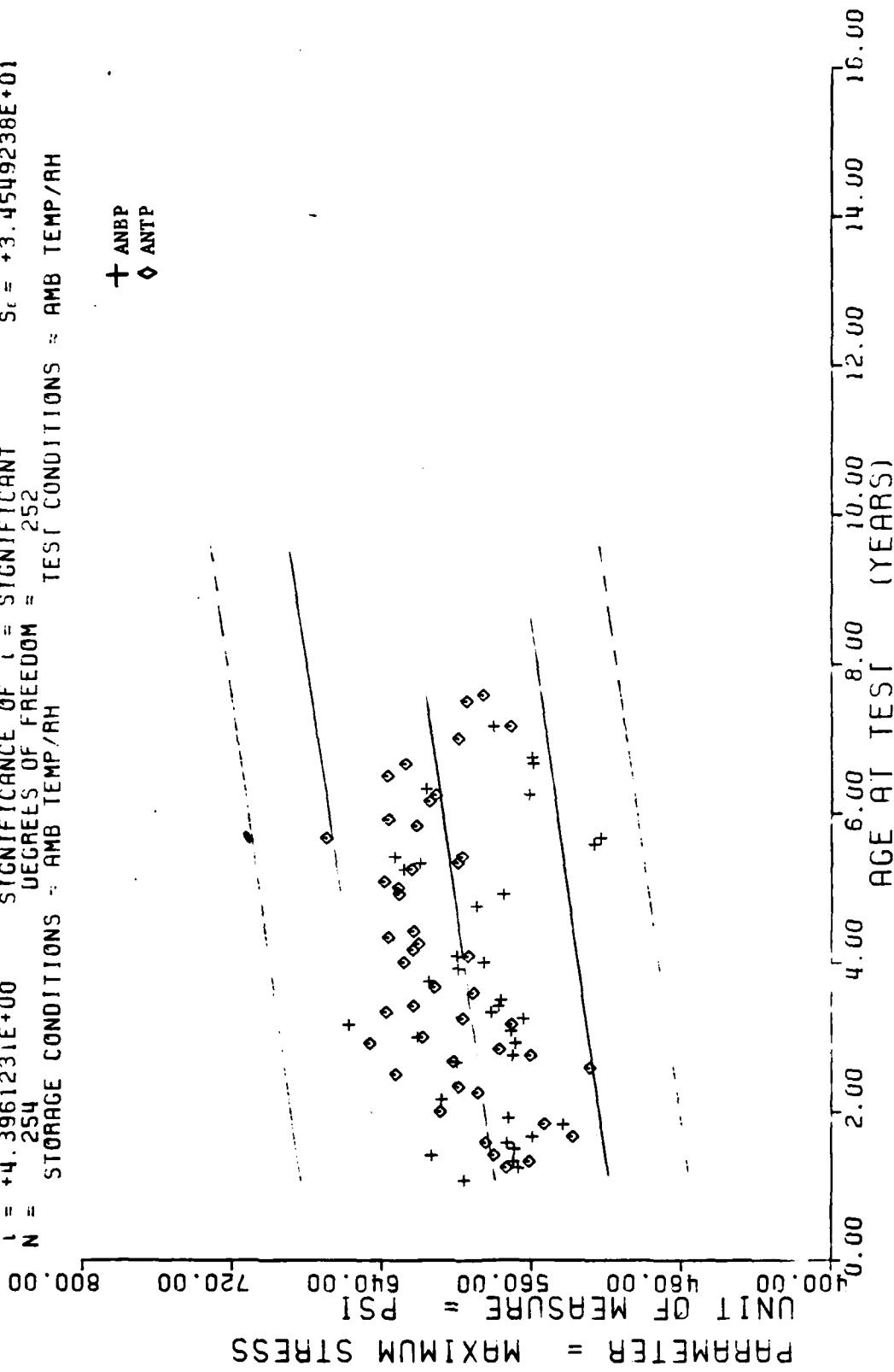


Figure 5-10

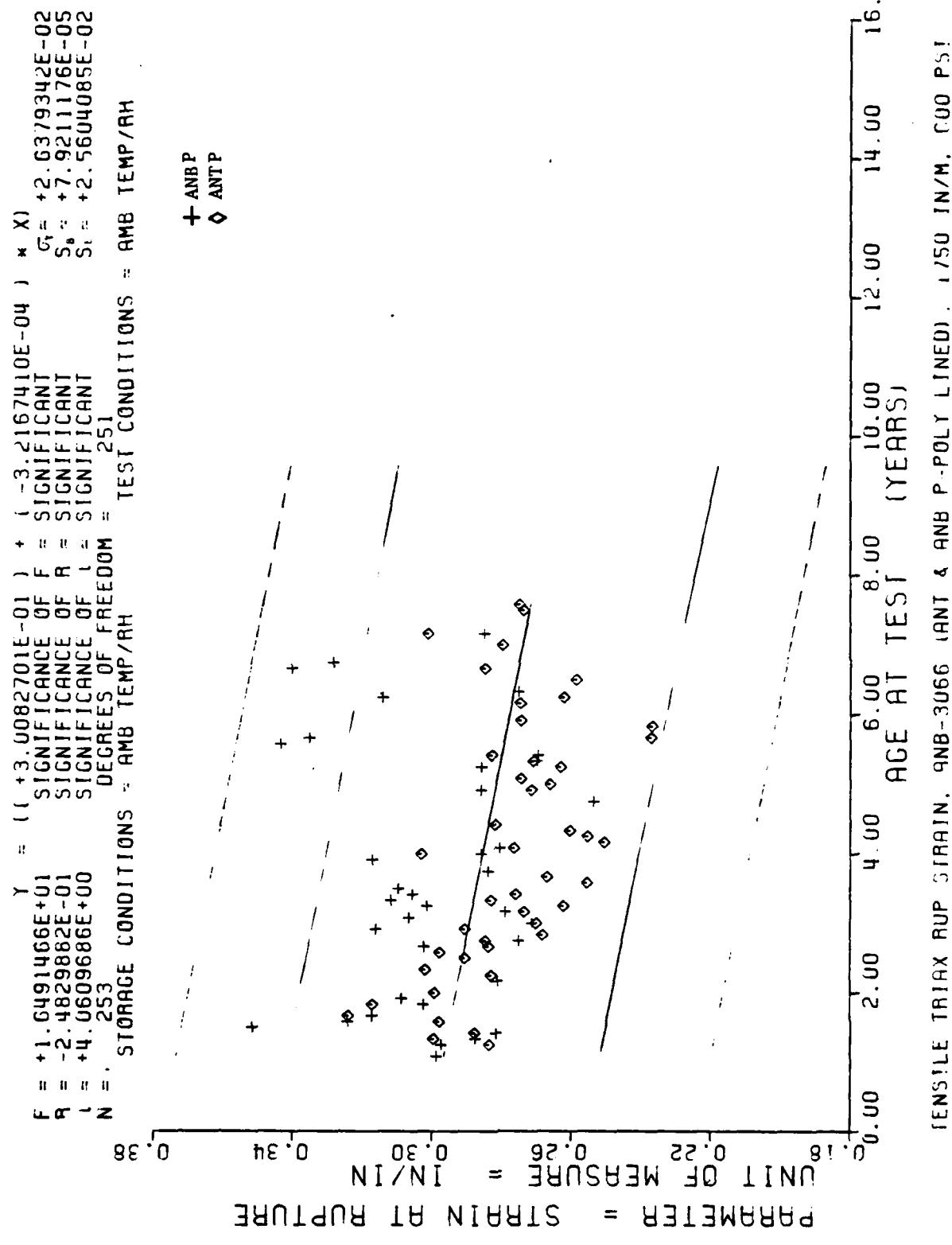
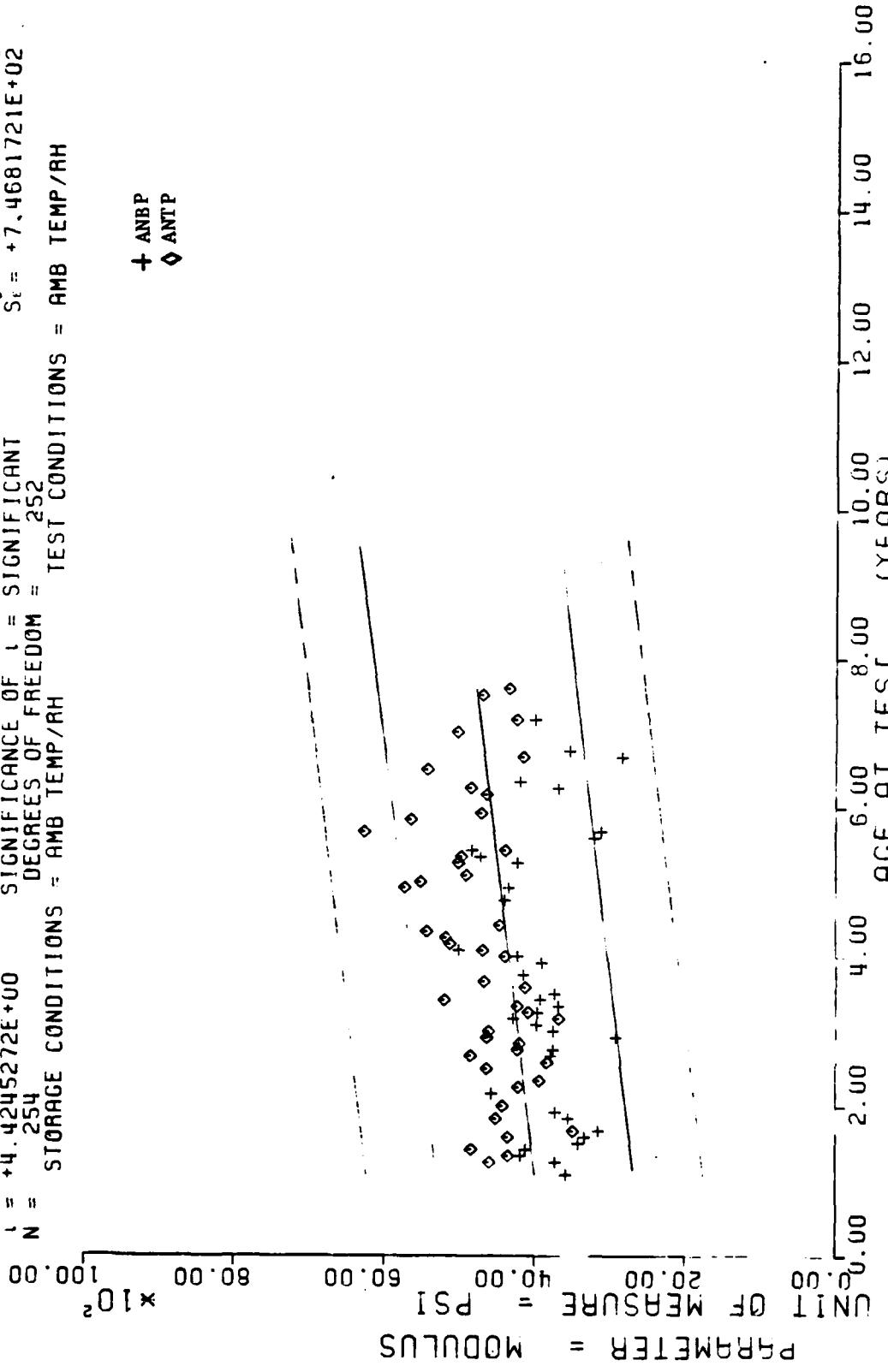


Figure 5-11

$F = +1.9576441E+01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +2.6848549E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $L = +4.4245272E+00$ SIGNIFICANCE OF L = SIGNIFICANT
 $N = 254$ DEGREES OF FREEDOM = 252

STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

\star ANBP
 \diamond ANT P



TENSILE TRIAXIAL MODULUS, QNB-3066 (ANT & ANB P-POLY LINED), 1750 IN/M, 600 PSI

Figure 5-12

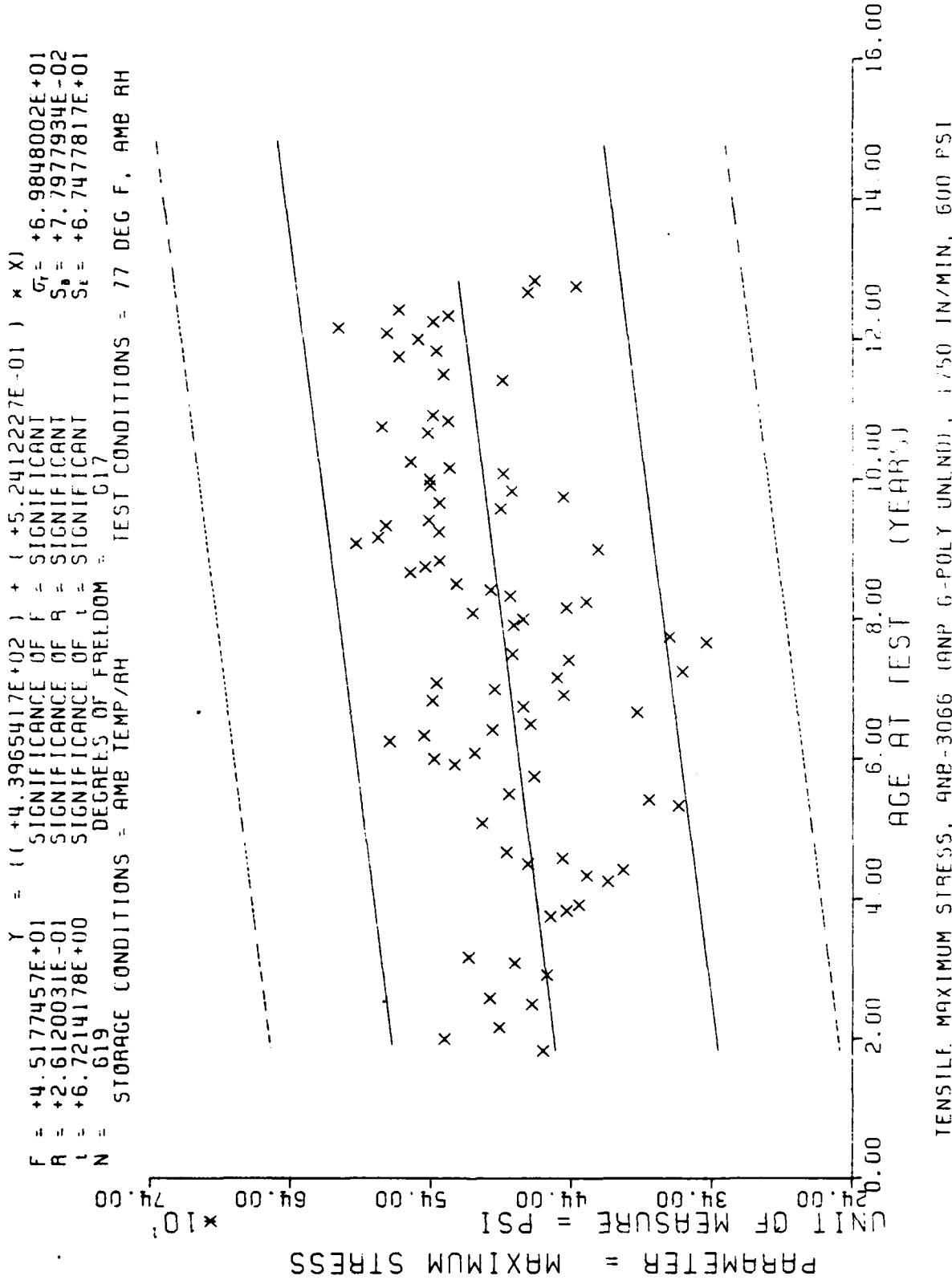


Figure 5-13

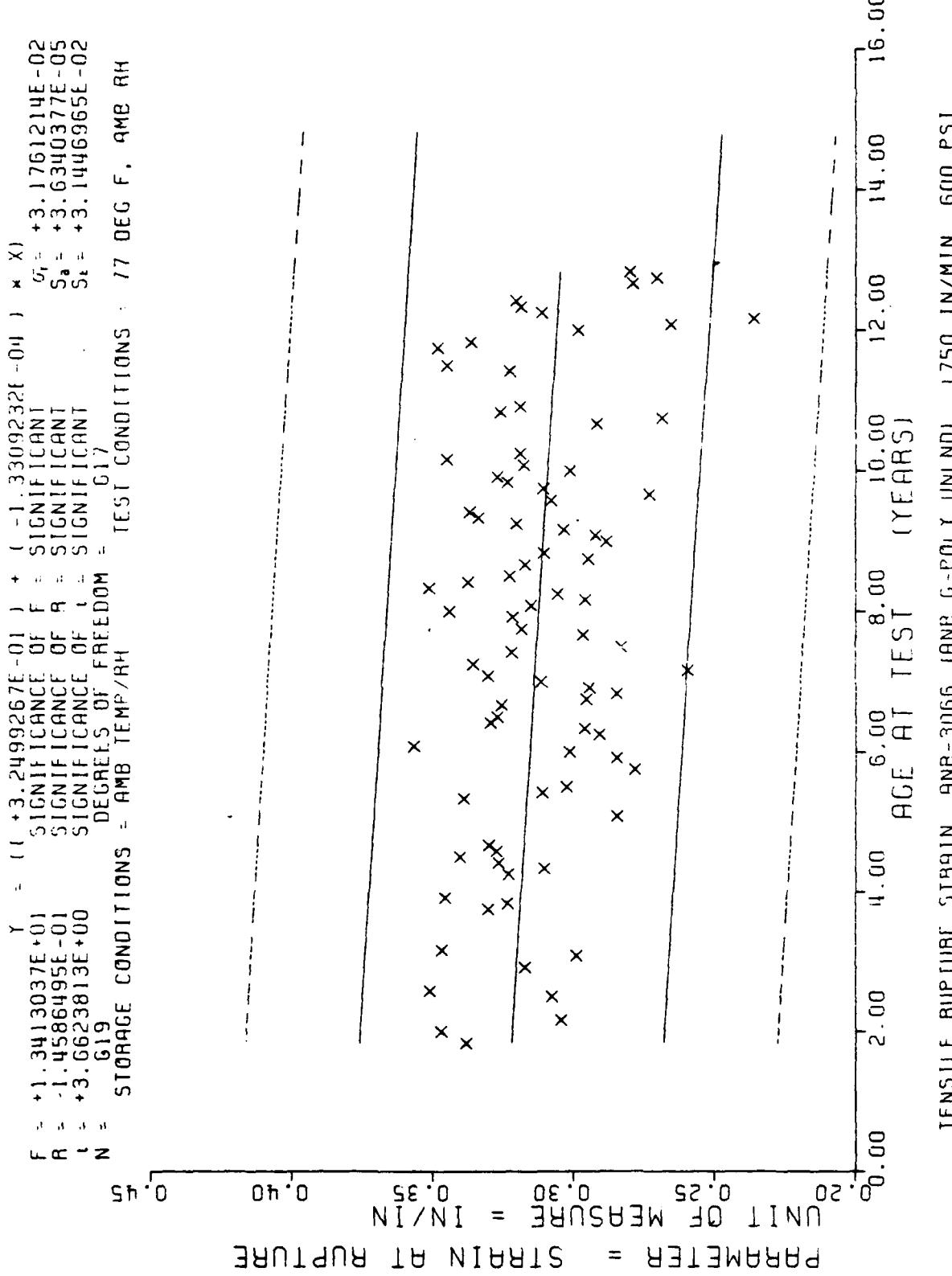


Figure 5-14

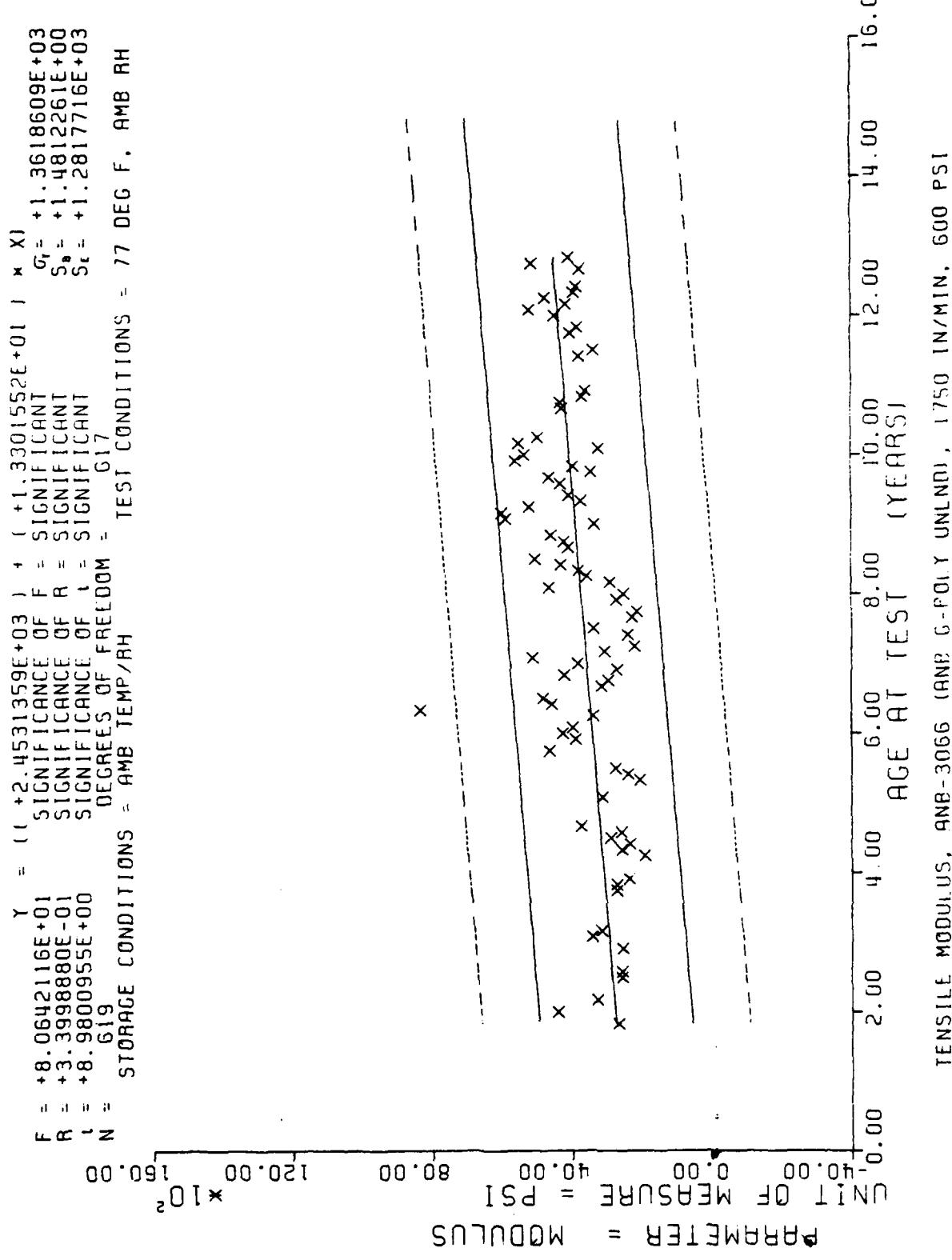


Figure 5-15

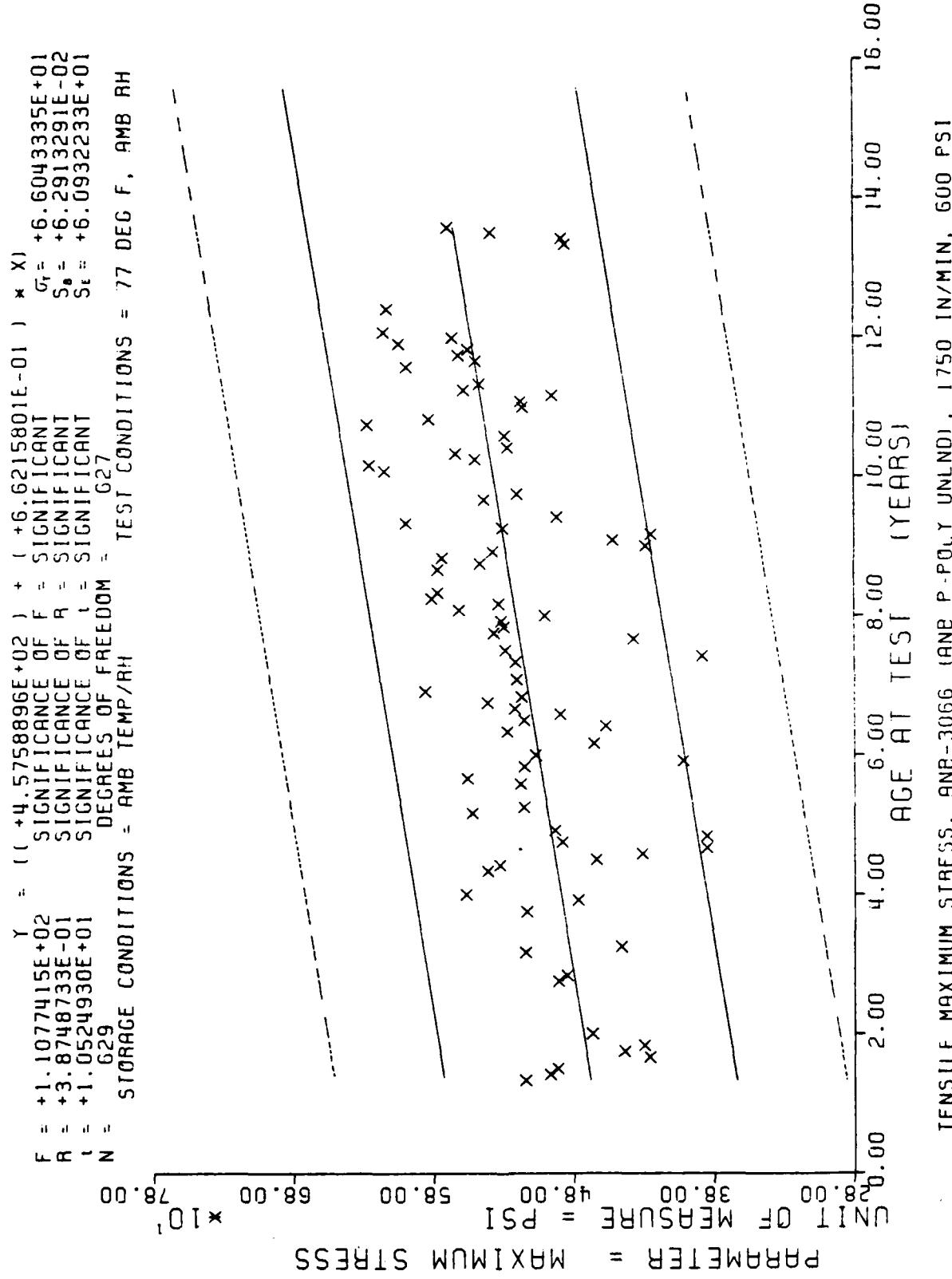


Figure 5-16

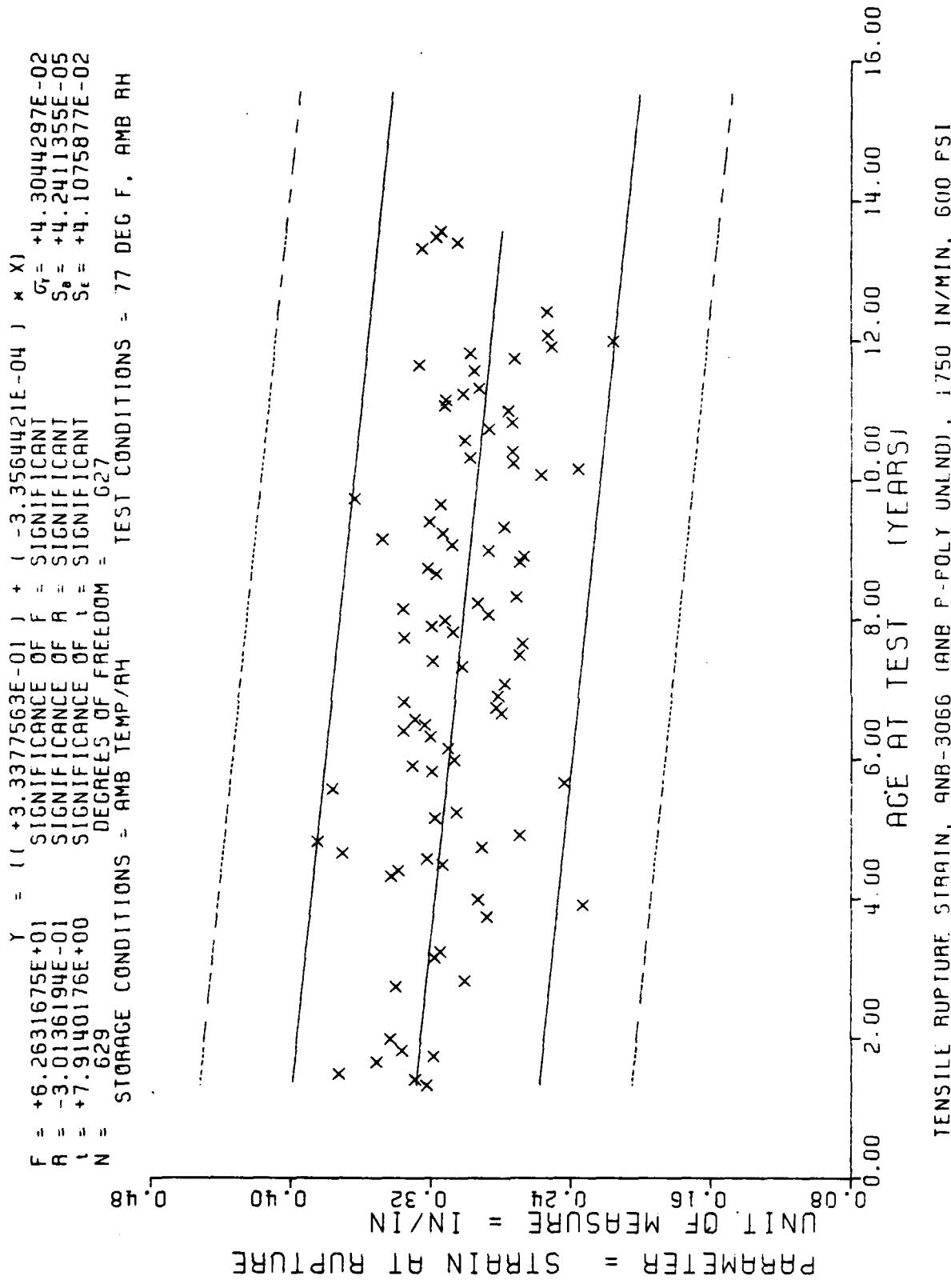


Figure 5-17

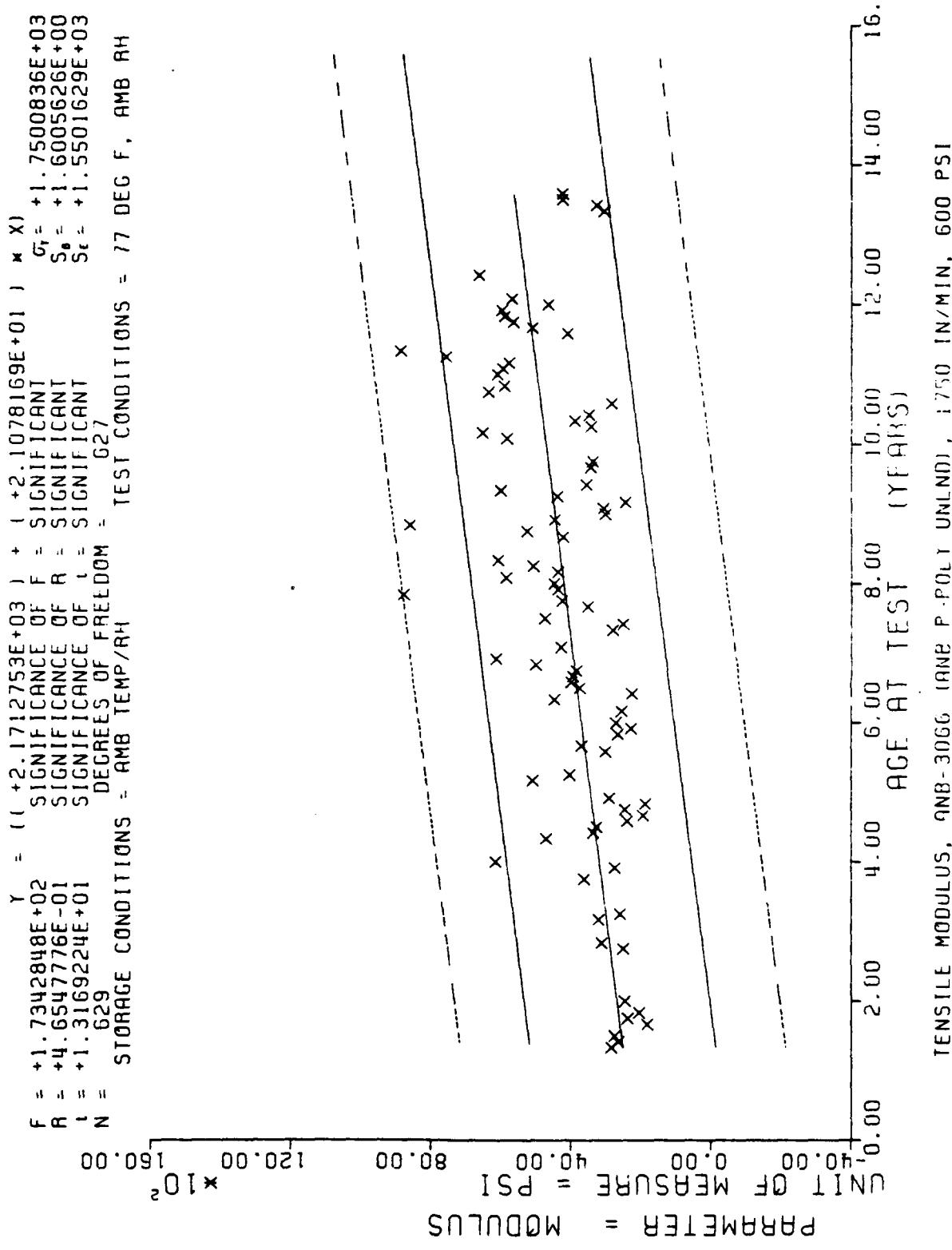


Figure 5-18

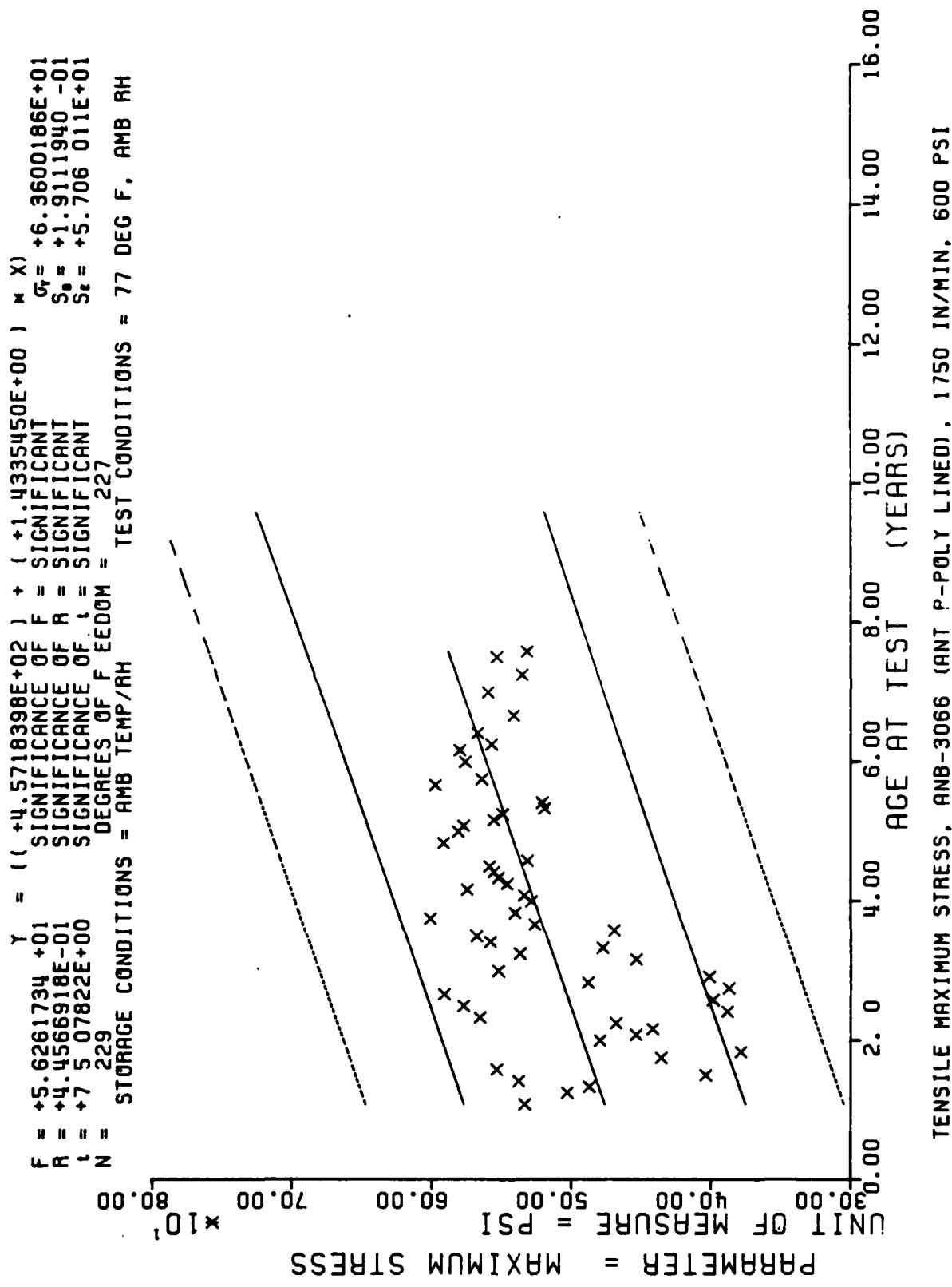


Figure 5-19

$F = +4.6940213E+00$
 $R = -1.4233611E-01$
 $I = +2.1665690E+00$
 $N = 229$
 SIGNIFICANCE OF F = NOT SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF I = SIGNIFICANT
 DEGREES OF FREEDOM = 227
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F. AMB RH

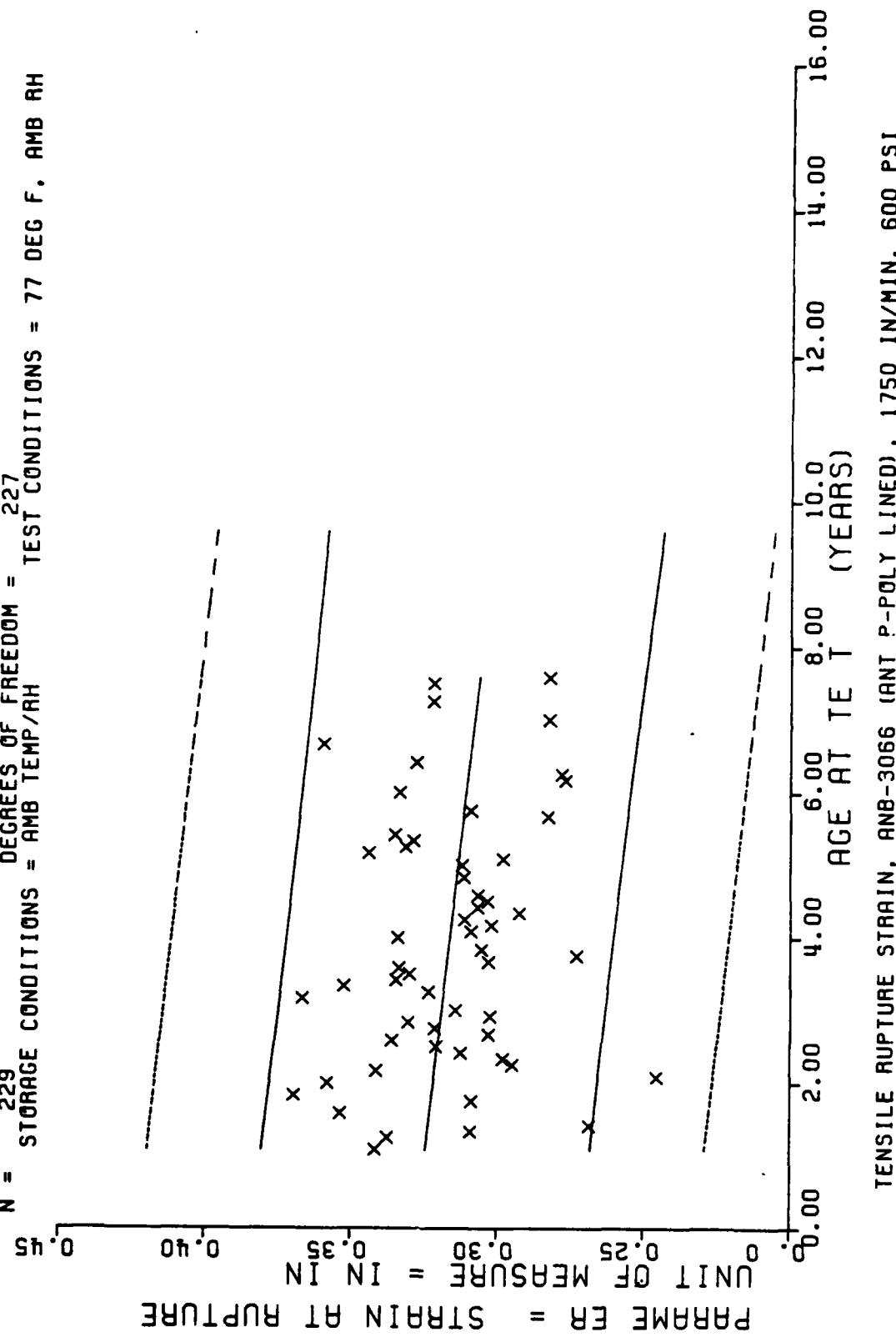


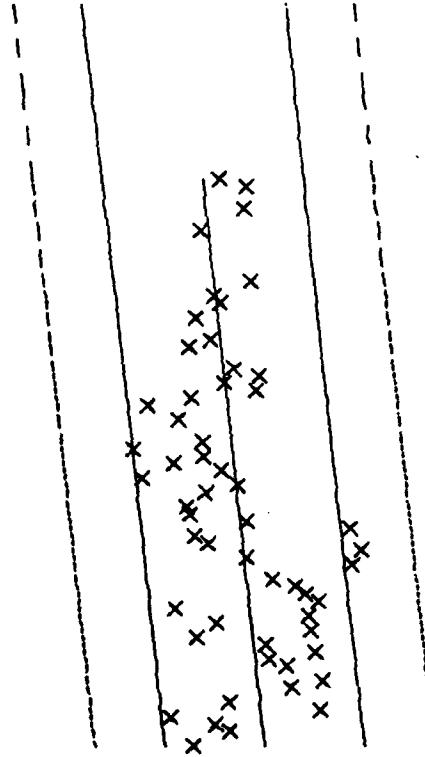
Figure 5-20

$F = +1.7190973E+01$ $\gamma = ((+3.3462286E+03) + (+1.8025853E+01) \times X)$
 $R = +2.6532943E-01$ SIGNIFICANCE OF F = SIGNIFICANT
 $I = +4.1461998E+00$ SIGNIFICANCE OF R = SIGNIFICANT
 $N = 229$ SIGNIFICANCE OF I = SIGNIFICANT
DEGREES OF FREEDOM = 227

STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

UNIT OF MEASURE = PSI PARAMETER = MODULUS
0.00 40.00 80.00 120.00 $\times 10^2$

TEST CONDITIONS = 77 DEG F, AMB RH



TEST CONDITIONS = 77 DEG F, AMB RH

Figure 5-21

SECTION VI

STRESS RELAXATION AND STRAIN DILATION

A. STRESS RELAXATION:

An end bonded 1/2" x 1/2" x 4" specimen (1.27 x 1.27 x 10.16 cm) is tested on the stress relaxometer. Load is applied at 2 in/min (.085 cm/sec). Timing begins when the load is applied. Specimens have been strained at both 1% and 3%.

The use of 1% strain over the range of temperatures was not introduced into the program until Phase 3 of Minuteman III testing and Phase B Series 2 for Minuteman II. In this report, data for both 1% and 3% at 77°F are shown for a comparison between applied strains. Thiokol has shown that strains introduced into the propellant during machining remain in the samples and a higher strain is required to give reproducible and accurate relaxation moduli. The 1% strain is considered to be very marginal insofar as reproducible data is concerned.

Table 6-1 gives the significance of 't' for both 1% and 3% strains. The number of specimens represented in each regression is shown so that the preponderance of test data at 3% strain is obvious. Next report will show composite regressions of 3% data.

Unlined cartons of ANB "G" show a significant decrease for both 1% and 3% (154 mo) while there is no significant change for lined cartons (82 mo).

Unlined cartons of ANB "P" show a significant increase at 1% (86 mo), but the 1000 second modulus at 3% shows a significant increase.

Unlined cartons of ANT "P" do not show a significant decrease at 1% (81), but the decrease is significant at 3% (91). Lined cartons (80 mo) still show a significant increase.

These data tend to contradict ASPC's findings which suggests that samples prepared from cartons appeared to decrease in modulus after 3.5 to 4 years of storage (ASPC 0162-06SAAS-21).

Gradient stress relaxation does not show a change from the last report. Minima occurs at approximately 2.2 inches from the liner.

B. STRAIN DILATATION:

The same type of specimen is used for this test as for stress relaxation. Testing is done in a gas dilatometer at 77°F (25°C) without pressure.

Poisson's Ratio at 15% strain consistently shows a significant decrease (Table 6-2). At maximum strain, Poisson's ratio is significantly decreasing for unlined cartons. ANB "G" and "P" unlined cartons do not show a significant change, while other cartons show a significant decrease.

TABLE 6-1
STRESS RELAXATION

Significance of Regression Slopes

SYSTEM	10 sec		10 sec		1000 sec	
	N	1%	N	3%	1%	3%
ANB G Unlined	180	Sig dec	760	Sig dec	Sig dec	Sig dec
ANB G Lined	48	NS	112	NS	NS	Sig inc
ANB P Unlined	168	Sig inc	589	Sig inc	Sig inc	Sig inc
ANB P Lined	72	NS	158	Sig inc	NS	Sig inc
ANT P Unlined	156	NS	399	Sig dec	NS	Sig dec
ANT P Lined	144	Sig inc	309	Sig dec	Sig inc	Sig inc
ANA & ANB G	218	Sig dec			Sig dec	
ANB G & P Unlined	348	Sig inc			NS	
ANB G & P Lined	120	NS			NS	
ANB & ANT P Unlined	324	Sig inc			Sig inc	
ANB & ANT P Lined	216	Sig inc			Sig inc	

TABLE 6-2
DILATATION

Significance of Regression Slopes

<u>SYSTEM</u>	<u>POISSONS RATIO</u> <u>AT 15% STRAIN</u>	<u>POISSONS RATIO</u> <u>AT MAX STRAIN</u>	<u>DILATATION AT</u> <u>MAX STRAIN</u>
ANB G Unlined	Sig dec	Sig dec	NS
ANB G Lined	Sig dec	NS	Sig dec
ANB P Unlined	Sig dec	Sig dec	NS
ANB P Lined	Sig dec	NS	Sig dec
ANT P Unlined	Sig dec	Sig dec	Sig dec
ANT P Lined	Sig dec	NS	Sig dec

NS = Not significantly different from zero slope

Sig inc = Positive slope

Sig dec = Negative slope

$F = +7.3109217E+00$
 $R = -1.9862575E-01$
 $t = +2.7038716E+00$
 $N = 180$
 STORAGE CONDITIONS = AMB TEMP/RH

$\gamma = ((+7.9693698E+02) + (-1.2943926E+00) \times X) / 10^4$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 178

TEST CONDITIONS = 77 DEG F. AMB RH

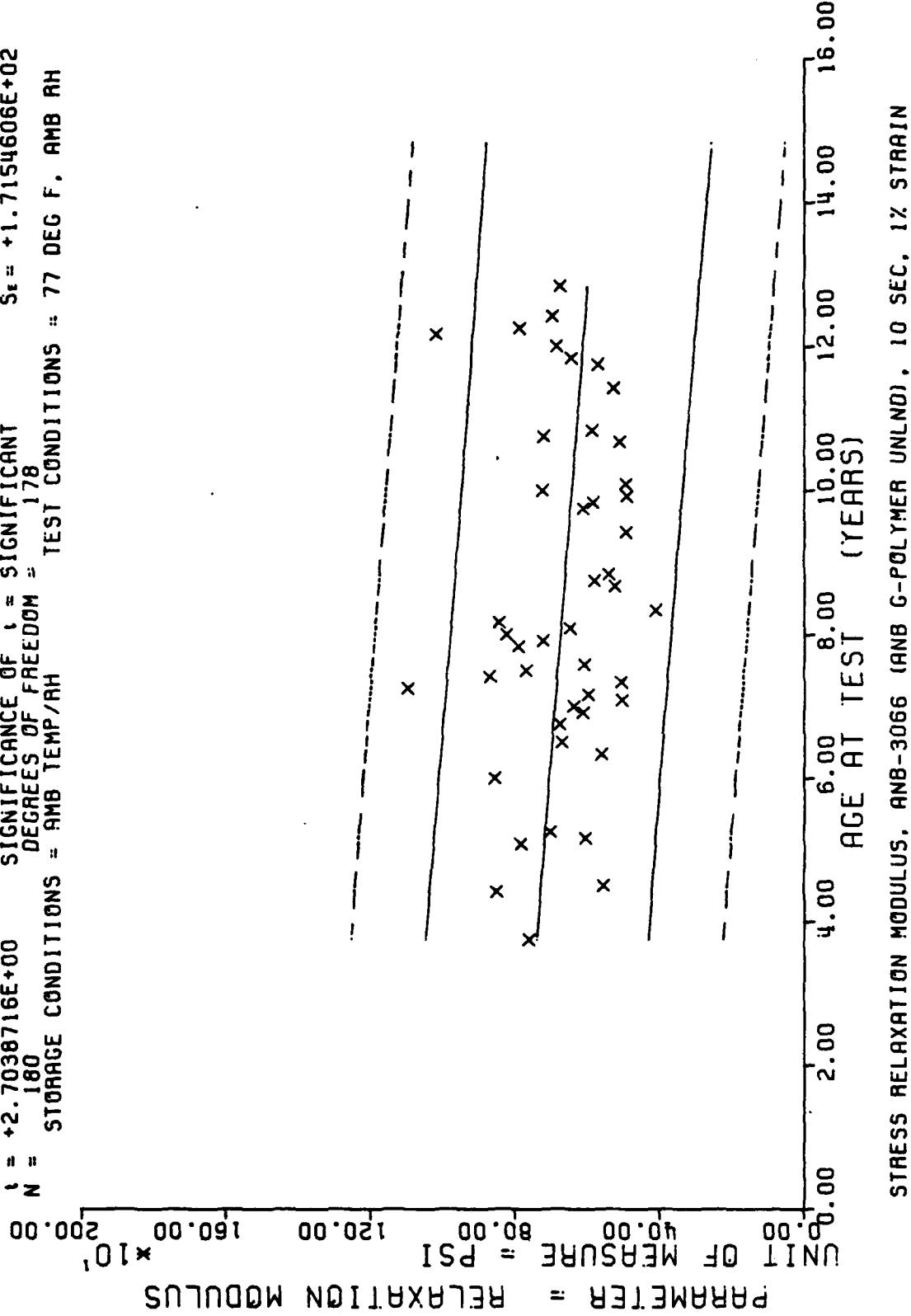


Figure 6-1

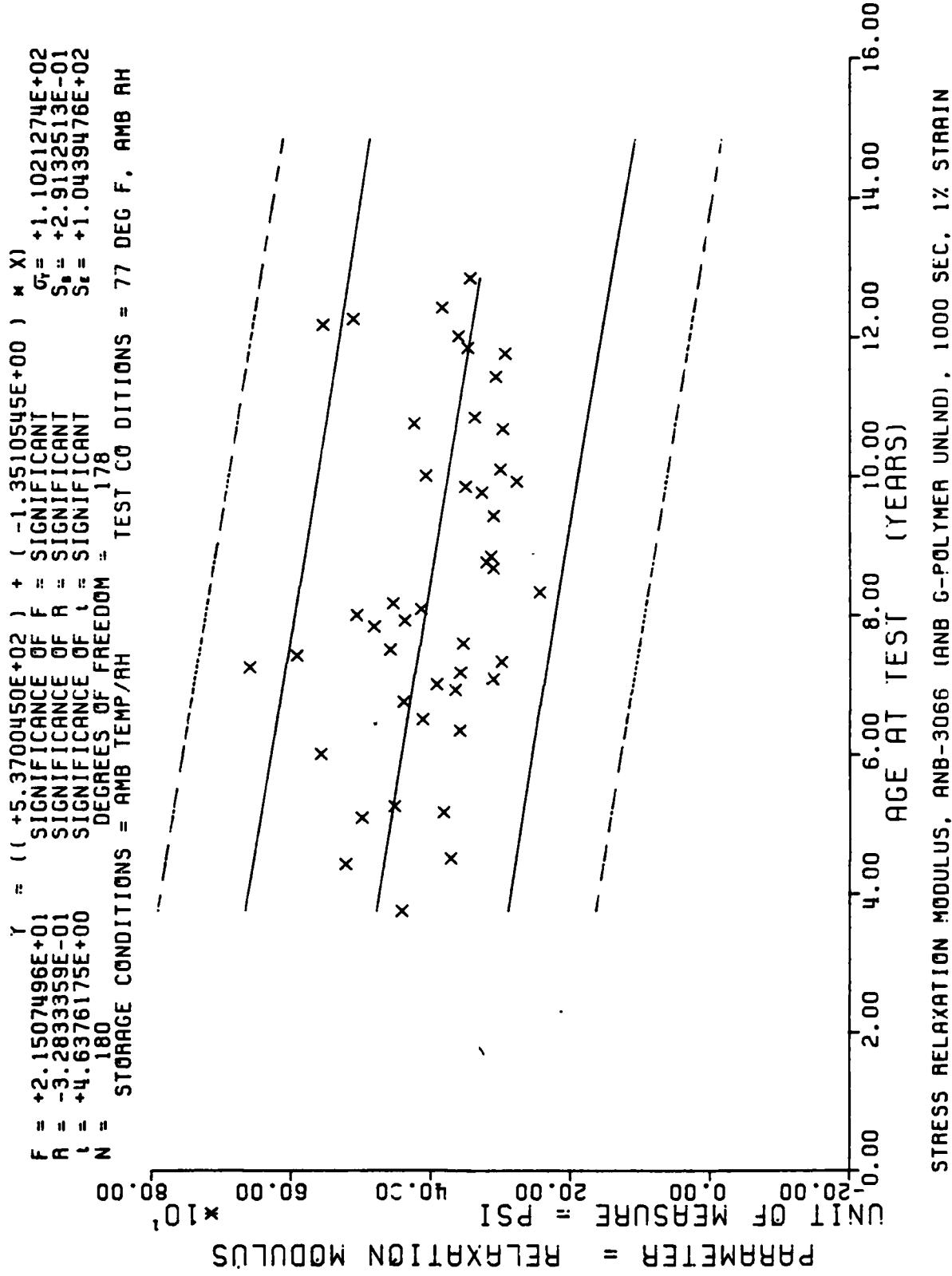


Figure 6-2

$F = +7.9981604E+00$
 $R = -1.0598773E-01$
 $L = +2.8281019E+00$
 $N = 706$
 STORAGE CONDITIONS = AMB TEMP/RH DEGREES OF FREEDOM = 704

$\gamma = ((+7.5483327E+02) + (-4.2640862E-01) * X)$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF L = SIGNIFICANT

$S_f = +1.6055503E+02$
 $S_o = +1.5077555E-01$
 $S_r = +1.5976404E+02$

TEST CONDITIONS = 77 DEG F. AMB RH

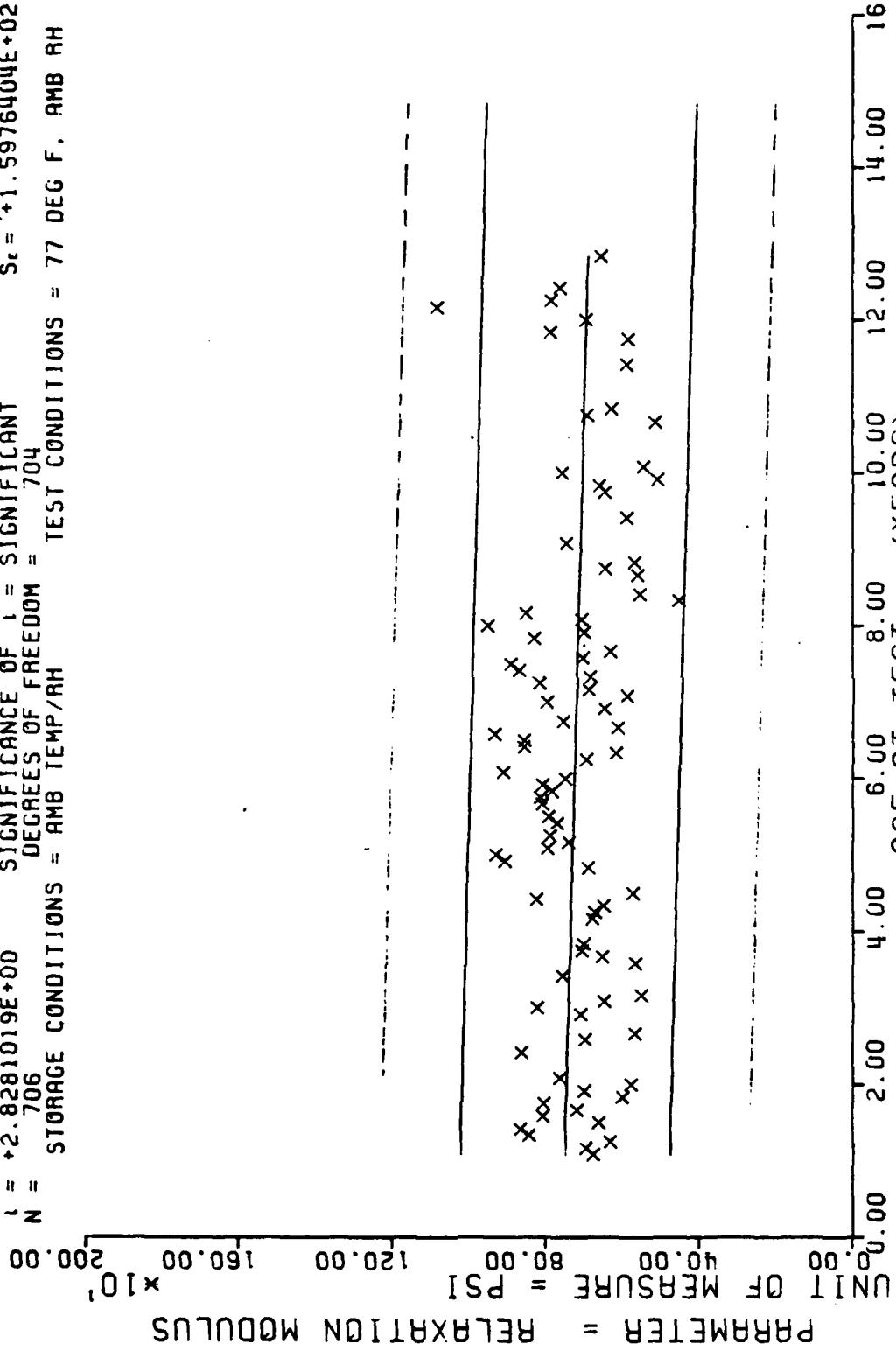


Figure 6-3

$F = +2.4782996E+01$
 $R = -1.8440716E-01$
 $t = +4.9782523E+00$
 $N = 706$
 STORAGE CONDITIONS = AMB TEMP/RH

$\gamma = ((+4.4533877E+02) + (-3.9686604E-01) * X)$
 SIGNIFICANCE OF F = SIGNIFICANT
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 704

TEST CONDITIONS = 77 DEG F, AMB RH

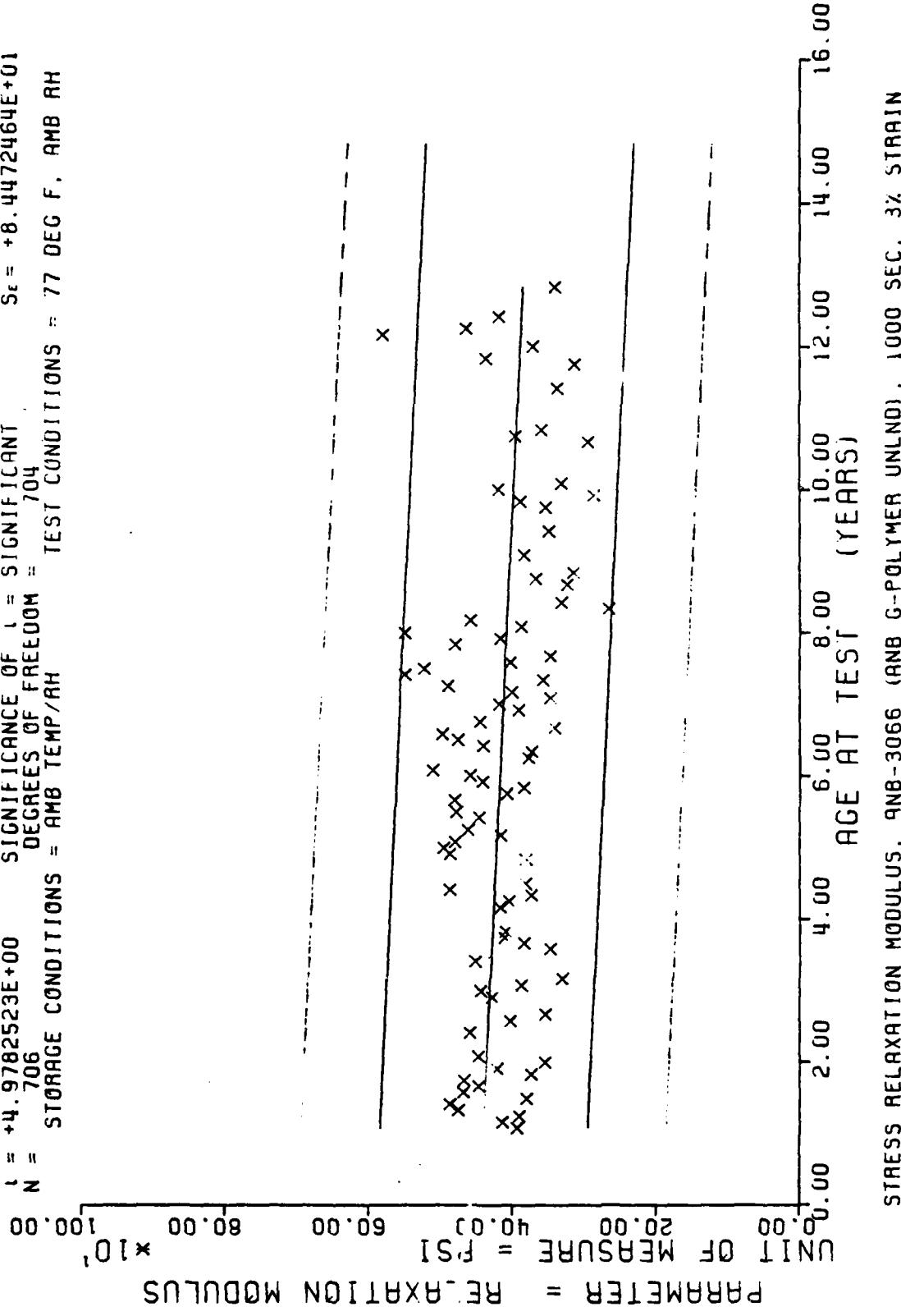


Figure 6-4

$F = +2.7423960E+01$ $\gamma = ((+6.3110886E+02) + (+2.4836118E+00) \times X)$
 $R = +3.7653899E-01$ $F = \text{SIGNIFICANT}$
 $I = +5.2367891E+00$ $R = \text{SIGNIFICANT}$
 $N = 168$ $I = \text{SIGNIFICANT}$
DEGREES OF FREEDOM = 166 TEST CONDITIONS = 77 DEG F, AMB RH

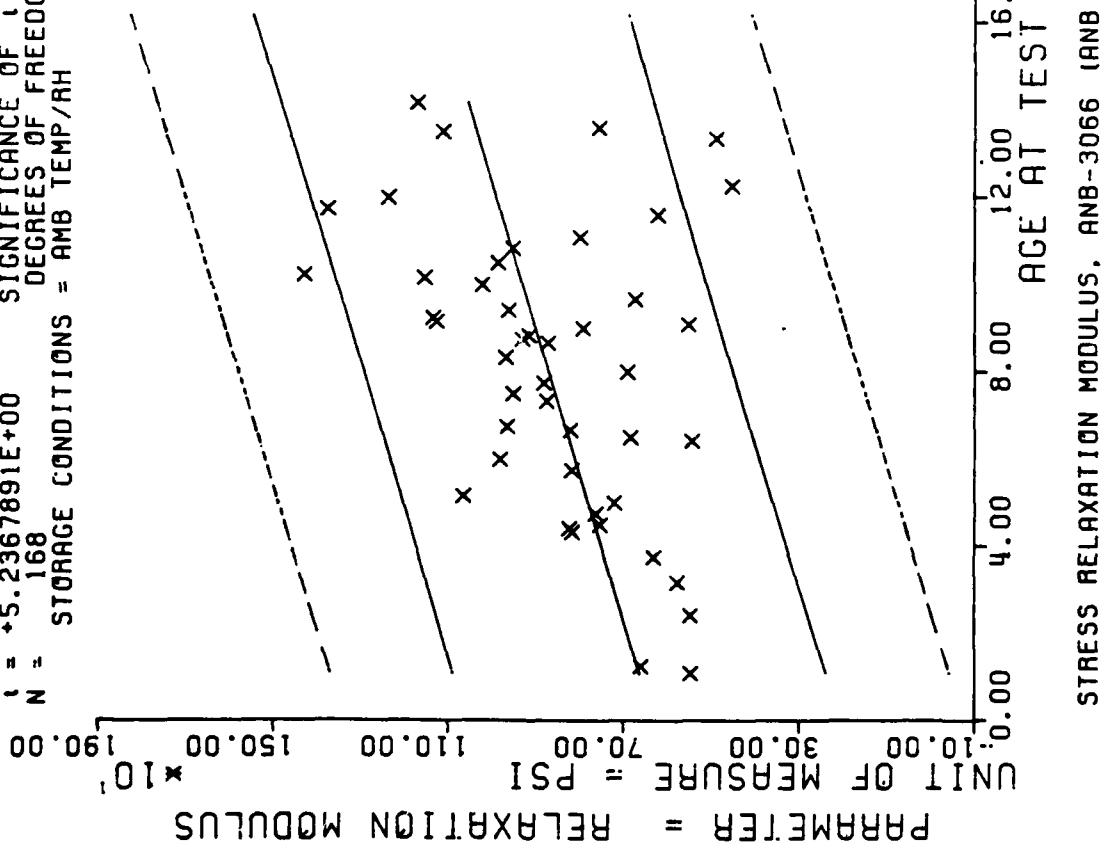


Figure 6-5

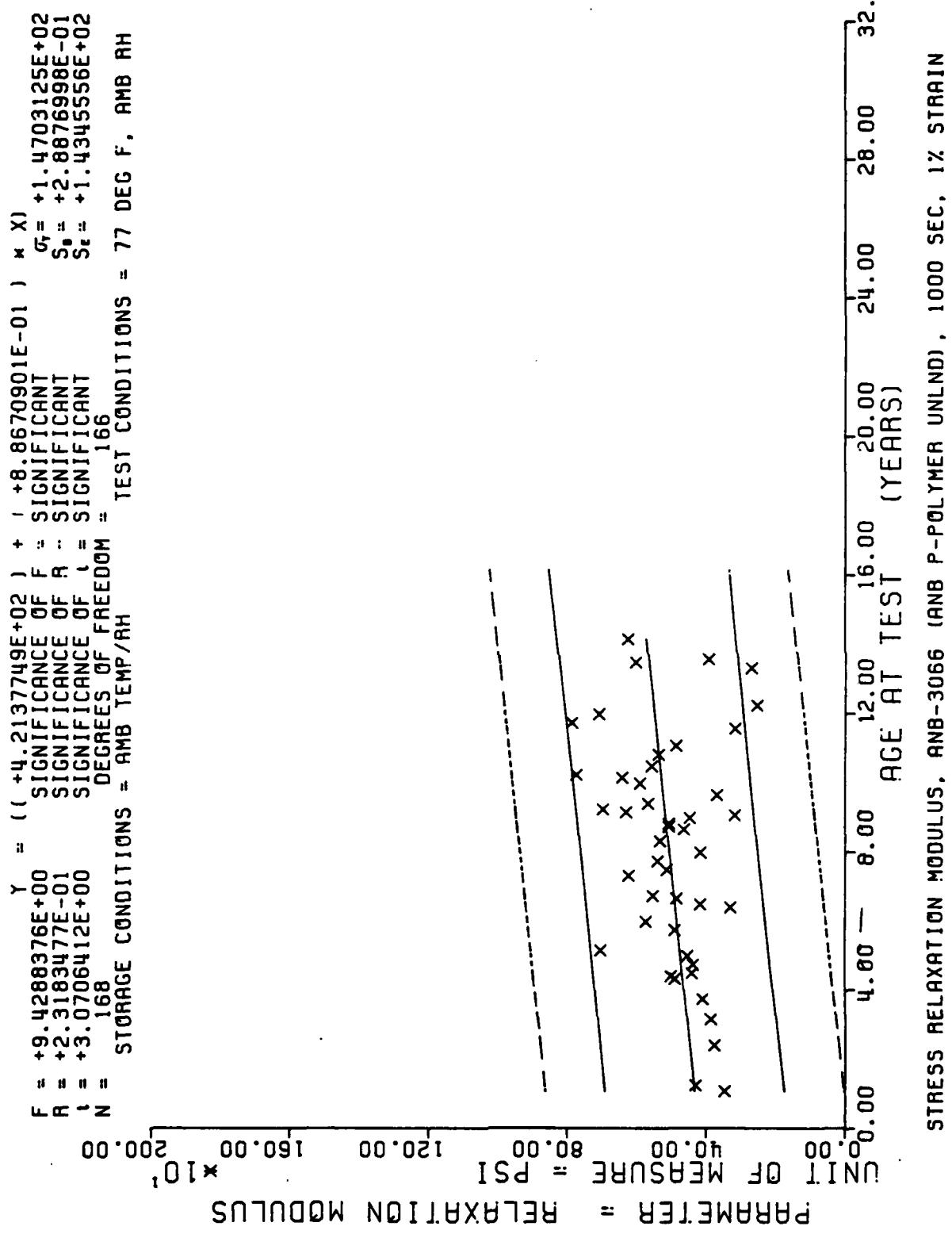


Figure 6-6

$\gamma = ((+7.6271664E+02) + (+1.3625473E+00) * X)$
 $F = \text{SIGNIFICANCE OF } F = \text{SIGNIFICANT}$
 $R = \text{SIGNIFICANCE OF } R = \text{SIGNIFICANT}$
 $I = \text{SIGNIFICANCE OF } I = \text{SIGNIFICANT}$
 $N = 589$
 $Degrees of Freedom = 587$
 $Storage Conditions = \text{AMB TEMP/RH}$
 $Test Conditions = 77 \text{ DEC F. AMB RH}$

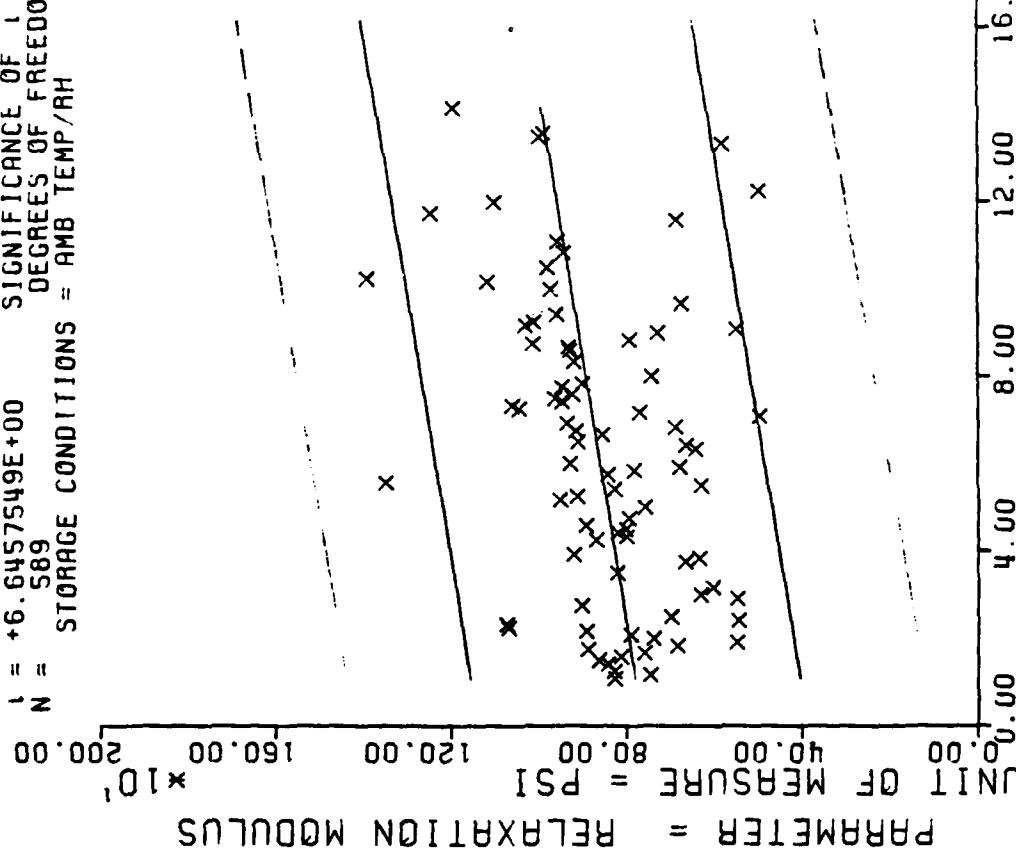


Figure 6-7

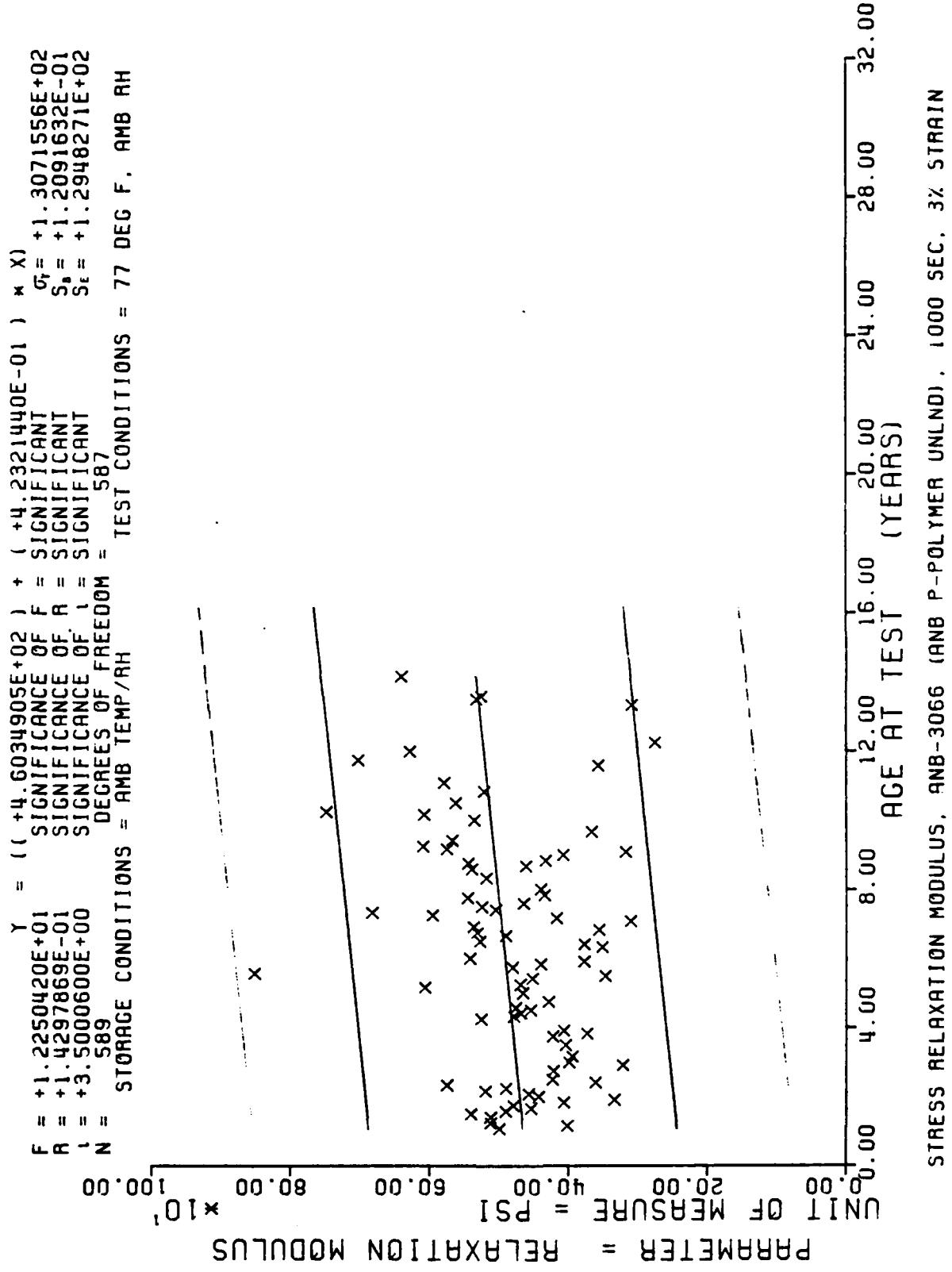


Figure 6-8

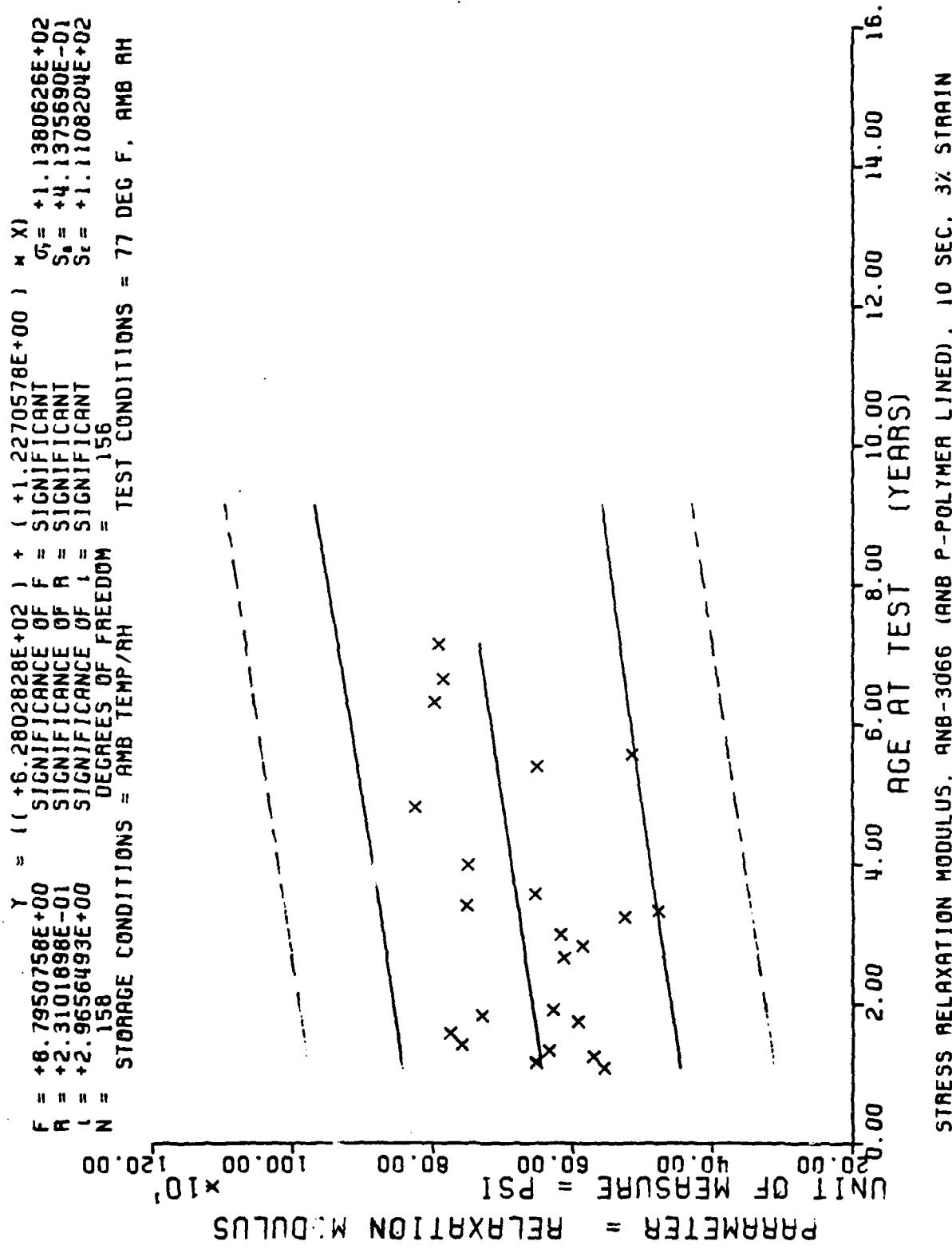


Figure 6-9

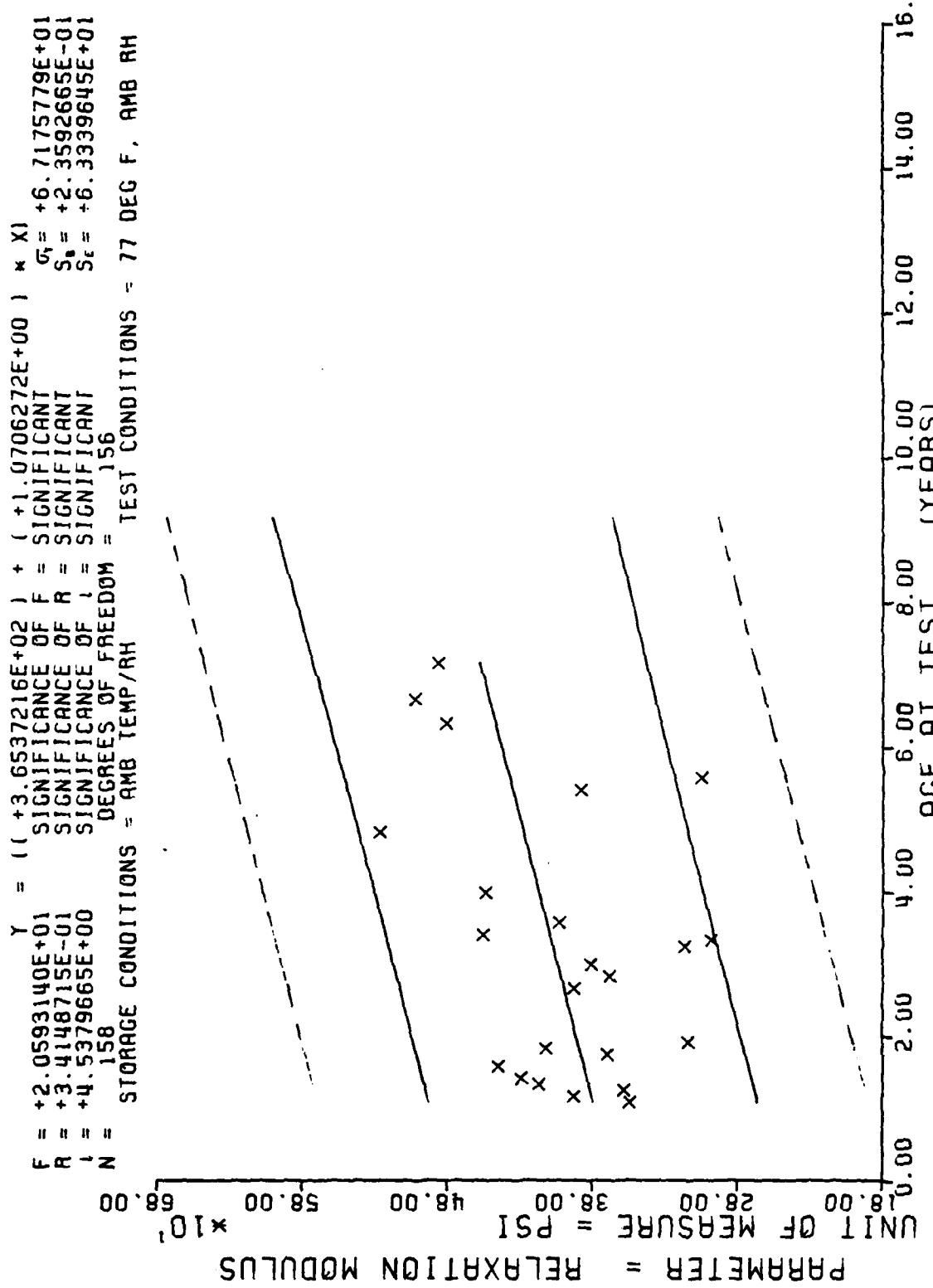
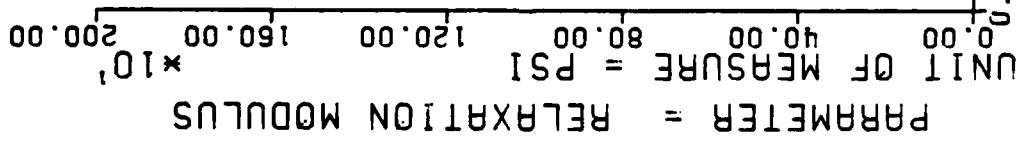


Figure 6-10

$F = +1.8371595E+01$ $\gamma = ((+9.6820688E+02) + (-1.7499184E+00)) * X$
 $R = -2.1030763E-01$ SIGNIFICANT OF F = SIGNIFICANT
 $I = +4.2862099E+00$ SIGNIFICANT OF R = SIGNIFICANT
 $N = 399$ SIGNIFICANT OF I = SIGNIFICANT
DEGREES OF FREEDOM = 397 TEST CONDITIONS = 77 DEG F. AMB RH



STRESS RELAXATION MODULUS, QNB-3066 (ANT P-POLYMER UNLND), 10 SEC. 3% STRAIN

Figure 6-11

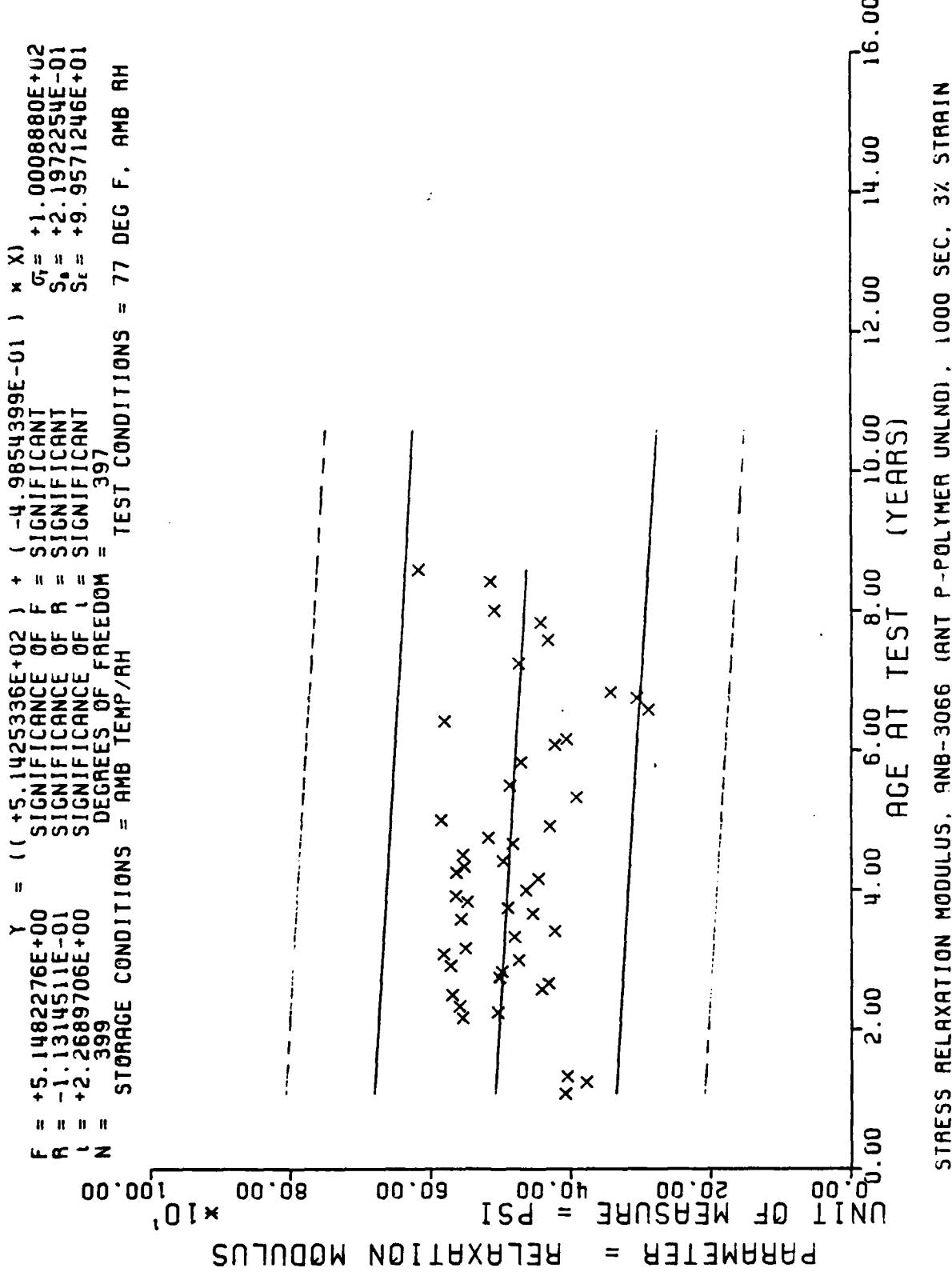


Figure 6-12

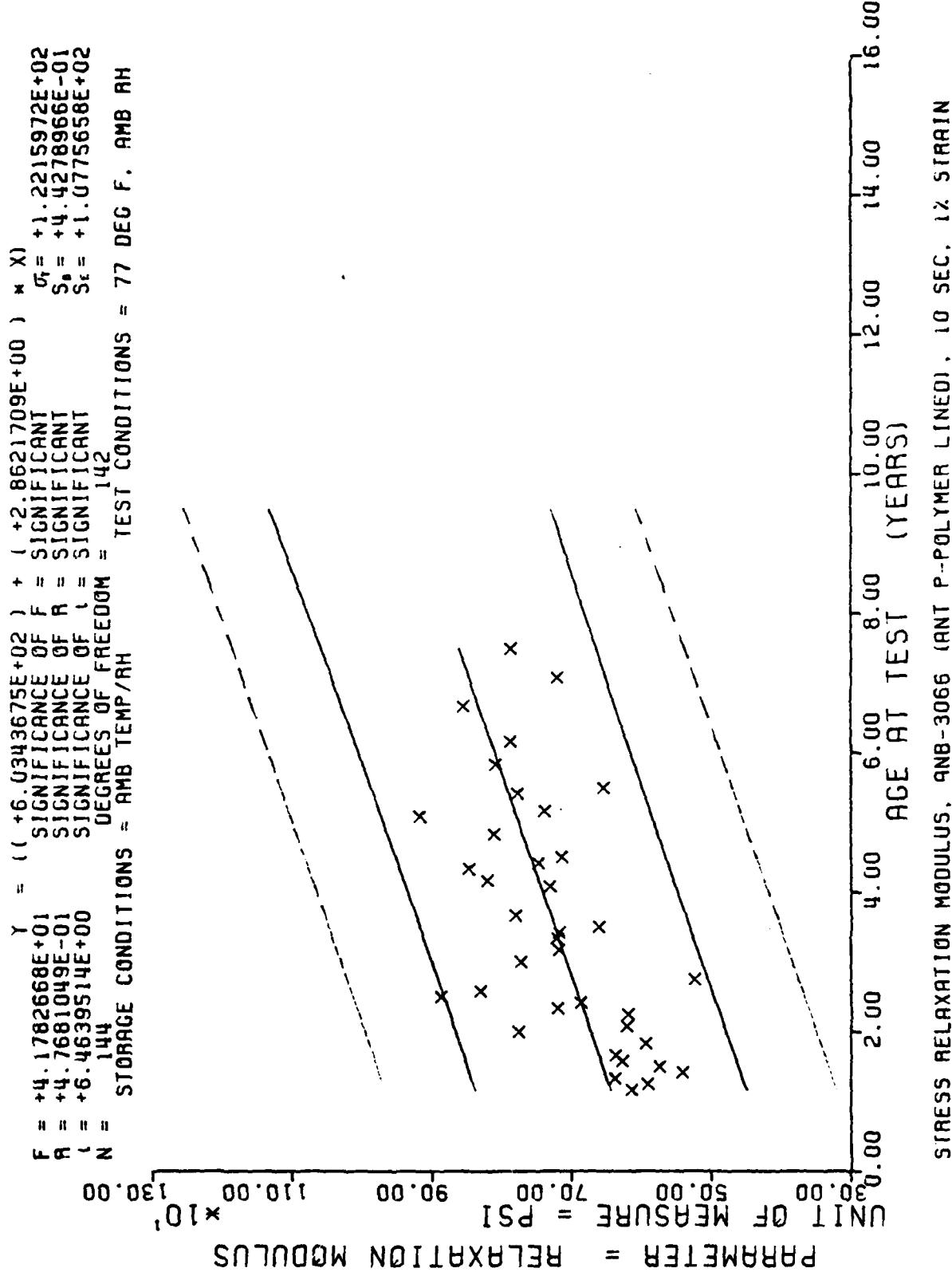
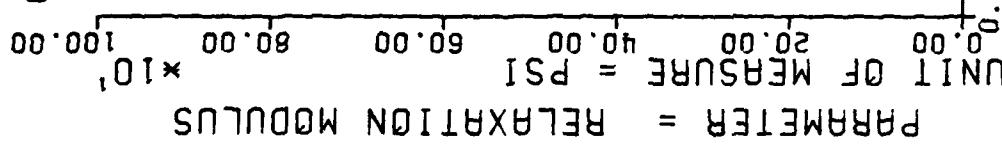


Figure 6-13

$\gamma = 1 (+3.7414550E+02) + (+1.8031072E+00) \times X$
 $F = +4.2453540E+01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +4.7974831E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $\lambda = +6.5156381E+00$ SIGNIFICANCE OF λ = SIGNIFICANT
 $N = 144$ DEGREES OF FREEDOM = 142
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



STRESS RELAXATION MODULUS, QNB-3066 (ANT P-POLYMER LINED), 1000 SEC, 1% STRAIN

Figure 6-14

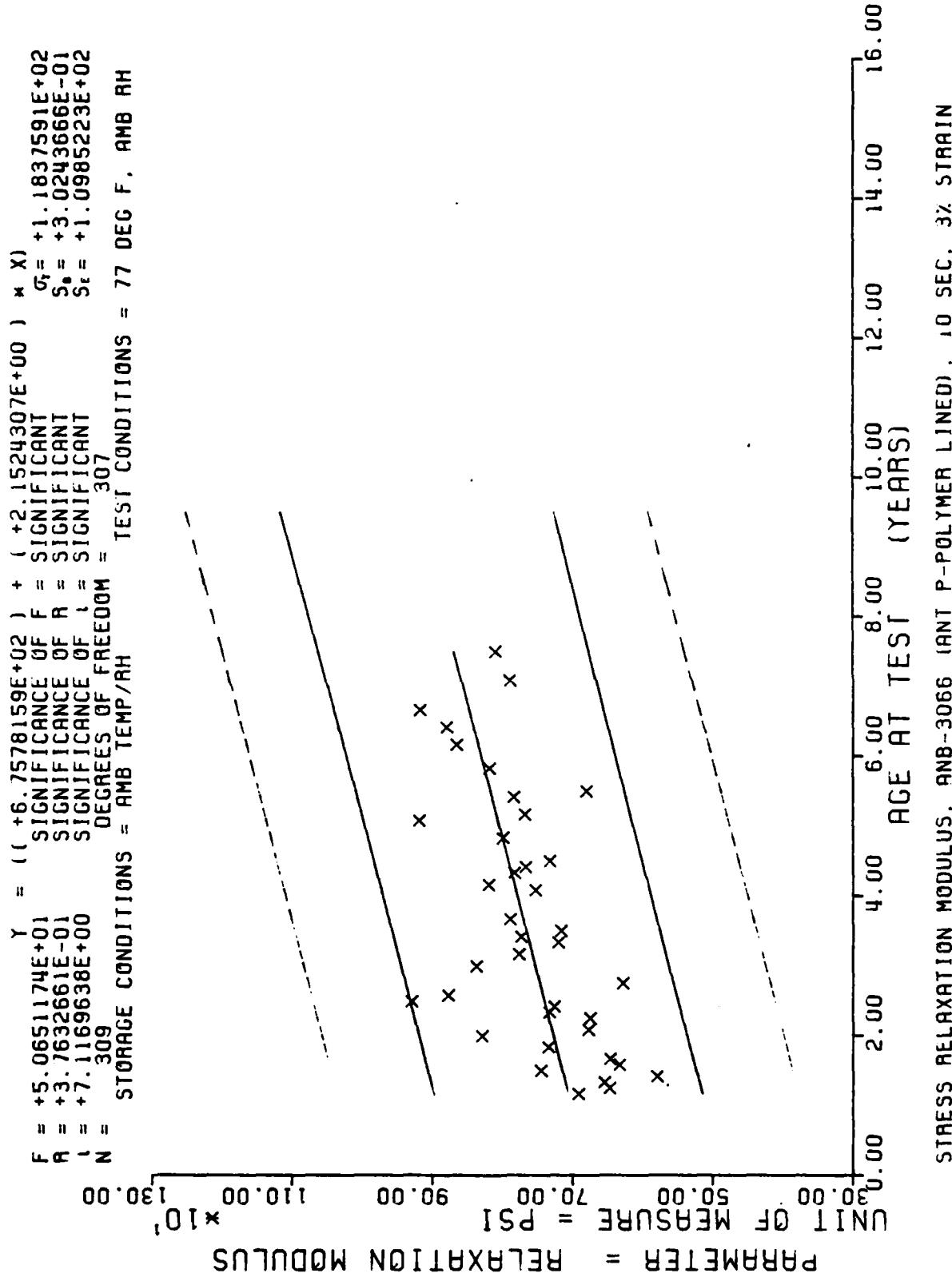


Figure 6-15

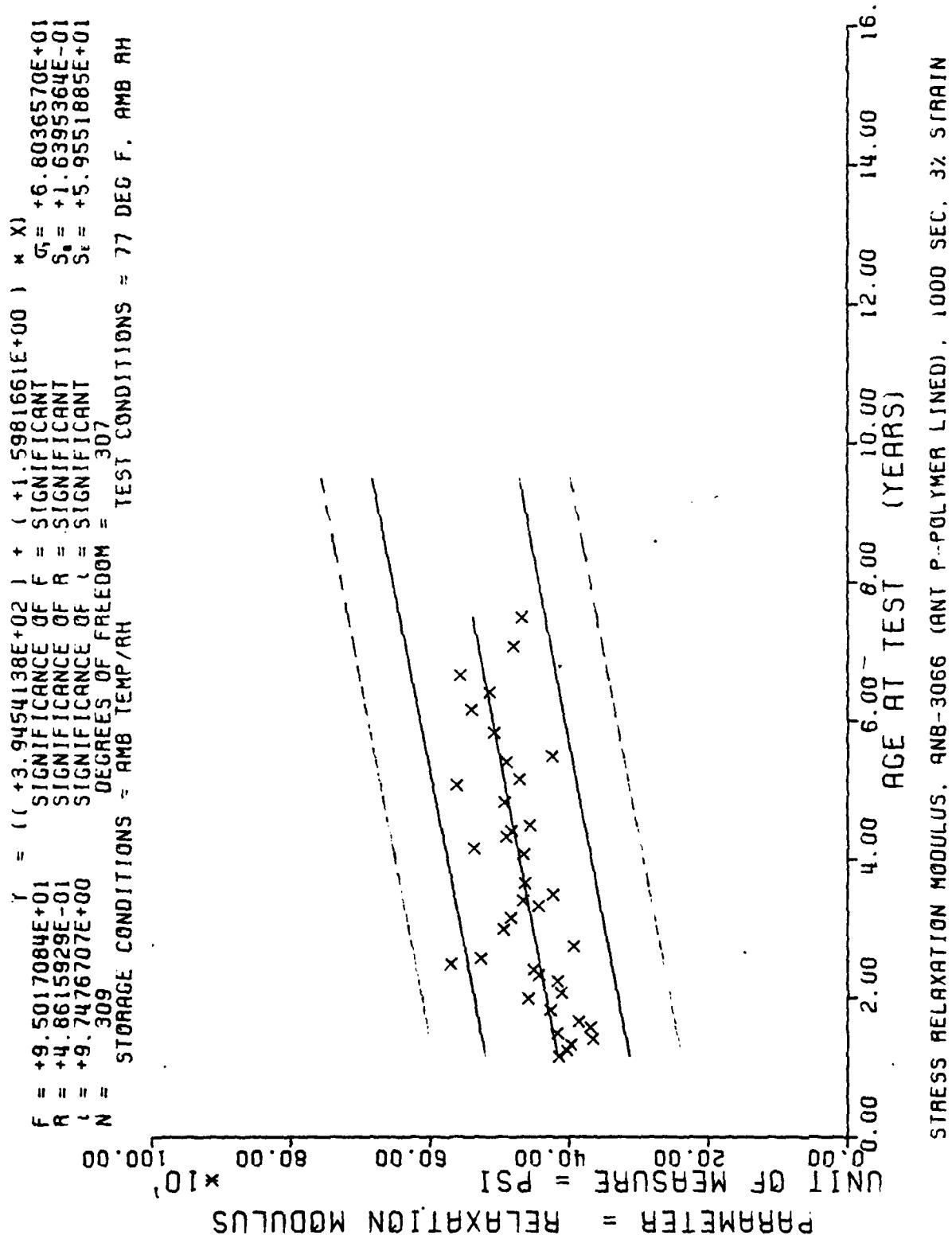


Figure 6-16

$F = +4.1606488E+00$
 $R = -1.3747087E-01$
 $t = +2.0397668E+00$
 $N = 218$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\gamma = ((+7.3579726E+02) + (-8.5378588E-01) * X) * \sigma_t = +1.7443472E+02$
 $S_a = \text{SIGNIFICANT}$
 $S_r = \text{SIGNIFICANT}$
 $S_f = \text{SIGNIFICANT}$
 $\text{DEGREES OF FREEDOM} = 216$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$

ANAG
 ANBG

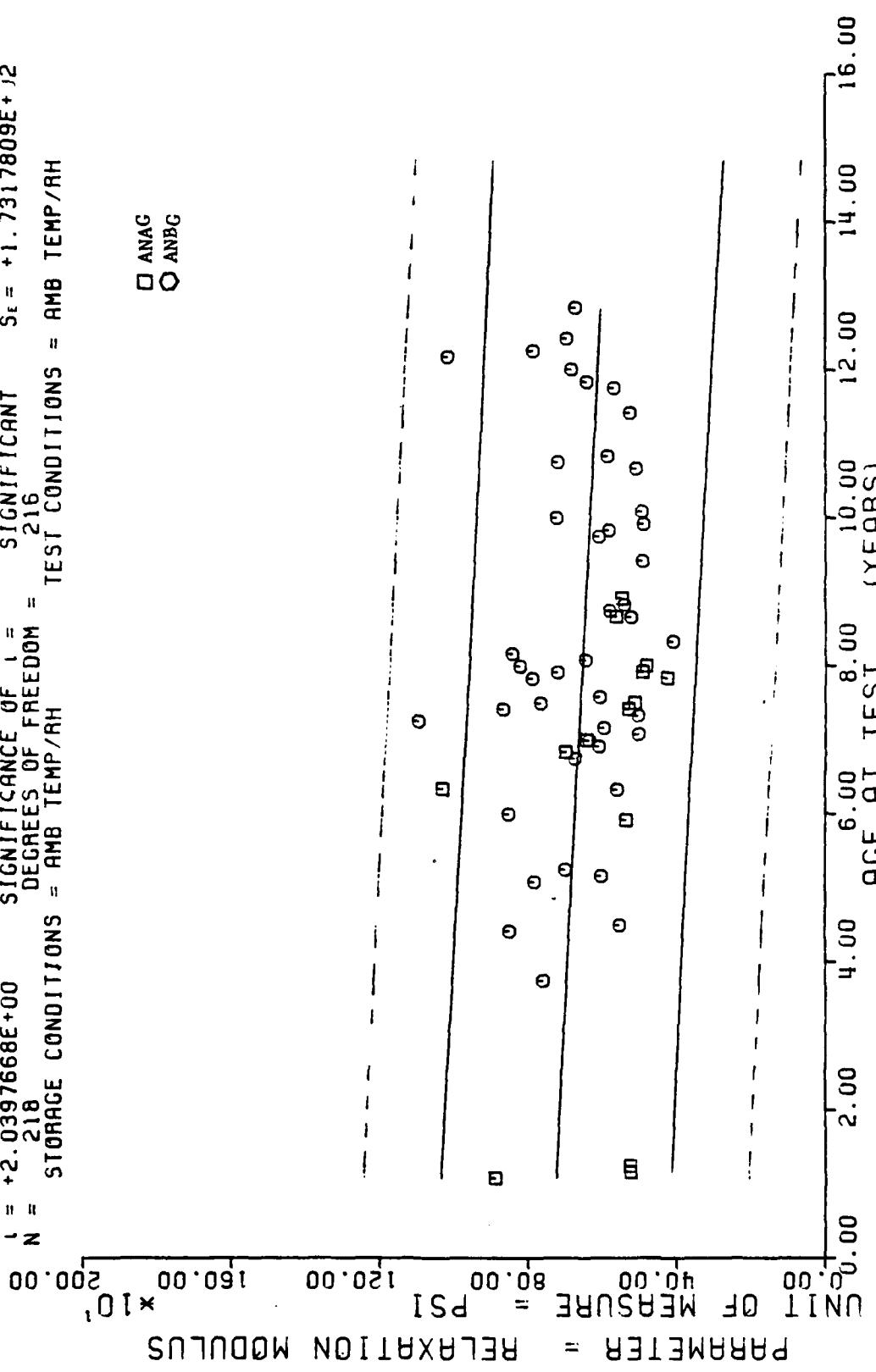


Figure 6-17

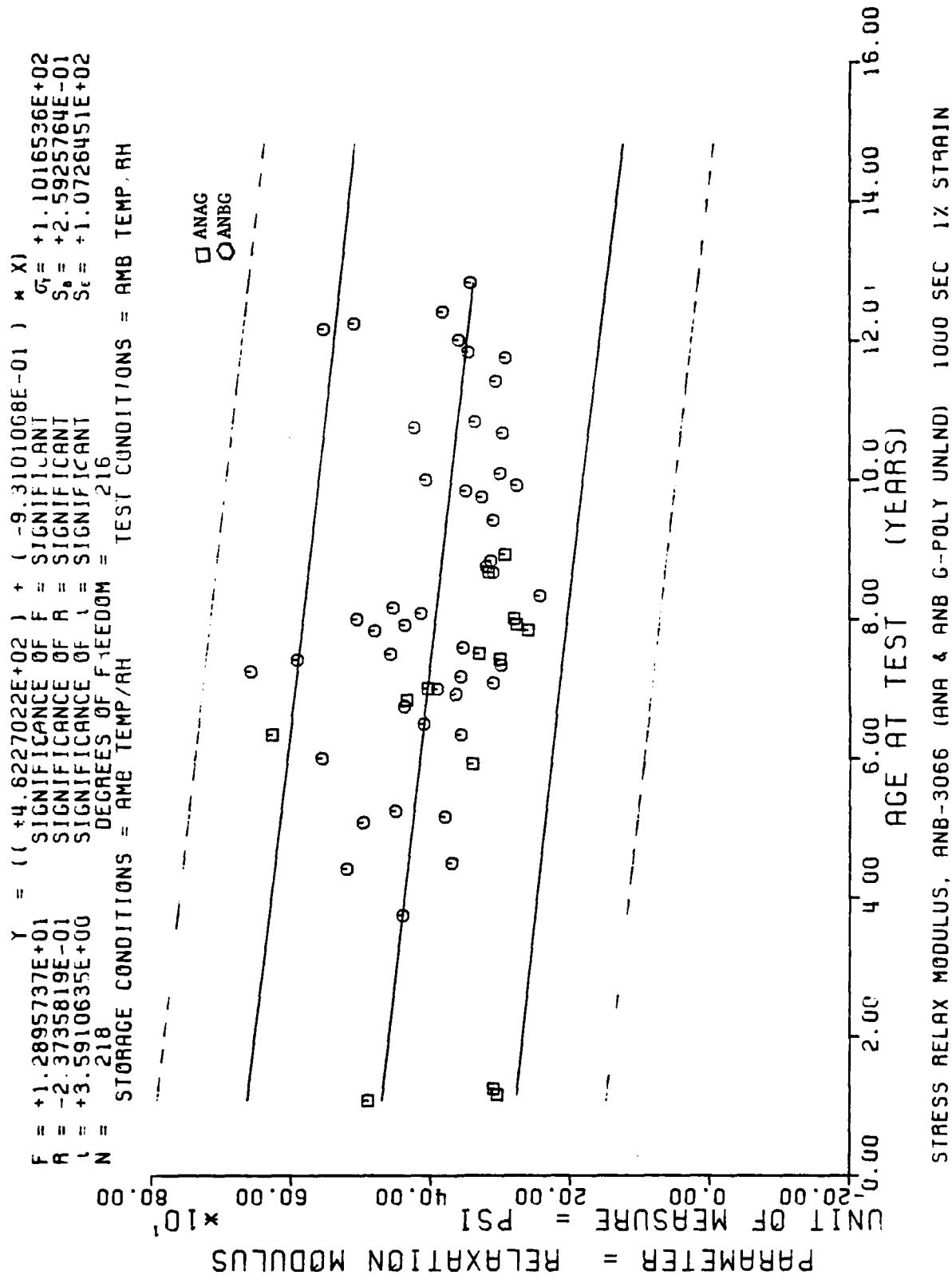


Figure 6-18

AD-A102 979

ODDEN AIR LOGISTICS CENTER HILL AFB UT PROPELLANT AN--ETC F/8 21/9.2
PROPELLANT SURVEILLANCE REPORT ANB-3066 PROPELLANT. (U)

DEC 80 E M DALABA

MAKPH-450(80)

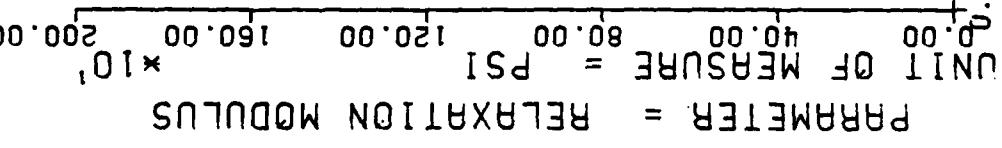
UNCLASSIFIED

NL

2 of 2
A102 979

END
DATE
FILED
9-8-81
DTIC

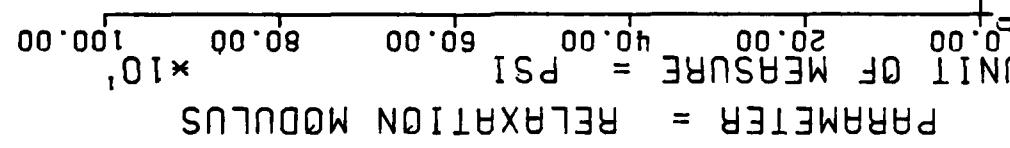
$\gamma = ((+6.6234143E+02) + (+2.1379174E+00) * X)$
 $F = \text{SIGNIFICANCE OF } F = \text{SIGNIFICANT}$
 $R = \text{SIGNIFICANCE OF } R = \text{SIGNIFICANT}$
 $I = \text{SIGNIFICANCE OF } I = \text{SIGNIFICANT}$
 $N = 324$
 $\text{STORAGE CONDITIONS} = \text{DEGREES OF FREEDOM} = 322$
 $\text{TEST CONDITION} = \text{AMB TEMP/RH}$



STRESS RELAX MODULUS, ANB-3066 (ANT & QNB P POLY UNLND), 10 SEC. IN STRAIN

Figure 6-19

$F = +1.8425693E+01$ $\gamma = ((+4.2277093E+02) + (+8.0032087E-01) \times X)$
 $R = +2.3264876E-01$ F = SIGNIFICANT
 $I = +4.2925160E+00$ R = SIGNIFICANT
 $N = 324$ SIGNIFICANCE OF TEST CONDITONS = AMB TEMP/RH
 $DEGREES OF FREEDOM = 322$ TEST CONDITIONS = AMB TEMP/RH



STRESS RELAX MODULUS. QNB-3066 (ANT & ANB P-POLY UNLND). 1000 SEC. IX STRAIN

Figure 6-20

$F = +3.9084643E+01$
 $R = +3.9297975E-01$
 $\chi^2 = +6.2517711E+00$
 $N = 216$
 SIGNIFICANCE OF DEGREES OF FREEDOM = 214
 SIGNIFICANCE OF R = SIGNIFICANT
 SIGNIFICANCE OF χ^2 = SIGNIFICANT
 TEST CONDITIONS = AMB TEMP/RH

$\gamma = ((+6.0726468E+02) + (+2.2996467E+00) \times X) \times Y$
 $\sigma_t = +1.2198399E+02$
 $S_b = +3.6703924E-01$
 $S_c = +1.1243180E+02$
 TEST CONDITIONS = AMB TEMP/RH

◊ ANTP
 + ANBP

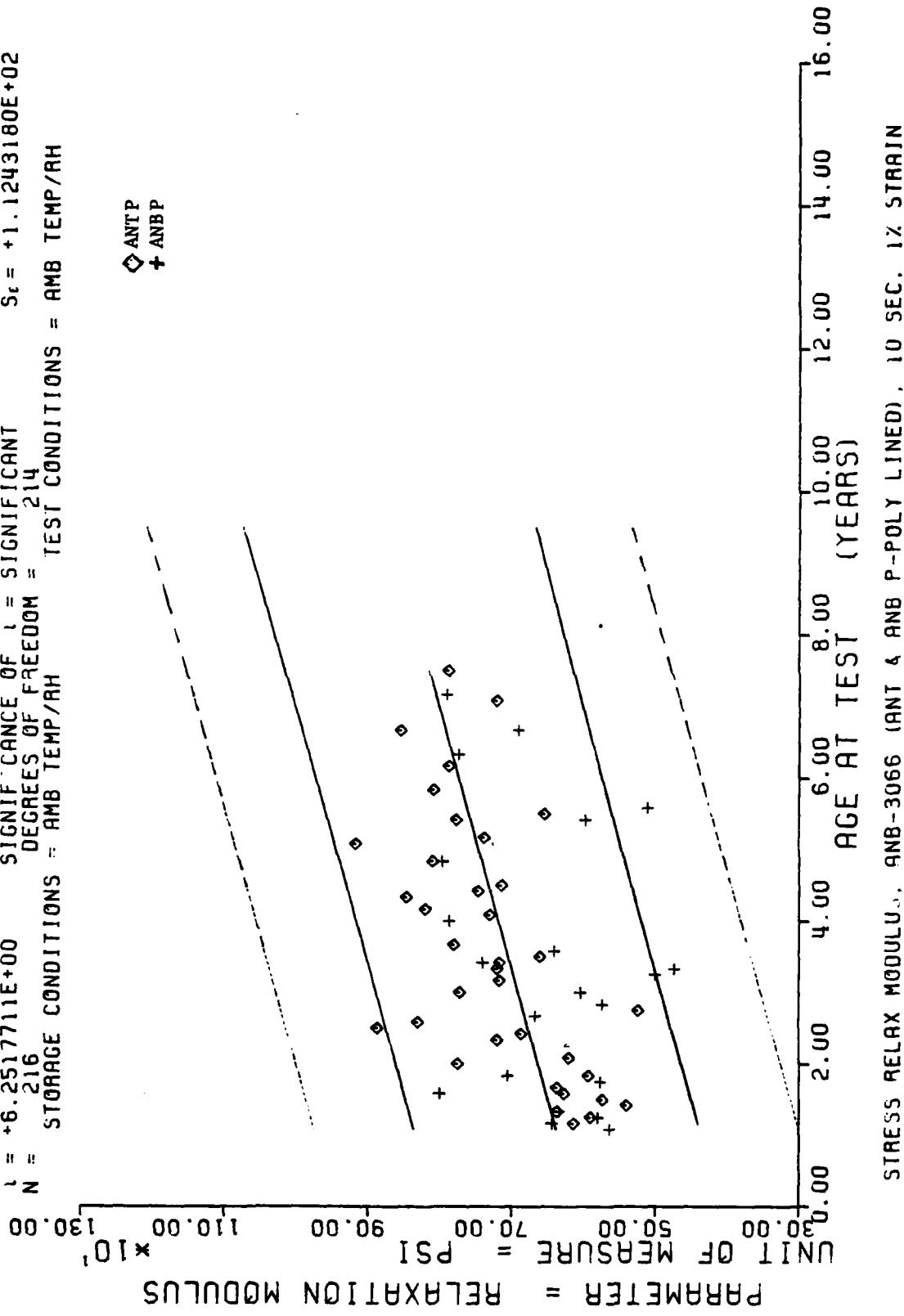


Figure 6-21

$F = +3.8865224E+01$ SIGNIFICANCE OF $F =$ SIGNIFICANT
 $R = +3.9204510E-01$ SIGNIFICANCE OF $R =$ SIGNIFICANT
 $I = +6.2341979E+00$ SIGNIFICANCE OF $I =$ SIGNIFICANT
 $N = 216$ DEGREES OF FREEDOM = 214

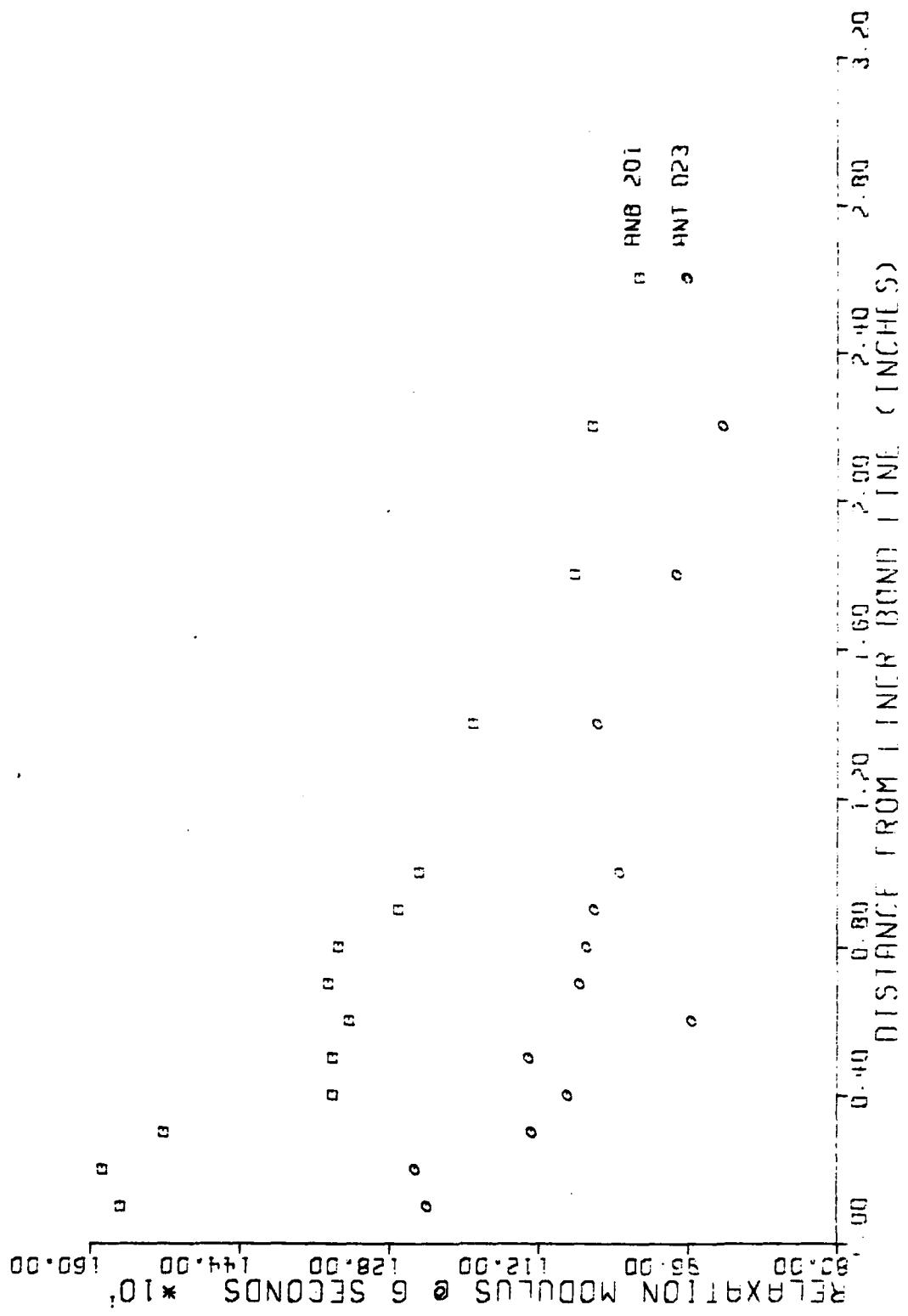
STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



STRESS RELAX MODULUS: ANB-3066 (ANT & ANB P-POLY LINED). 10³ SEC. 12 STRAIN

Figure 6-22

Figure 6-23



AMOUNT OF GROUND SURFACE RELAXATION MODULUS AT 37°

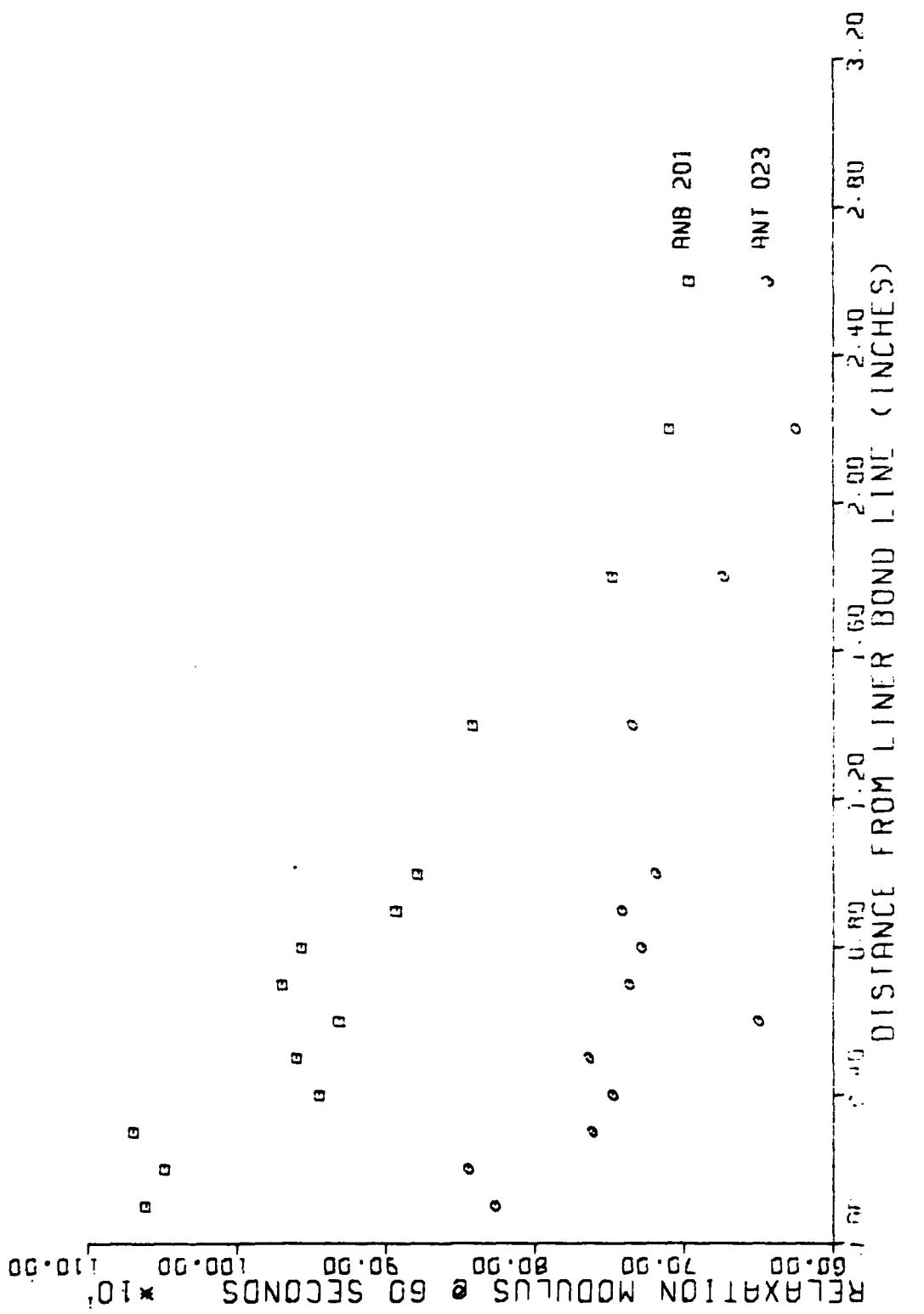


Figure 6-24

SECTION VII

THERMAL COEFFICIENT OF LINEAR EXPANSION

Thermal coefficient of linear expansion is run on the DuPont 990 Thermal Analyzer using the thermomechanical analyzer with expansion probe. The specimen used is a wafer approximately .200" (.508 cm) thick by .33" (.84 cm) diameter. The specimen is cooled to -110°C (-166°F) then heated at 5°C/min (9°F/min) to 40°C (104°F). The glass point (Tg), TCLE below Tg and TCLE above Tg are determined.

According to ASPC, where a volume coefficient of expansion is determined, the glass point for propellant stored at 80°F ranges from -91°C (-132°F) to -79.5°C (-111°F). All systems show a significant lowering of the glass point.

Expansion below the glass point is not considered to be a significant factor in analysis. This region is linear. Lined cartons of ANB "G" and "P" do not show a trend. Others show a significant increase.

TCLE above Tg is not significant for ANB "G" lined cartons. ANB "G" and "P" unlined cartons show a significant increase. ANB "P" lined and ANT "P" unlined and lined cartons show a significant decrease in this parameter.

TABLE 7-1
TCLE

Significance of Regression Slopes

<u>SYSTEM</u>	<u>Tg</u>	<u>Fig</u>	<u>Below Tg</u>	<u>Fig</u>	<u>Above Tg</u>	<u>Fig</u>
ANB "G" Unlined	Sig dec	7-1	Sig inc	7-2	Sig inc	7-3
ANB "G" Lined	Sig dec		NS		NS	
ANB "P" Unlined	Sig dec	7-4	Sig inc	7-5	Sig inc	7-6
ANB "P" Lined	Sig dec		NS		Sig dec	
ANT "P" Unlined	Sig dec	7-7	Sig inc	7-8	Sig dec	7-9
ANT "P" Lined	Sig dec	7-10	Sig inc	7-11	Sig dec	7-12

NS = Not significantly different from zero slope

Sig dec = Negative slope

Sig inc = Positive slope

$\gamma = ((-7.2665744E+01) + (-4.2050218E-02) * X) * \sigma$
 $\sigma = +3.4435779E+00$
 $S_a = +4.6003755E-03$
 $S_t = +3.2114046E+00$
 $F = +8.3550670E+01$ SIGNIFICANT
 $R = -3.6314853E-01$ SIGNIFICANT
 $L = +9.1406055E+00$ SIGNIFICANT
 $N = 552$ DEGREES OF FREEDOM = 550
 $\gamma = \text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$ TEST CONDITIONS = AMB TEMP/RH

UNIT OF MEASURE = DEG C
 PARAMETER = GLASS POINT
 0.00 2.00 4.00 6.00 8.00 10.00 12.00 14.00 16.00

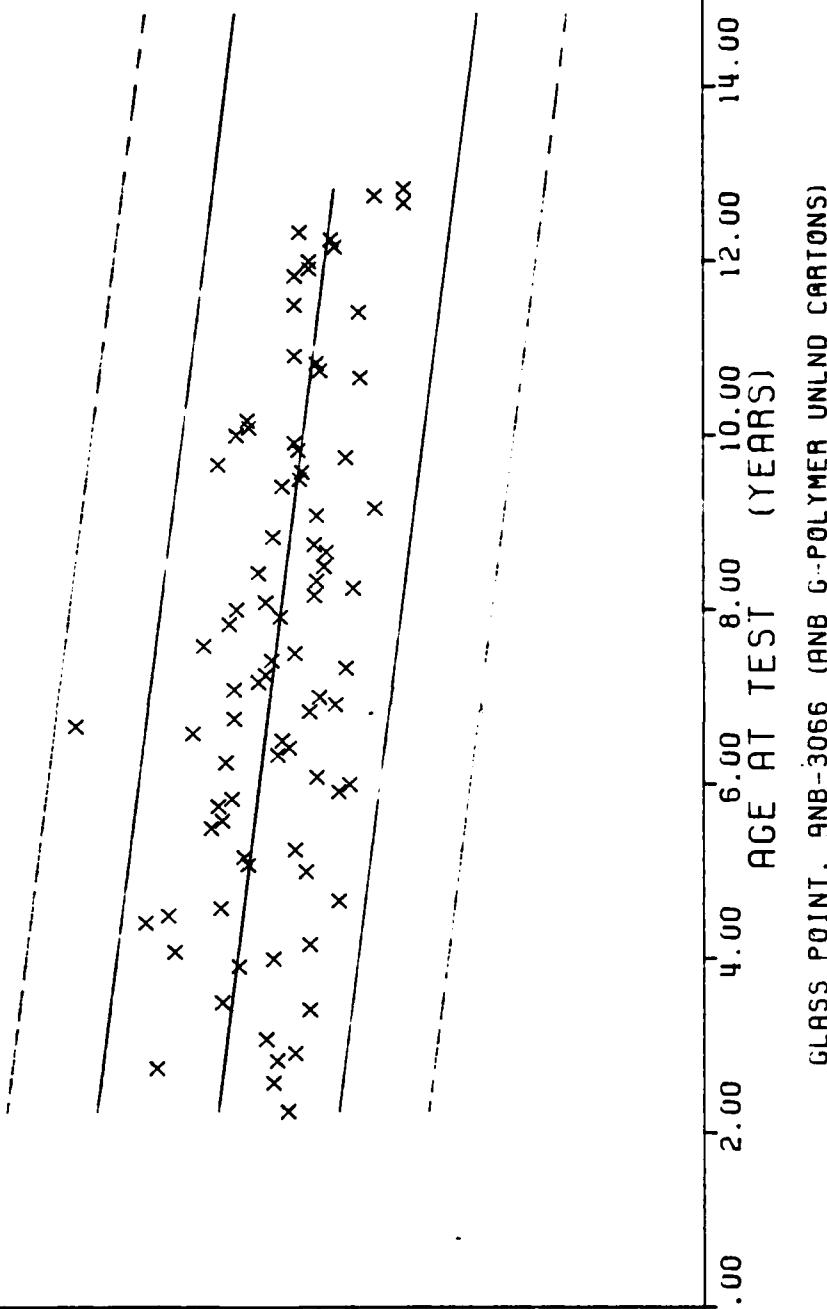


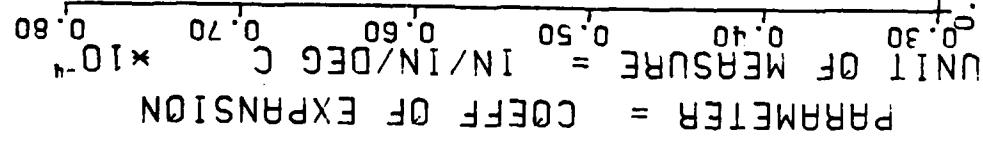
Figure 7-1

$F = +2.8541771E+01$
 $R = +2.3150673E-01$
 $t = +5.342499E+00$
 $N = 506$
 STORAGE CONDITIONS = AMB TEMP/RH

$$Y = ((+5.0525084E-05) + +5.4403078E-08) * X$$

$\sigma_F = +6.7056598E-06$
 SIGNIFICANCE OF F = SIGNIFICANT
 $S_F = +1.0183170E-08$
 SIGNIFICANCE OF R = SIGNIFICANT
 $S_R = +6.5299577E-06$
 SIGNIFICANCE OF t = SIGNIFICANT
 DEGREES OF FREEDOM = 504

TEST CONDITIONS = AMB TEMP/RH

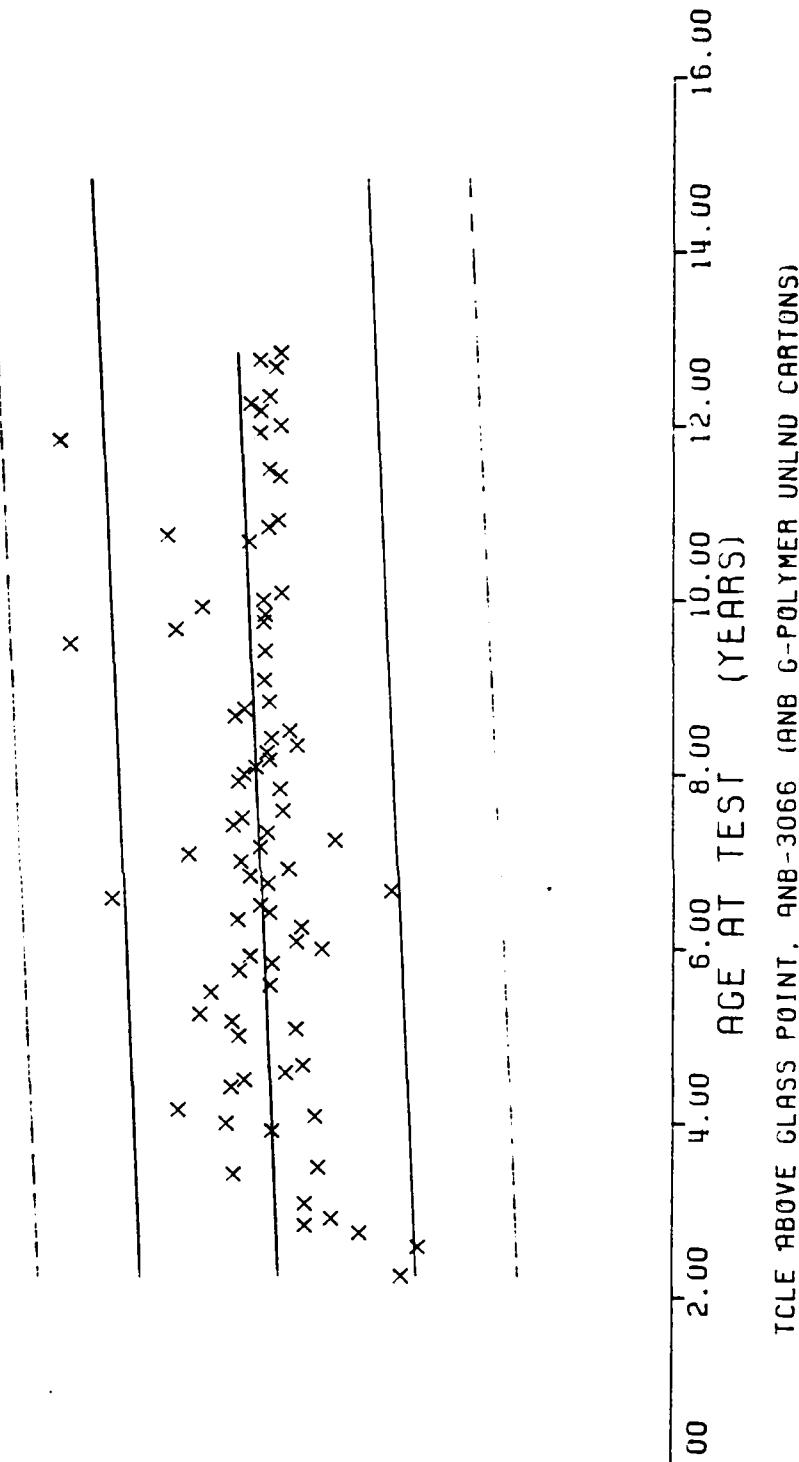


TCLE BELOW GLASS POINT. ANB-3066 (ANB G-POLYMER UNLND CARTONS)

Figure 7-2

$F = +7.9151916E+00$
 $\sigma_F = +8.7970235E-05$
 $F = \text{SIGNIFICANCE OF }$
 $\sigma_F = +7.5021302E-08$
 $F = \text{SIGNIFICANT}$
 $\sigma_F = +1.8383270E-05$
 $F = +1.2532912E-01$
 $F = \text{SIGNIFICANT}$
 $\sigma_F = +2.6665755E-08$
 $F = +2.8133950E+00$
 $F = \text{SIGNIFICANT}$
 $\sigma_F = +1.8256698E-05$
 $N = 498$
 $Degrees of Freedom = 496$
 $Storage Conditions = \text{AMB TEMP/RH}$
 $Test Conditions = \text{AMB TEMP/RH}$

PARAMETER = COEFF OF EXPANSION
 UNIT OF MEASURE = IN/IN/DEG C
 $*10^{-3}$
 0.00 0.04 0.08 0.12 0.16 0.20



TCLE ABOVE GLASS POINT, ANB-3066 (ANB G-POLYMER UNLND CARTONS)

Figure 7-3

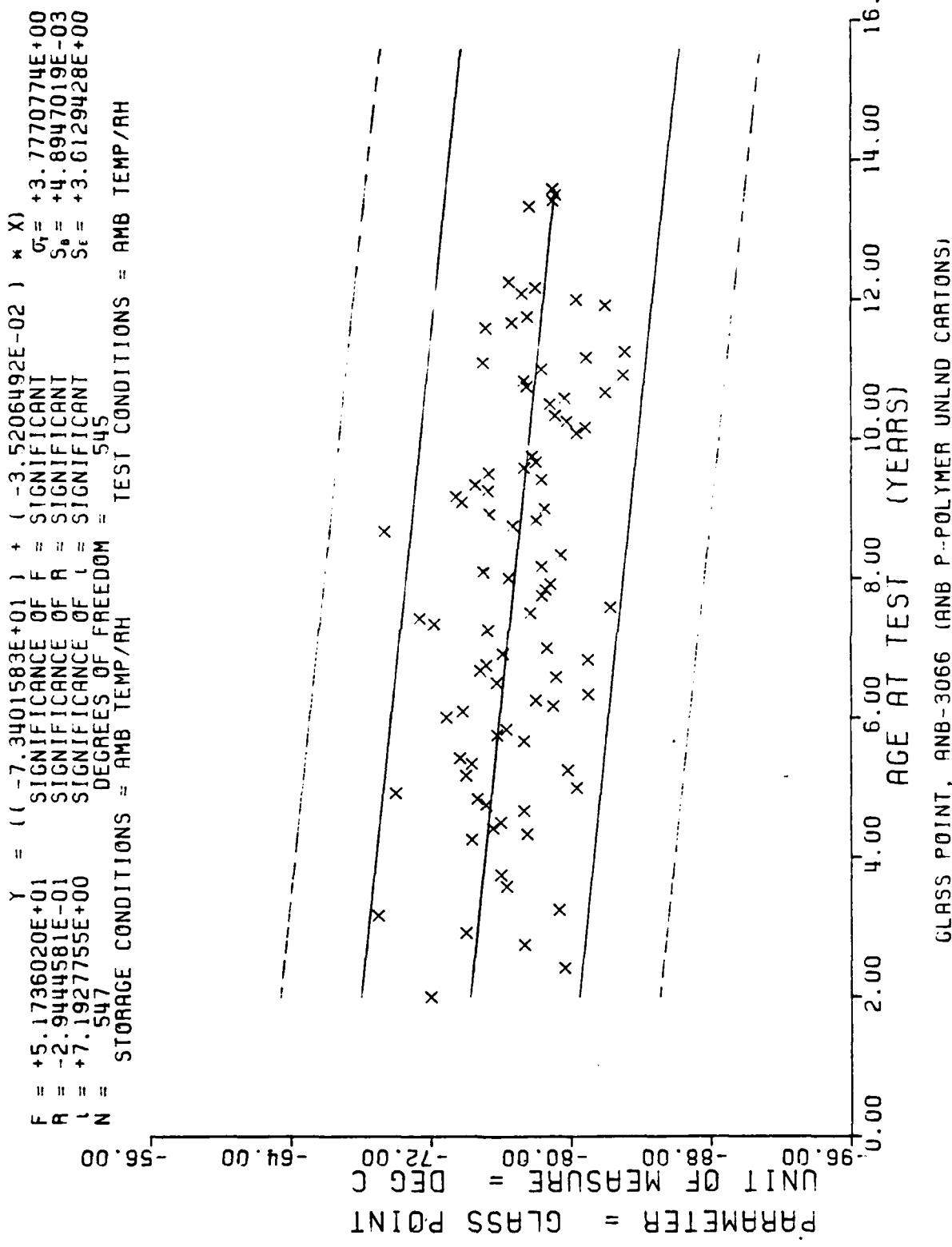


Figure 7-4

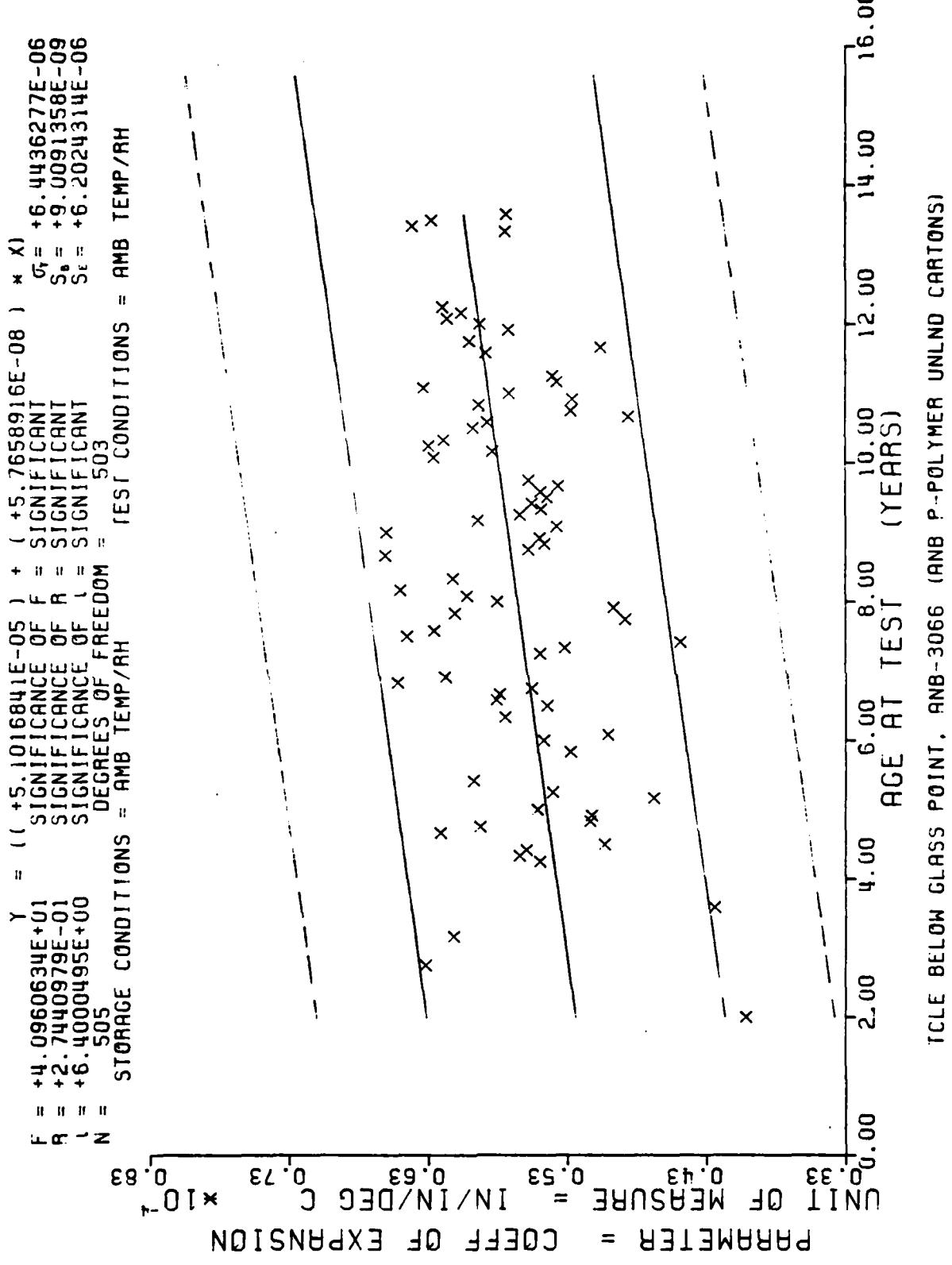
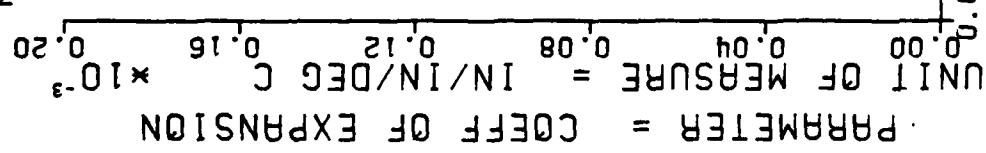


Figure 7-5

$y = (+8.8493186E-05) + (+8.9286053E-08) * x$
 $F = +9.9589215E+00$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = +1.3734286E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $t = +3.1557759E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $N = 520$ DEGREES OF FREEDOM = 518
 $S = \text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$ TEST CONDITIONS = AMB TEMP/RH



TCLE ABOVE GLASS POINT, ANB-3066 (ANB P-POLYMER UNLND CARTONS)

Figure 7-6

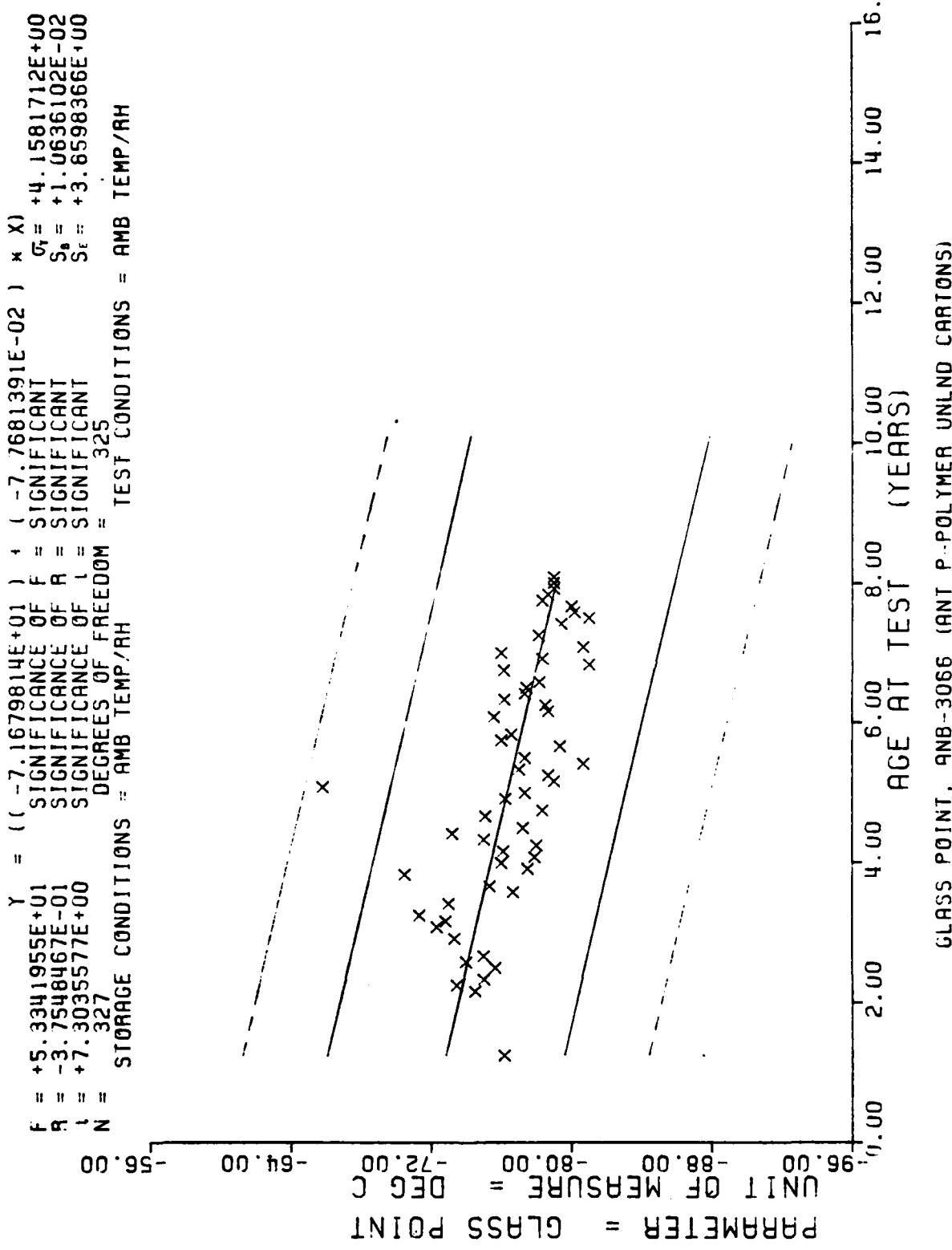
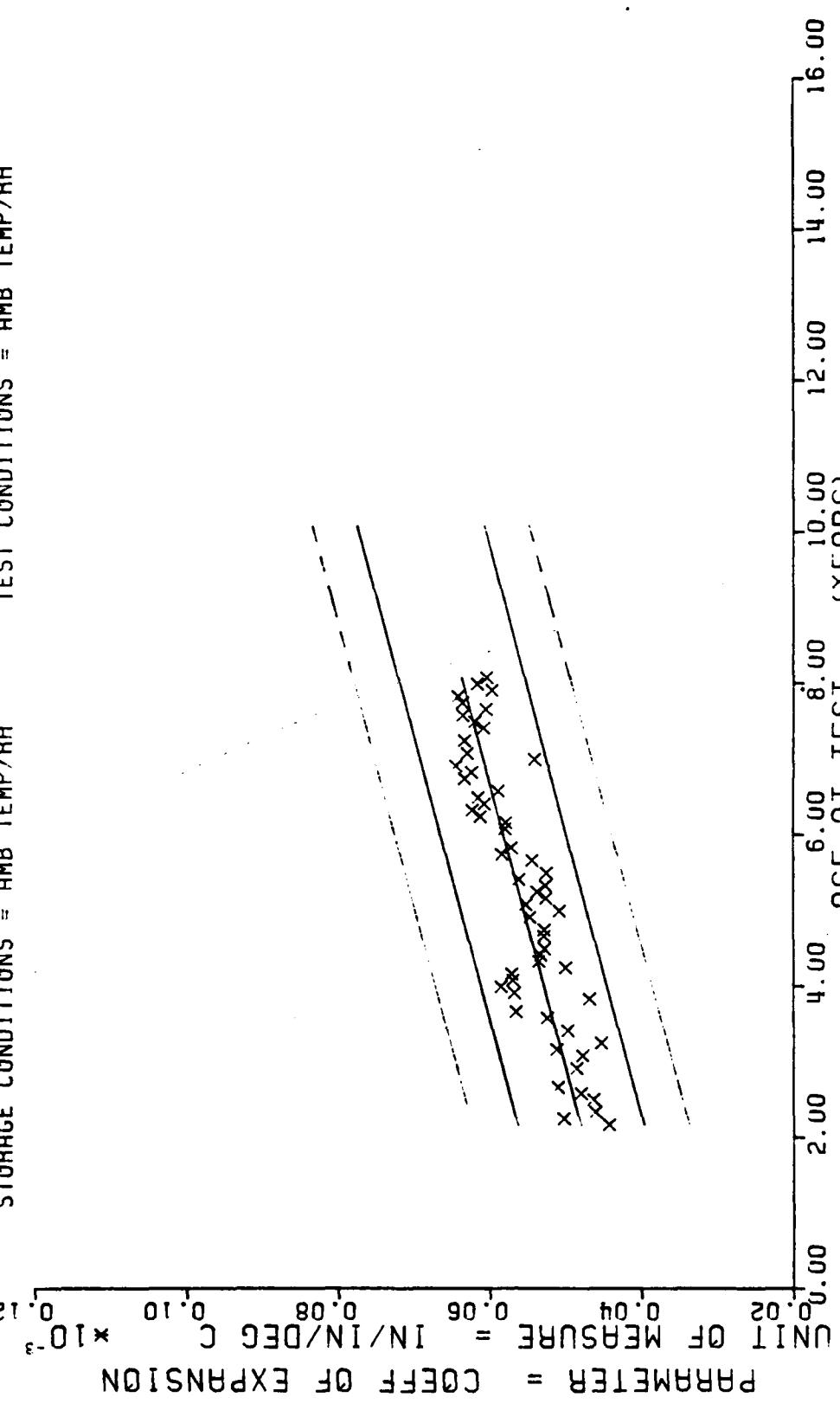


Figure 7-7

$F = +2.5884936E+02$
 $\sigma_F = +4.2197215E-05$
 $\alpha = +6.6929292E-01$
 $\sigma_\alpha = +1.0088796E+01$
 $N = 321$
 $\text{STORAGE CONDITIONS} = \text{AMB TEMP/RH}$
 $\text{DEGREES OF FREEDOM} = 319$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$
 $\text{SIGNIFICANCE OF } F = \text{SIGNIFICANT}$
 $\text{SIGNIFICANCE OF } \alpha = \text{SIGNIFICANT}$
 $\text{SIGNIFICANCE OF } N = \text{SIGNIFICANT}$
 $\text{TEST CONDITIONS} = \text{AMB TEMP/RH}$



TCLE BELOW GLASS POINT. QNB-3066 (ANT P-POLYMER UNLND CARTONS)

Figure 7-8

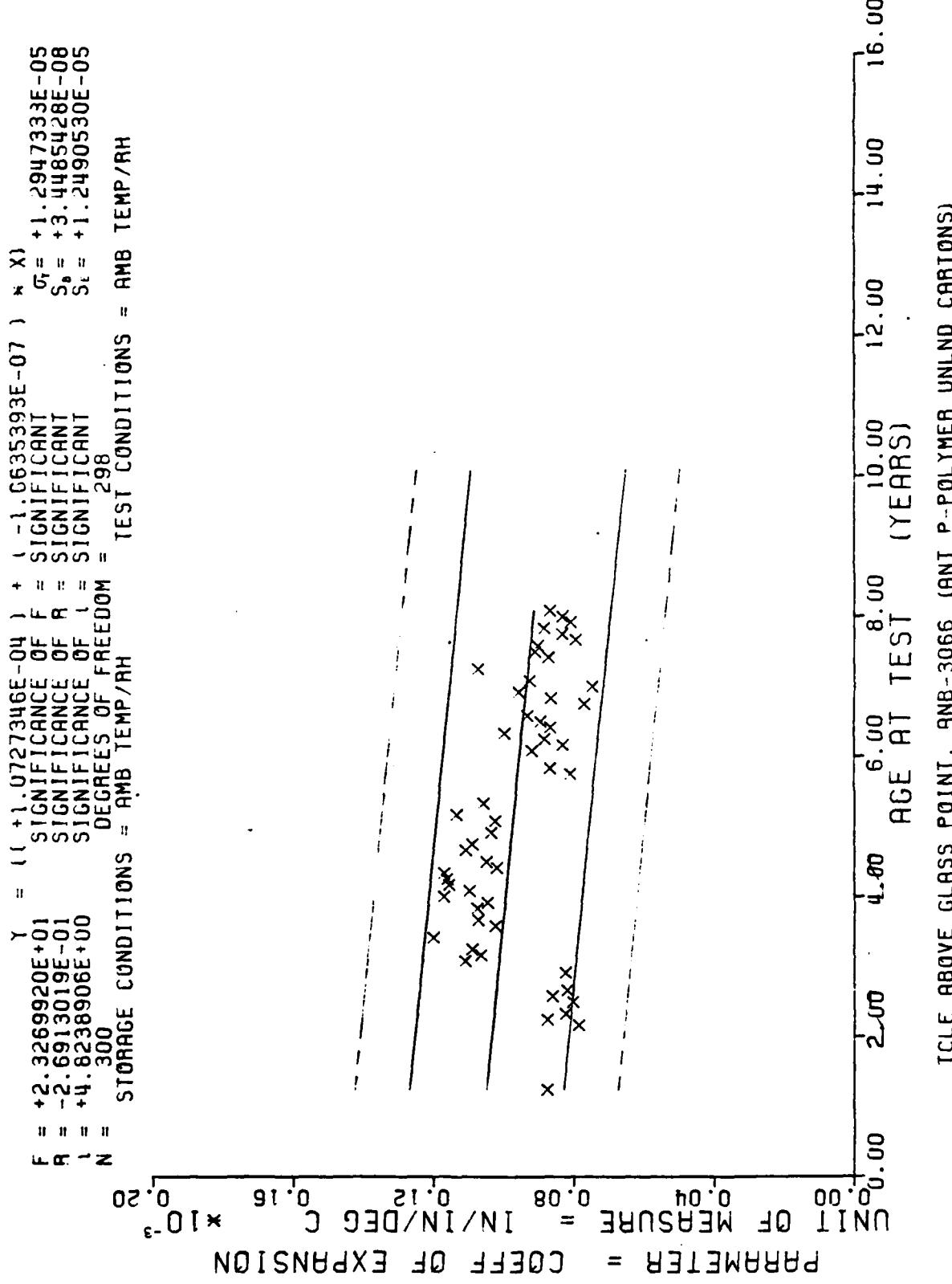


Figure 7-9

$y = (-7.5069317E+01) + (-3.5563139E-02) \times x$
 $F = +1.1399958E+01$ SIGNIFICANCE OF F = SIGNIFICANT
 $R = -1.9916283E-01$ SIGNIFICANCE OF R = SIGNIFICANT
 $t = +3.3763825E+00$ SIGNIFICANCE OF t = SIGNIFICANT
 $f = 278$ DEGREES OF FREEDOM = 276
 $N =$ STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

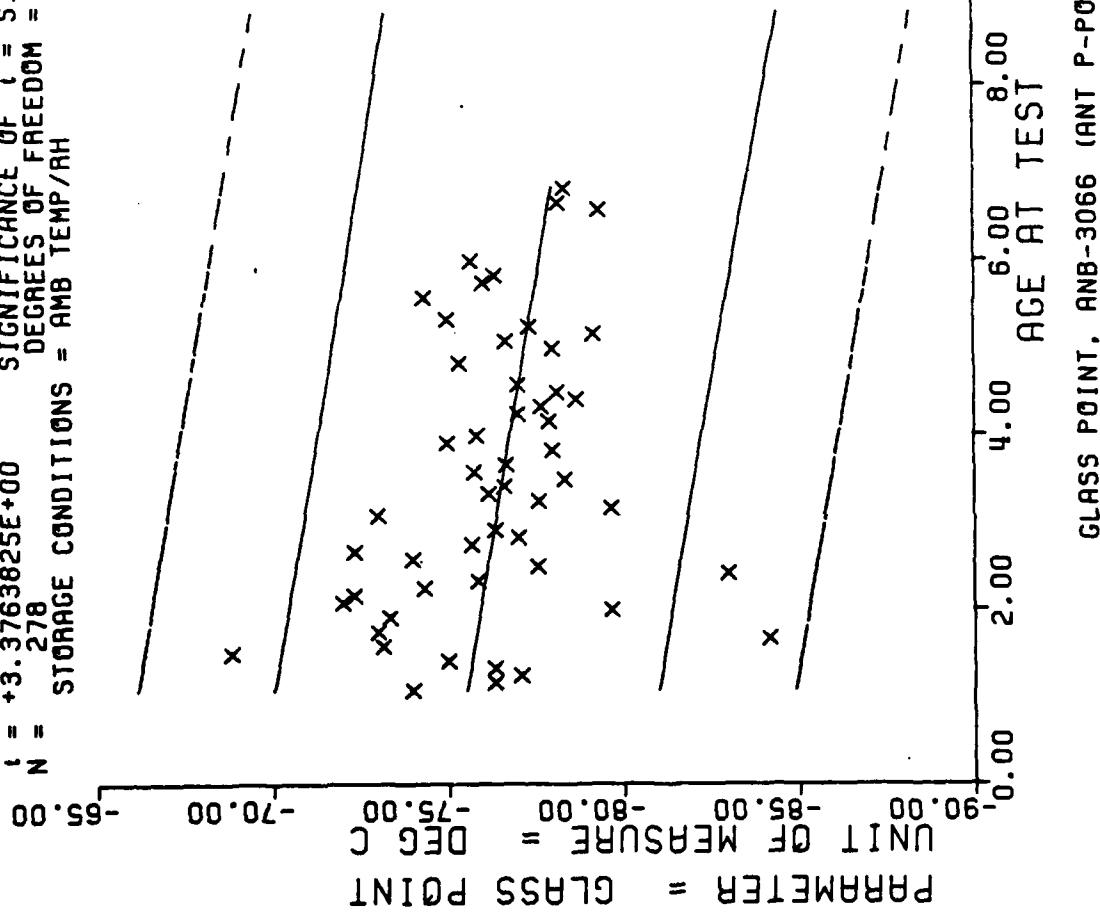


Figure 7-10

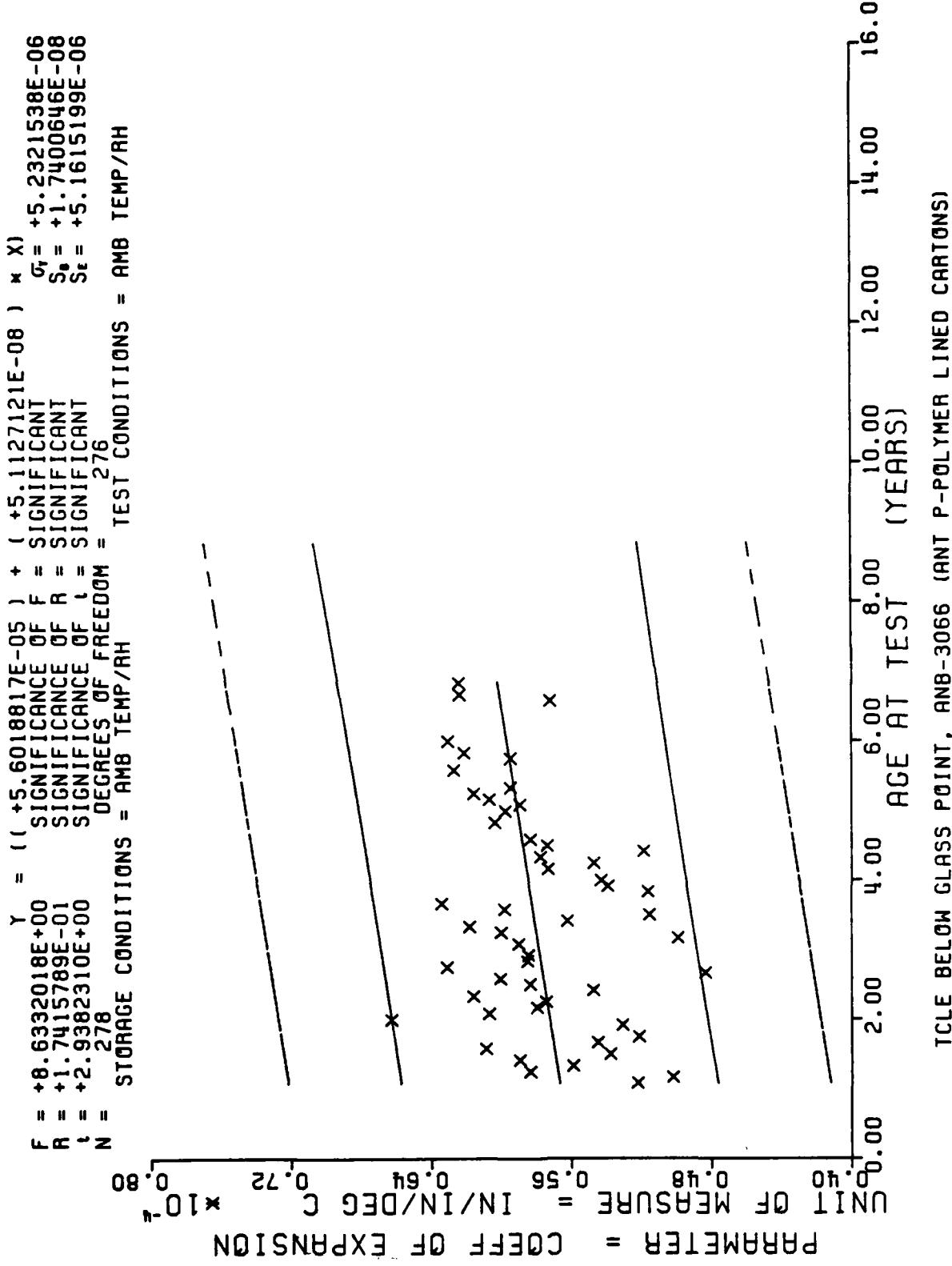
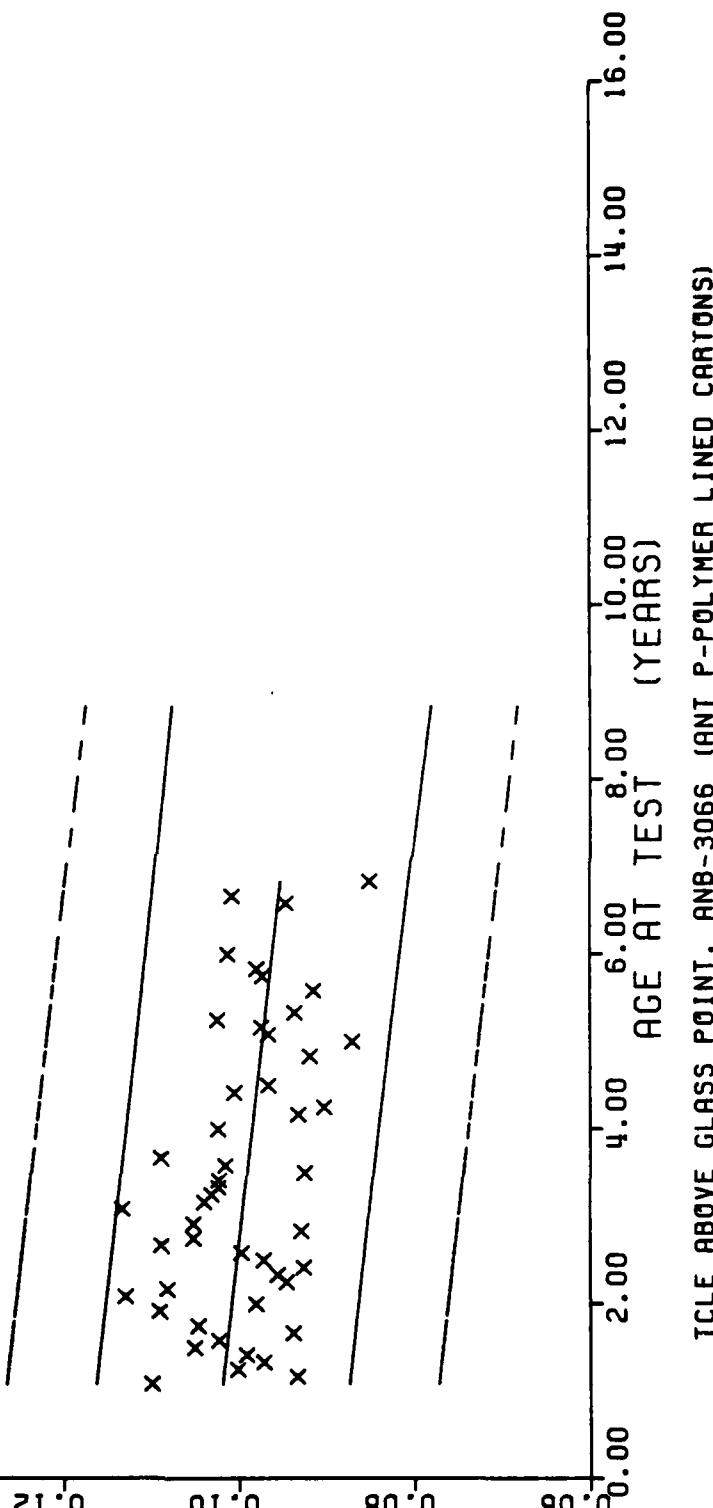


Figure 7-11

$F = +1.1886196E+01$ SIGNIFICANCE OF $F = \text{SIGNIFICANT}$
 $R = -2.1223309E-01$ SIGNIFICANCE OF $R = \text{SIGNIFICANT}$
 $t = +3.4476363E+00$ SIGNIFICANCE OF $t = \text{SIGNIFICANT}$
 $N = 254$ DEGREES OF FREEDOM = 252
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

PARAMETER = COEFF OF EXPANSION
 UNIT OF MEASURE = IN/IN/DEG C
 $\times 10^{-3}$



TCLE ABOVE GLASS POINT, ANB-3066 (ANT P-POLYMER LINED CARTONS)

Figure 7-12

SECTION VIII
CASE LINER BONDS

Cartons of propellant were lined with SD-851-2 liner/v45 rubber simulating motor conditions. In the preparation of the cartons, liner sometimes penetrated the propellant to a depth of 0.5 inches. Irregularities are most apparent on outer surfaces. Corners may be particularly affected by curvature of the insulation.

Liner color varies from a pale buff to deep buff or a deep pink which apparently develops from moisture plus anti-oxidant. In general, the pink liner tends to be sticky and strings out in tensile testing. Shear strength may be negligible.

Aerojet did a study of 44 manufacturing variables to determine those which had a significant effect on liner bond strength. According to their report (MVS-1, June 76) several factors had a statistically significant effect on bond strength. Initial high bond strength and low insulation moisture content usually mean a longer time to degradation of the liner bond.

OO-ALC has made an extensive statistical study of the constant load tensile and shear tests. Regressions for these data as well as other parameters will be published in a supplement to this report.

SECTION IX
TEAR ENERGY

Tear energy specimens are microtomed to a thickness of 0.1 in (.254 cm) from a block of propellant 3" x 1 1/8" x 1 1/2" (7.62 cm x 2.8 cm x 3.8 cm). The microtomed specimen is bonded to wood and a 1 inch (2.54 cm) slit is cut lengthwise in the center of the specimen. Specimens are tested at four temperatures (40°, 77°, 120° and 160°F) and three rates (0.01 in/min, 0.1 in/min and 1.0 in/min) on the Instron.

Time to tear is measured at crack initiation. Cohesive tear energy is calculated from the critical stress and strain at that same time. As with other tests involving increasing rates, time to tear decreases with an increasing rate. Cohesive energy usually decreases with increasing temperature.

Time to tear is a more consistent parameter than cohesive tear energy. Lined cartons of "P" Polymer do not show a trend at any temperature and unlined cartons of ANT P shows a significant increase at all temperatures. The dimensions of the specimen also enter into the calculation.

TABLE 9-1

TEAR ENERGY

Significance of Regression Slopes

<u>System</u>	<u>Temp °F</u>	<u>Cohesive Energy</u>	<u>Time to Tear</u>
ANB G Unlined	40	NS	NS
	77	Sig inc	Sig inc
	120	Sig inc	Sig inc
	160	Sig inc	Sig inc
ANB G Lined	40	NS	NS
	77	Sig inc	Sig inc
	120	NS	NS
	160	NS	Sig inc
ANB P Unlined	70	Sig inc	NS
	77	Sig inc	Sig inc
	120	Sig inc	Sig inc
	160	NS	NS
ANB P Lined	40	NS	NS
	77	NS	NS
	120	NS	NS
	160	Sig dec	NS
ANT P Unlined	40	Sig inc	Sig inc
	77	Sig inc	Sig inc
	120	NS	Sig inc
	160	NS	Sig Inc
ANT P Lined	40	Sig inc	NS
	77	NS	NS
	120	NS	NS
	160	NS	NS

NS = Not significantly different from zero slope

Sig inc = Positive slope

Sig dec = Negative slope

DISTRIBUTION

	<u>NR</u> <u>COPIES</u>
OOALC	
MMWRBM	1
MMWRAM	1
DDC (TISIR) Cameron Station, Alexandria, VA 22314	2
SAMSO, Norton AFB, CA 92409	1
Attn: Mr. Sanford Collins, Bldg 562, Room 613	
AFFPRO, Aerojet, Sacramento, CA 95813	1
Aerojet Strategic Propulsion Company	1
P. O. Box 15699C, Sacramento, CA 95813	
Attn: Mr. R. Kiefer for Mr. Stan Lake	
AFRPL (MKPB) Edwards AFB, CA 93523	1
SAC (LGBM) Offutt AFB, NB 68113	1
U. S. Naval Ordnance Station, Indian Head, MD 20460	1
M. E. Loman, Code 3012A4	
Air Launched Weapons Branch	
Weapons Quality Engineering Center	
CPIA, Johns Hopkins University	1
Applied Physics Lab	
John Hopkins Road, Laurel, MD 20810	
Attn: Mr. Ronald D. Brown	

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER MAKPH Report Nr 450(80)	2. GOVT ACCESSION NO. AD-A102979	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Propellant Surveillance Report ANB-3966 Propellant	5. TYPE OF REPORT & PERIOD COVERED Test Results / Semi Annual	
6. AUTHOR(s) ELIZABETH M. DALABA	7. PERFORMING ORG. REPORT NUMBER	
8. PERFORMING ORGANIZATION NAME AND ADDRESS Propellant Analysis Laboratory Directorate of Maintenance 00-ALC Hill AFB, UT 84056	9. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
10. CONTROLLING OFFICE NAME AND ADDRESS Ammunitions Management Division Directorate of Materiel Management 00-ALC Hill AFB, UT 84056	11. REPORT DATE December 1980	
12. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)	13. NUMBER OF PAGES 121	
	14. SECURITY CLASS. (of this report) Unclassified	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release, distribution unlimited	17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)	
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Solid Propellant Minuteman		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report contains test results from LGM-30 F & G, Stage II and Stage III Propellant. Data are shown in linear regression plots. The differences between polymers used in the propellant are shown in the composite plots for very low rate tensile, high rate tensile and stress relaxation data and is most evident in gradient stress relaxation modulus. Case liner bonds continue to show significant degradation although the rate of change has slowed.		

